Comune di Padova (PD)

Provincia di Padova

Piazza Bardella, 2
Padova

Realizzazione di nuovo edificio ad uso scolastico
in Area Ex Configliachi di Via Guido Reni

Indagine geognostica
caratterizzazione geologica e geotecnica

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Indice

1. PREMESSA 3

2. INQUADRAMENTO DELL'AREA 4

4. ASSETTO GEOLOGICO – STRATIGRAFICO, GEOMORFOLOGICO ED IDROGEOLOGICO LOCALE 6

5. INDAGINE GEOGNOSTICA ESEGUITA 8

6. RISULTATI DELL' INDAGINE GEOGNOSTICA 16

7. VALUTAZIONE DELL'AZIONE SISMICA 23

8. CONCLUSIONI 3

ALLEGATO 1: CPTU E SCPTU 4

ALLEGATO 2: LIQUEFAZIONE 40

ALLEGATO 3: SONDAGGIO A CAROTAGGIO CONTINUO – STRATIGRAFIA, FOTO CASSETTE E CAMPIONI GEOTECNICI 127

ALLEGATO 4: TRINCEE ESPLORATIVE 155

ALLEGATO 5: RISPOSTA SISMICA LOCALE 159

1. PREMESSA

La presente relazione viene prodotta a corredo del progetto di nuova costruzione di un edificio ad uso scolastico all'interno dell'area Ex Configliachi, in Via Guido Reni del Comune di Padova commissionata dalla Provincia di Padova (Determina Dirigenziale n.1592 del 22/12/2025).

La presente nota costituisce quindi la "Relazione Geologica" prevista dal D.M. 17/01/2018 aggiornamento alle "Norme tecniche per le costruzioni" al punto 6.2.1 "Caratterizzazione e modellazione geologica del sito" e 6.2.2 "Indagini, caratterizzazione e modellazione geotecnica", in accordo con la circolare n. 7 del Consiglio Superiore dei Lavori Pubblici del 21/01/2019; essa, pertanto, descrive le operazioni di indagine eseguite ed i relativi risultati.

L'indagine geognostica è consistita, come previsto nel piano di indagine e previa esecuzione di prescavi con pala meccanica, nell'esecuzione di due prove penetrometriche statiche con piezocono (CPTU) spinte fino a -20 m (CPTU1-2) ed una prova penetrometrica statica con punta sismica (SCPTU) spinta a 30 m di profondità dal piano campagna, oltre ad un sondaggio a carotaggio continuo a -10 m dal piano campagna; all'interno del foro di sondaggio è stato installato un piezometro a 6 m di profondità. In fase di esecuzione del sondaggio sono stati infine prelevati n. 2 campioni indisturbati da sottoporre ad analisi geotecniche.

E' stata inoltre eseguita una verifica sismica ottenuta mediante la prova SCPU è stata inoltre integrata, con il metodo della sismica passiva HVSR.

Alla presente relazione è allegata la documentazione completa relativa alle indagini eseguite:
Allegato 1:

- certificato di laboratorio con i dati numerici risultanti da ciascuna prova penetrometrica eseguita (CPTU e SCPTU);
- suddivisione stratigrafica del sottosuolo;

Allegato 2: vengono riportate le elaborazioni relative alla verifica alla liquefazione dei terreni.

Allegato 3: stratigrafia del sondaggio a carotaggio continuo e risultati di laboratorio geotecnico sui campioni indisturbati prelevati durante l'esecuzione del sondaggio.

Allegato 4: stratigrafie di trincee eseguite per mezzo di escavatore

Allegato 5: riporta l'elaborato della Risposta sismica locale.

2. INQUADRAMENTO DELL'AREA

L'area di cui trattasi si trova in Via Guido Reni, all'interno del complesso denominato Ex Configliachi, da molti anni dismesso (Figura 1 e 2).

La previsione del nuovo edificio scolastico vede la sua realizzazione parte in area occupata da un corpo di edificio ora demolito (ancora visibile in Figura 1 e Figura 2) e parte nell'area attualmente a verde.



Figura 1: ubicazione area su carta tecnica regionale (riduzione da scala 1:10.000)



Figura 2: foto dell'area da via Berti (a est)

In un quadro geologico regionale l'area interessata dal progetto appartiene all'area della bassa pianura veneta, tale fascia territoriale si inquadra in un complesso sistema deposizionale fluviale di stile a meandri in cui si sono avvicendate nel tempo le diverse modalità di sedimentazione dei singoli fiumi che interessano l'area in oggetto. I processi di sedimentazione fluviale in ambito di pianura hanno portato alla deposizione di materiali a granulometria fine con una notevole variabilità laterale di facies legata alla presenza di macroforme sedimentarie che risultano dalla sedimentazione cumulativa che spazia in tempi anche lunghi. Da ciò risulta che i depositi appartenenti ad ogni singolo sistema non sono sufficientemente delineabili e distinguibili da permettere di creare delle unità di pertinenza relative ad ogni singolo corso d'acqua o riconducibili a formazioni geologiche differenziate o di facies specifiche.

In generale quindi il sottosuolo risulta costituito per spessori di centinaia di metri da depositi alluvionali di limi ed argille prevalenti rispetto a livelli sabbiosi.

Dal punto di vista idrogeologico il territorio in esame è caratterizzato dalla struttura idrogeologica comune a tutta la bassa pianura padano-veneta determinata dalla presenza nel sottosuolo di materiali sciolti di diversa granulometria, compresi tra le argille e le sabbie, quindi dotati, oltre che di diverse caratteristiche geotecniche, anche di permeabilità assai variabile.

I vari corpi stratigrafici costituiti da questi materiali, presenti frequentemente in termini misti, sono sovrapposti e variamente interdigitati. La loro genesi deriva principalmente dall'attività di deposizione fluviale recente (Quaternaria).

Il suddetto assetto stratigrafico definisce una differenziazione del sottosuolo in corpi a diversa permeabilità: corpi acquiferi (costituiti da sabbie, quindi permeabili) confinati entro livelli

impermeabili o a bassissima permeabilità (costituiti da banchi di limi ed argille). Risulta inoltre sempre presente una falda superficiale di tipo freatico (non in pressione) la cui superficie è posta appena al di sotto del piano campagna; più che di una singola falda freatica si tratta di un insieme di limitate falde in sabbie e/o limi sabbiosi sub-superficiali in comunicazione idraulica tra loro e talora dotate di debole pressione.

Tale falda superficiale risulta fisicamente e idraulicamente separata dal sistema acquifero profondo, a causa dei già citati potenti livelli argillosi impermeabili, essa trae alimentazione prevalentemente dagli afflussi meteorici diretti.

4. ASSETTO GEOLOGICO – STRATIGRAFICO, GEOMORFOLOGICO ED IDROGEOLOGICO LOCALE

La situazione geologico-stratigrafica a scala locale viene evidenziata nella “Carta Litologica” del “Piano di Assetto Territoriale” (PAT) comunale (anno 2014).

Nell’estratto della suddetta carta, riportato in Figura 3, si può osservare come la litologia dell’area di cui trattasi risulti caratterizzata dalla presenza di terreni di natura coesiva (prevalentemente limi e argille).

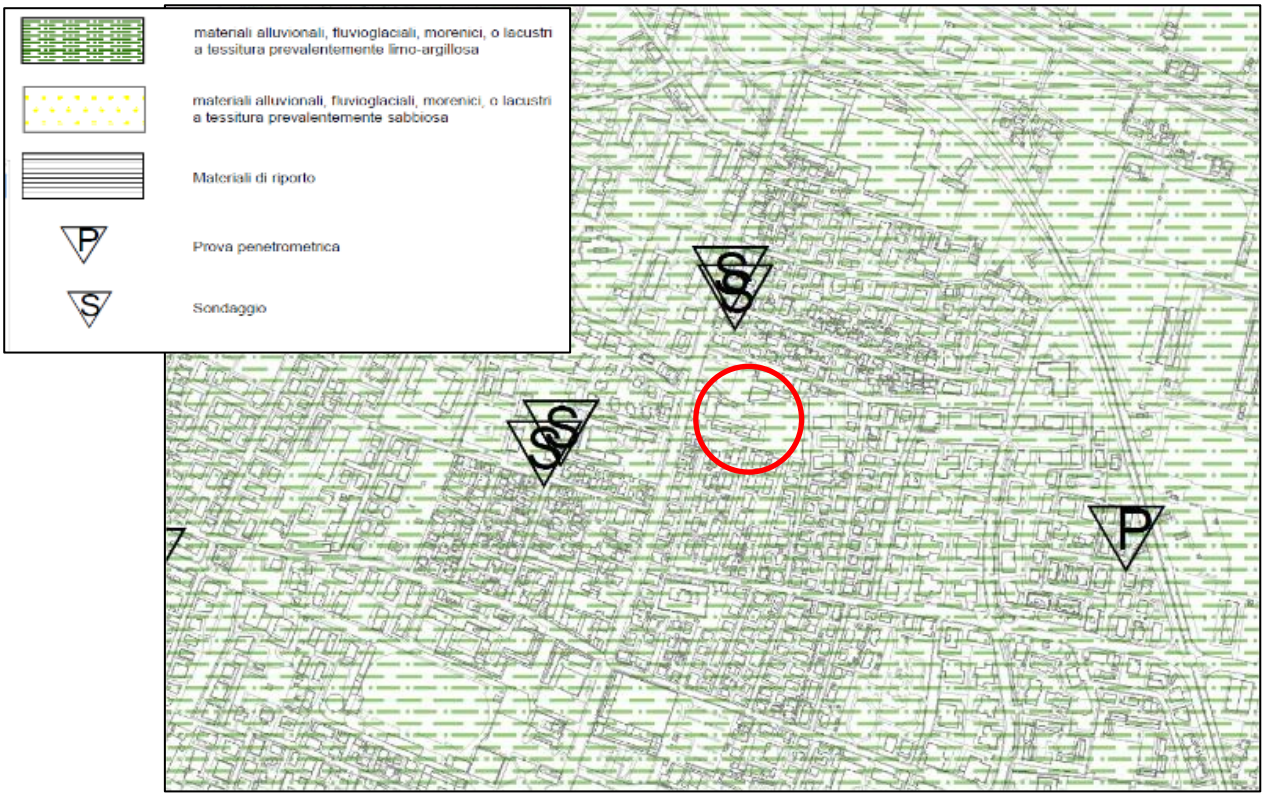


Figura 3: estratto Carta Litologica del PAT comunale

Morfologicamente l'area si inserisce in un contesto di bassa pianura alluvionale, interessata da corsi d'acqua, che per le basse pendenze dell'alveo, sviluppano per lo più un andamento meandriforme (piana di divagazione a meandri). In particolare, si possono distinguere anche aeree in cui il fiume Brenta, scorrendo pensile sulla pianura, ha sviluppato un modello di deposizione a dossi e depressioni (pianura modale e depressioni), si parla quindi di paleoalvei, antichi meandri, dossi fluviali.

Le forme naturali sono costituite dalle tracce superficiali dei corsi fluviali estinti, dalle fasce di divagazione fluviale, dai dossi e dagli argini fluviali. Come sempre in aree fortemente antropizzate sono evidenti e spesso prevalenti forme di modellamento morfologico antropico quali arginature, scavi e rilevati.

Riguardo alle caratteristiche geomorfologiche del comune non si evincono nell'area di studio elementi di particolare interesse geomorfologico, si veda a tal proposito l'estratto della Carta Geomorfologica del PAT comunale.

Dal punto di vista idrogeologico, l'elemento che incide con la realizzazione delle opere riguarda il solo livello della falda acquifera superficiale

Dall'estratto della carta idrogeologica della provincia di Padova si nota che la falda superficiale ha profondità media di 2,0 m da p.c.

Le oscillazioni medie della falda sono stimabili in ± 1m nel corso delle variazioni annuali.

La Carta Idrogeologica del PAT (vedi estratto in Figura 4) fornisce informazioni sulla profondità della falda freatica superficiale e sulla generale direzione di deflusso. Nell'area di progetto la falda si pone entro i 2 m di profondità dal p.c. mentre la direzione di deflusso è circa da nord a sud.

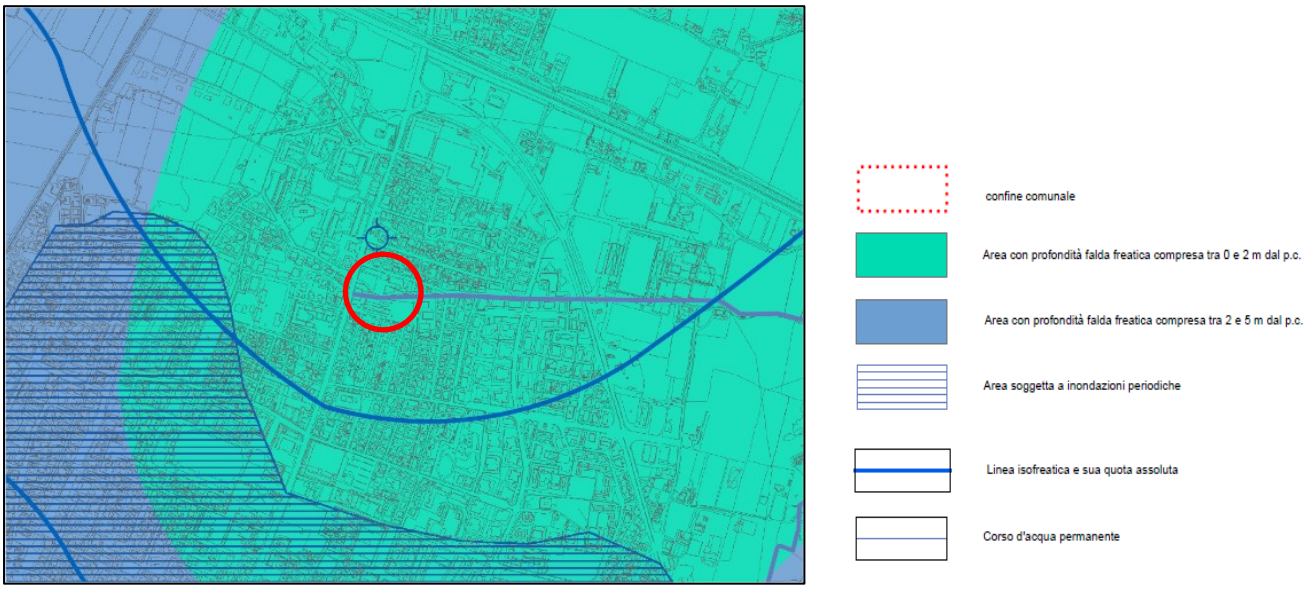


Figura 4: estratto "Carta Idrogeologica" del PAT comunale

5. INDAGINE GEOGNOSTICA ESEGUITA

La situazione rilevata in fase di indagine ha consentito di rispettare sostanzialmente le attività previste.

In data 11/02/2026 è stato eseguito lo scavo di n. 6 trincee con escavatore meccanico per la verifica del materiale del primo sottosuolo nonché della presenza di sottoservizi in funzione della successiva esecuzione di indagini profonde. Le trincee sono state spinte fino a circa -1,1 m di profondità dal piano campagna.

In data 23/02/2026 e 05/03/2026 sono state eseguite tre prove penetrometriche statiche con piezocono: CPTU2 e CPTU3, spinte fino alla profondità di -20 m da p.c. oltre ad una prova penetrometrica con piezocono e punta sismica (SCPTU1) spinta fino a -30 m da p.c..

In data 26/02/2026 è stato eseguito un sondaggio a carotaggio continuo spinto a 10 m dal piano campagna, durante la perforazione sono stati prelevati n. 2 campioni indisturbati destinati ad analisi geotecniche. I campioni sono stati successivamente consegnati al laboratorio Geodata srl di Ponte San Nicolò (PD). In fase di sondaggio è stata inoltre eseguita una prova di permeabilità in foro tipo "Lefranc" sull'unico livello sabbioso rilevato in fase di sondaggio nel quale la prova risultasse significativa.

Al termine della perforazione è stato installato un tubo piezometrico in pvc atossico alla profondità di 6 m dal piano campagna, del diametro di 3'', con tratto filtrato tra -2 m e -6 m dal piano campagna, denominato PZ1.

Le prove penetrometriche sono state necessariamente eseguite in corrispondenza di alcune delle trincee eseguite in precedenza per la verifica di assenza dei sottoservizi e previa rimozione di frammenti grossolani di materiale alloctono di riporto qualora presente. Per tale motivo i valori registrati fino alla profondità di scavo delle trincee non risultano significativi.

In Figura 5 si riportano le ubicazioni dei posizionamenti delle prove penetrometriche, delle trincee eseguite nonché l'ubicazione del sondaggio a carotaggio continuo (S1), a seguire le foto delle prove penetrometriche, le foto delle trincee e del sondaggio (Figura 6).

Nei seguenti allegati saranno visibili gli elaborati e le stratigrafie delle indagini svolte:

- Allegato 1: Cptu e Scptu;
- Allegato 2: verifica alla liquefazione sulla base delle prove penetrometriche;
- Allegato 3: Sondaggio a carotaggio continuo (stratigrafie e foto);
- Allegato 4: Trincee esplorative (stratigrafie e foto).



Figura 5: ubicazione delle prove penetrometriche (CPTU- SCPTU) e delle trincee (T)

SCPTU1 (30 m da p.c.)	CPTU2 (20 m da p.c.)	CPTU3 (20 m da p.c.)
		





SONDAGGIO S1





TRINCEA T1 (prof.-1,1 m da p.c.)




TRINCEA T2 (prof. -1,1 m da p.c.)





TRINCEA T3 (prof. -1,1 m da p.c.)




TRINCEA T4 (prof. -1,2 m da p.c.)





TRINCEA T5 (prof. -1,1 m da p.c.)



TRINCEA T6 (prof. -1,1 m da p.c.)

Figura 6: foto del posizionamento del penetrometro, trincee e scavi

PROVE PENETROMETRICHE (CPTU E SCPTU)

Le prove penetrometriche statiche con piezocono (punta elettrica) permettono di effettuare in continuo, per ogni cm di avanzamento, la misura dei valori di resistenza alla punta (qc) e dell'attrito laterale locale (fs). La punta elettrica standard è dotata di un trasduttore di pressione che acquisisce il valore della pressione neutra (U) del terreno attraversato.

Le misure di qc e fs sono effettuate direttamente alla profondità della sonda e sono: continue e puntuali, indipendenti tra loro, relative alla stessa profondità (a meno della distanza tra sezioni di misura) inoltre risultano accurate ed estremamente ripetibili.

Il segnale è inviato in superficie mediante dei cavi elettrici che scorrono all'interno della cavità centrale delle aste e sono collegati al sistema di acquisizione in superficie, viene misurata anche la forza totale di spinta per il controllo della stabilità del sistema.

Il parametro pressione interstiziale (U) permette di interpretare in modo più accurato la stratigrafia del terreno. Da ogni strato poi possono essere stimati i parametri geotecnici.

Tramite il piezocono sismico si ha a disposizione un sistema per determinare, oltre alla stratigrafia ed i parametri geotecnici, anche la velocità delle onde di taglio. Esso permette di determinare, in contemporanea ai parametri di una prova penetrometrica statica (qc, fs, U), le velocità delle onde di taglio (Vs); è costituito da geofoni triassiali ortogonali tra di loro secondo le direzioni X, Y e Z.

L’utilizzo di due accelerometri posti ortogonalmente tra di loro consente di acquisire un segnale significativo dell’onda sismica a prescindere dall’orientamento della sonda (durante la fase di infissione non è possibile mantenere un orientamento prestabilito).

Il sistema di energizzazione deve generare prevalentemente onde di taglio a larga ampiezza con poche componenti compressionali. L’analisi del segnale avviene graficando i singoli segnali registrati dagli accelerometri. Lo schema seguente (Figura 7) illustra il funzionamento del sistema.

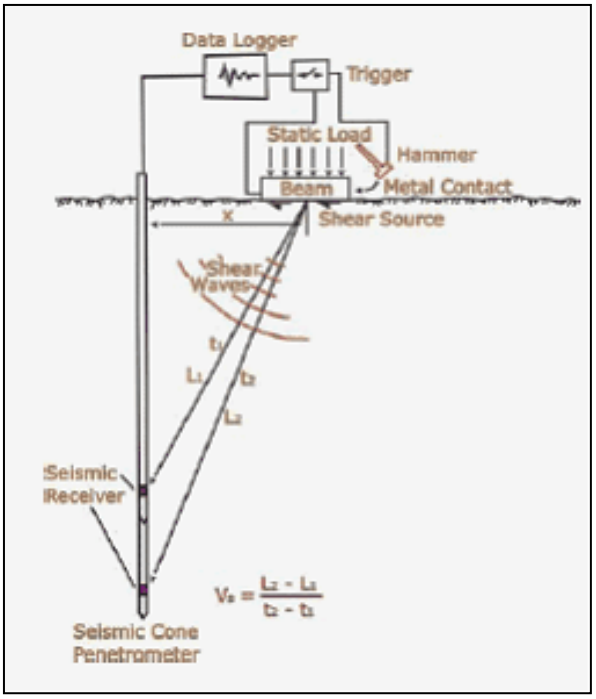


Figura 7: Schema di acquisizione SCPTU

Per la valutazione dei tempi di arrivo si può utilizzare il metodo cross-over della sovrapposizione di due segnali polarizzati.

Dai valori dei tempi di arrivo sono state calcolate le Vs relative al tratto sorgente-accelerometro e successivamente le Vs nel livello litologico.

Per la stima delle categorie di profilo stratigrafico si fa quindi riferimento alle nuove Norme Tecniche per le Costruzioni (2018).

Nel corso dell’indagine denominata SCPTU, sono state eseguite le registrazioni dei tempi di arrivo delle onde Vs a determinate profondità. La metodologia prevede di eseguire, alla stessa profondità, una battuta a destra e una battuta a sinistra rispetto alla verticale dove è infisso il modulo sismico. Successivamente, tramite il software SPAS della ditta Geologismiki, si elabora il segnale ed i tempi di arrivo delle onde S in modo da ottenere i valori di Vs alle varie profondità per le singole battute (destra e sinistra) dalle quali poi ottenere i valori medi di Vs.

SONDAGGIO A CAROTAGGIO CONTINUO

Il sondaggio è stato eseguito con sonda cingolata, in data 26/02/2026, la perforazione è stata spinta fino a -10 m dal piano campagna, le carote sono state deposte in apposite cassette catalogatrici. Sono stati prelevati da esso due campioni indisturbati durante la perforazione del sondaggio. Si veda la seguente tabella.

Profondità prelievo (m da p.c.)	**Nome campioni geotecnici**	**Litologia**
Da -3,2 m a -3,8 m	S1-C1	Limo argilloso grigio
Da -6,0 m a -6,5 m	S1-C2	Limo e argilla grigio

Tabella 1: campioni indisturbati prelevati dal sondaggio S1

La stratigrafia rilevata ha permesso di ricostruire la stratigrafia del sottosuolo fino alla profondità raggiunta. In Allegato 3 vengono riportate le foto delle cassette e la colonna stratigrafica nonché i certificati del laboratorio geotecnico.

Al termine del sondaggio è stato installato un piezometro a tubo aperto in PVC atossico, diametro 3'', spinto a – 6 m di profondità dal piano campagna, con ubicazione dei filtri da -2 a -6 m dal piano campagna. Il pozzetto di protezione del piezometro, in plastica rossa, è stato installato fuori terra (Figura 8). Il livello di falda misurato in data 05/03/2026 è di -1,3 m da b.p.



Figura 8: Piezometro PZ1 – profondità 6 m

6. RISULTATI DELL' INDAGINE GEOGNOSTICA

Trincee eseguite con escavatore meccanico

Le trincee svolte per mezzo di escavatore meccanico, in data 11/02/2026, hanno messo in luce la seguente situazione stratigrafica:

- Tra 0,2 e 0,3 - 0,45 m da p.c. è presente terreno limoso nocciola/marrone con presenza di rari elementi ghiaiosi (terreno alloctono);
- Tra 0,3-0,45 e 1,2-1,8 m da p.c. è presente limo sabbioso o sabbia limosa alloctono, di color da marrone a marrone scuro, con talora presenza di materiale antropico, talvolta grossolano (ghiaia, ciottoli, frammenti di laterizi, frammenti di calcestruzzo, frammenti di inerti da demolizione);
- Tra 1,2-1,8 e 2,7 m da p.c. è presente il terreno naturale in posto limo argilloso e argilla limosa di color marrone/nocciola, compatta a partire da circa 2 m di profondità.

Le stratigrafie delle trincee eseguite sono riportate in Allegato 2.

CPTU E SCPTU

Le prove penetrometriche eseguite nell'area mettono in evidenza un sottosuolo caratterizzato da alternanze di terreni granulari (sabbie limose e limi sabbiosi) e terreni coesivi (argille e argille limose). Le prove sono state svolte in data 23/02/2026 e 06/03/2026.

Il confronto delle tre prove penetrometriche mette in luce una discreta coerenza tra i risultati ottenuti dalle prove pur all'interno di una variabilità granulometrica tra percentuali di materiali fini coesivi e granulari.

Nelle Tabelle seguenti vengono descritte le suddivisioni in livelli stratigrafici del sottosuolo investigato e riportati i valori medi dei principali parametri geotecnici di ciascun livello riscontrato durante le prove penetrometriche statiche con piezocono. In Allegato 1 vengono riportati i certificati delle prove eseguite.

Il livello di falda rilevato durante le prove, all'interno del foro di infissione delle aste del penetrometro, si attesta a 0,80 m da p.c. nella SCPTU1 e 1,40 m dal p.c. nella CPTU2 e nella CPTU3. Tale misura risulta coerente con quella rilevata nel piezometro superficiale installato. Essa ovviamente può oscillare di diversi decimetri in concomitanza di fasi climatiche differenti.

Tabella 1: situazione stratigrafica e principali parametri geotecnici – SCPTU1 (prof. 30 m)

Strato	Profondità m da p.c.	Descrizione litostratigrafica	Natura	γ t/m³	Cu Kg/cm²	ϕ°	M (Eed) Kg/cm2
-	0 – 1,13	Prescavo	-	-	-	-	-
1	1,13 – 2,61	Terreno molto compatto a granulometria fine	Coesiva	1,9	1,97	-	45
2	2,61 – 3,68	Argille e argille limose	Coesiva	1,76	0,81	-	42
3	3,68 – 4,31	Limo sabbioso e sabbie limose	Granulare	1,76	-	36,1	55
4	4,31 – 6,36	Argille e argille limose	Coesiva	1,65	0,60	-	42
5	6,36 – 7,33	Sabbie e sabbie limose	Granulare	1,8	-	37,1	60
6	7,33 – 7,87	Sabbie e sabbie limose	Granulare	1,9	-	41,4	90
7	7,87 – 10,68	Argille	Coesiva	1,6	0,59	-	45
8	10,68 – 15,08	Sabbie e sabbie limose	Granulare	1,8	-	36,0	55
9	15,08 – 16,67	Argille	Coesiva	1,7	0,91	-	45
10	16,67 – 18,88	Sabbie e limi sabbiosi	Granulare	1,9	-	37,4	60
11	18,88 – 21,36	Limi sabbiosi e sabbie limose	Granulare	1,87	-	35,3	55
12	21,36 – 24,90	Argille e argille limose	Coesiva	1,83	1,66	-	45
13	24,90 – 26,96	Argille	Coesiva	1,8	1,39	-	45
14	26,96 – 27,96	Argille e argille limose	Coesiva	1,9	1,32	-	45
15	27,96 – 29,61	Sabbie e sabbie limose	Granulare	2,0	-	37,0	60
16	29,61 – 30,00	Argille	Coesiva	1,8	1,27	-	45

Tabella 2: situazione stratigrafica e principali parametri geotecnici – CPTU2 (prof. 20 m)

Strato	Profondità m da p.c.	Descrizione litostratigrafica	Natura	γ t/m³	Cu Kg/cm²	ϕ°	M (Eed) Kg/cm2
-	0 – 0,02	Terreno vegetale	-	-	-	-	-
1	0,02 – 1,04	Limo sabbioso e sabbie limose	Granulare	1,43	-	35	55
2	1,04 – 3,79	Argille e argille limose	Coesiva	1,84	1,3	-	45
3	3,79 – 4,51	Limo sabbioso e sabbie limose	Granulare	1,83	-	37	55
4	4,51 – 6,60	Argille e argille limose	Coesiva	1,62	0,56	-	42
5	6,60 – 7,86	Sabbie e sabbie limose	Granulare	1,87	-	40	90
6	7,86 – 8,39	Argille e argille limose	Coesiva	1,73	0,54	-	42

Strato	Profondità m da p.c.	Descrizione litostratigrafica	Natura	γ t/m³	Cu Kg/cm²	ϕ°	M (Eed) Kg/cm2
7	8,39 – 8,90	Sabbie e sabbie limose	Granulare	1,83	-	37	55
8	8,90 – 11,11	Argille	Coesiva	1,66	0,63	-	45
9	11,11 – 15,30	Sabbie e limi sabbiosi	Granulare	1,83	-	36	60
10	15,30 – 16,95	Argille e argille limose	Coesiva	1,72	0,8	-	42
11	16,95 – 18,61	Sabbie e limi sabbiosi	Granulare	1,95	-	38,5	65
12	18,61 – 19,57	Argille	Coesiva	1,78	1,0	-	45
13	19,57 – 20,00	Sabbie e limi sabbiosi	Granulare	1,87	-	35,4	60

Tabella 3: situazione stratigrafica e principali parametri geotecnici – CPTU3 (prof. 20 m)

Strato	Profondità m da p.c.	Descrizione litostratigrafica	Natura	γ t/m³	Cu Kg/cm²	ϕ°	M (Eed) Kg/cm2
-	0 – 0,02	Terreno vegetale	-	-	-	-	-
1	0,02 – 1,43	Argille e argille limose	Coesiva	1,69	0,6	-	42
2	1,43 – 2,43	Argille e argille limose	Coesiva	1,89	1,65	-	45
3	2,43 – 4,20	Sabbie limose e limi sabbiosi	Granulare	1,72	-	34,9	55
4	4,20 – 7,12	Argille e argille limose	Coesiva	1,65	0,59	-	42
5	7,12 – 7,67	Sabbie e sabbie limose	Granulare	1,85	-	38,8	65
6	7,67 – 10,63	Argille e argille limose	Coesiva	1,69	0,57	-	42
7	10,63 – 11,67	Sabbie limose e limi sabbiosi	Granulare	1,76	-	34,1	55
8	11,67– 15,03	Sabbie e limi sabbiosi	Granulare	1,85	-	36,4	60
9	15,03 – 16,58	Argille	Coesiva	1,68	0,63	-	42
10	16,58 – 18,40	Sabbie e limi sabbiosi	Granulare	1,90	-	37	65
11	18,40 – 19,72	Sabbie limose e limi sabbiosi	Granulare	1,86	-	35	55
12	19,72 – 20,00	Sabbie e limi sabbiosi	Granulare	1,89	-	35,9	55

Valutazione in merito al fenomeno della liquefazione

In riferimento agli effetti di instabilità cui sono sottoposti i terreni di fondazione se sottoposti ad una sollecitazione sismica, come da indicazioni delle NTC 2018 e stata valutata la stabilita del sito di costruzione nei confronti della liquefazione, fenomeno associato alla perdita di resistenza al taglio o ad accumulo di deformazioni plastiche in terreni saturi, prevalentemente sabbiosi, in seguito ad un significativo aumento istantaneo della pressione interstiziale dell'acqua presente nei vuoti intergranulari, che determina una fluidificazione del materiale con conseguenti potenziali effetti di instabilità nei confronti delle strutture di fondazione e delle strutture in elevazione.

Mediante l'utilizzo di un programma dedicato (CLiq – Geologismiki) sono stati ottenuti i diagrammi riportati in Allegato 2 relativi alle prove penetrometriche statiche con piezocono, dai quali si evince l'assenza di significativi livelli potenzialmente suscettibili alla liquefazione (si veda il grafico del potenziale di liquefazione LPI di seguito riportato in Figura 9).

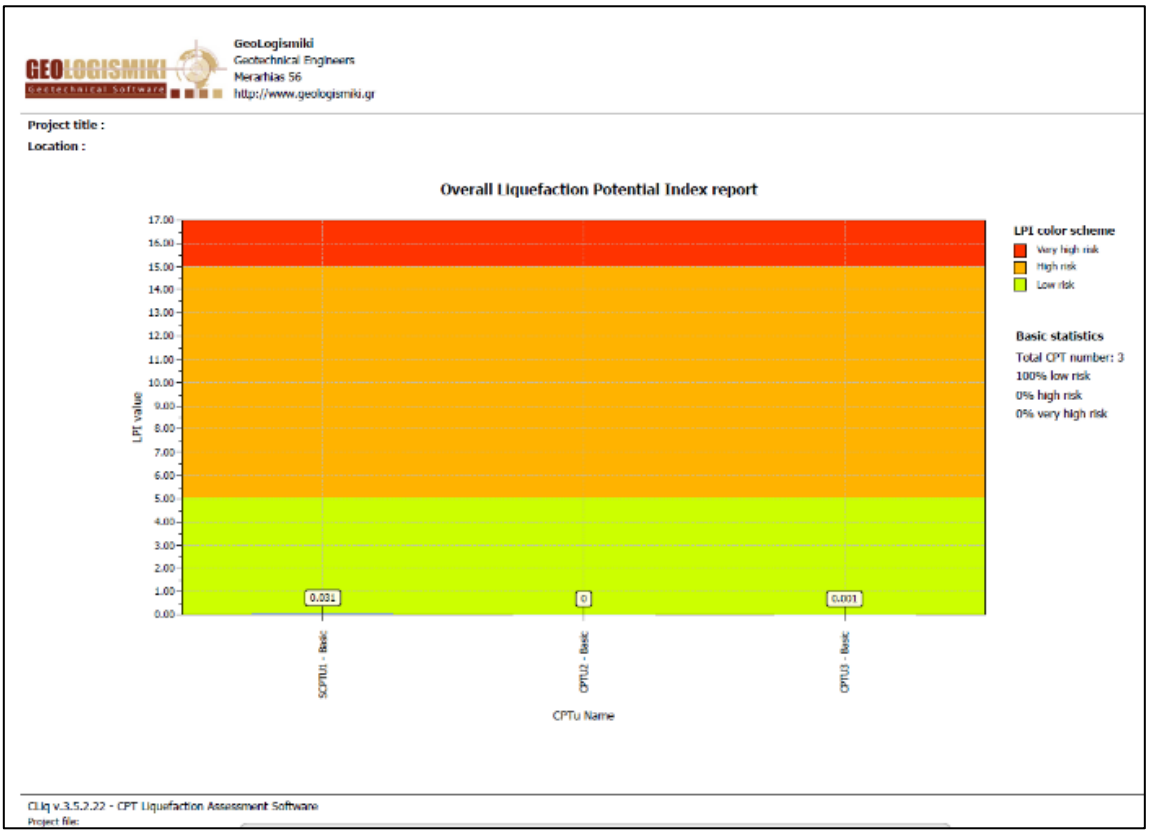


Figura 9: report verifica alla liquefazione

Sondaggio a carotaggio continuo

I terreni rilevati dall'osservazione delle cassette catalogatrici vede la generale alternanza tra terreni argillosi e limosi con limo sabbioso nel primo sottosuolo, fino a circa 3 m dal piano campagna.

Oltre i 3 metri di profondità sono maggiormente presenti sabbie e sabbie fini alternate a limi e limi sabbiosi. Si vedano le foto della cassetta porta campioni e la colonna stratigrafica da esse desunta in Allegato 3.

Prova Lefranc

Inoltre, durante l'esecuzione del sondaggio è stata eseguita una prova di permeabilità in foro di tipo Lefranc a carico variabile, in particolare la prova è stata eseguita tra -4 m e -4,50 m dal piano campagna, ovverosia all'interno dell'unico livello significativo di sabbie presente a profondità vicine a quelle di posa di eventuali "aghi" di impianti Well Point.

Durante le perforazioni sono state eseguite, sotto il livello della falda piezometrica, una prova di permeabilità tipo "Lefranc" a carico variabile, allo scopo di misurare la conducibilità idraulica orizzontale del terreno.

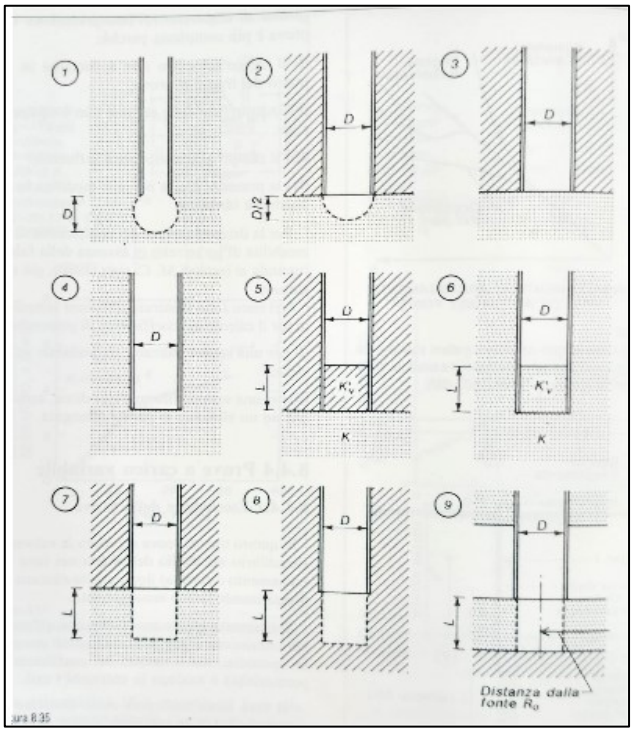
La prova Lefranc è stata preceduta dall'allestimento della tasca di prova, secondo le seguenti modalità esecutive:

- installazione del rivestimento nel foro fino al "tetto" della tasca di prova, avendo cura di approfondire gli ultimi 30 cm di rivestimento con modalità di avanzamento "a secco".
- perforazione con carotiere fino alla quota di prova;
- inserimento nella tasca di prova di ghiaia pulita fino a riempire l'intero spessore della tasca.

La metodologia utilizzata per la valutazione della permeabilità (K) fa riferimento a quella consigliata dalla Associazione Geotecnica Italiana (AGI) ed utilizza i seguenti schemi geometrici e relazioni di calcolo:

$$K = A/FT$$

- K=permeabilità (m/s)
- A= area del foro (m)
- F= fattore di forma (dipende dalla geometria della cavità realizzata durante la prova, si veda la Figura 10)
- T= tempo (s)



	GEOMETRIA DELLA CAVITÀ (RIF. FIG. 8.35)	VALORI DEL COEFFICIENTE DI FORMA DELLA CAVITÀ "F"
1	Filtro sferico in terreno uniforme	$2 \pi D$
2	Filtro emisferico al tetto di uno strato confinato	πD
3	Fondo filtrante piano al tetto di uno strato confinato	$2 D$
4	Fondo filtrante piano in terreno uniforme	$2{,}75 D$
5	Tubo parzialmente riempito al confine con uno strato permeabile	$\frac{2 D}{(1 + \frac{8}{\pi} \frac{L}{D} \frac{K_n}{K'_v})}$
6	Tubo parzialmente riempito in terreno uniforme	$\frac{2{,}75 D}{(1 + \frac{11}{\pi} \frac{L}{D} \frac{K_n}{K'_v})}$
7	Filtro cilindrico al confine con uno strato permeabile	$\frac{3 \pi L}{I_n (\frac{3L}{D} + \sqrt{1 + (\frac{3L}{D})^2})}$
8	Filtro cilindrico in terreno uniforme	$\frac{3 \pi L}{I_n [1{,}5 \frac{L}{D} + \sqrt{1 + (\frac{1{,}5 L}{D})^2}]}$
9	Filtro cilindrico attraversante uno strato confinato	$\frac{2 \pi L}{I_n (R_0/R)}$

Figura 10: geometrie per il calcolo del fattore di forma F

Il fattore di forma utilizzato per il calcolo della permeabilità è quello relativo alla formula n. 7 (filtro cilindrico al confine con uno strato permeabile), di seguito si riportano i risultati di permeabilità ottenuti.

T		H	DH	DT	k
misura	*s*	*m*	*m*	*s*	*m/s*
1	10	0,1	-	-	-
2	20	0,15	0,05	10	0,000850527
3	30	0,17	0,07	20	0,000425264
4	45	0,18	0,08	35	0,000243008
5	60	0,21	0,11	50	0,000170105
6	90	0,29	0,19	80	0,000106316
7	120	0,37	0,27	110	7,73207E-05
8	150	0,44	0,34	140	6,07519E-05
9	180	0,5	0,4	170	5,0031E-05
10	240	0,6	0,5	230	3,69794E-05
11	300	0,7	0,6	290	2,93285E-05
12	360	0,8	0,7	350	2,43008E-05
13	480	0,96	0,86	470	1,80963E-05
14	600	1,09	0,99	590	1,44157E-05
15	900	1,32	1,22	890	9,55649E-06

Il valore medio della permeabilità ottenuto durante la prova è di 1,5 E-4 m/s. I valori di permeabilità calcolati risultano corrispondere ai terreni rilevati (sabbie fini e sabbie limose).

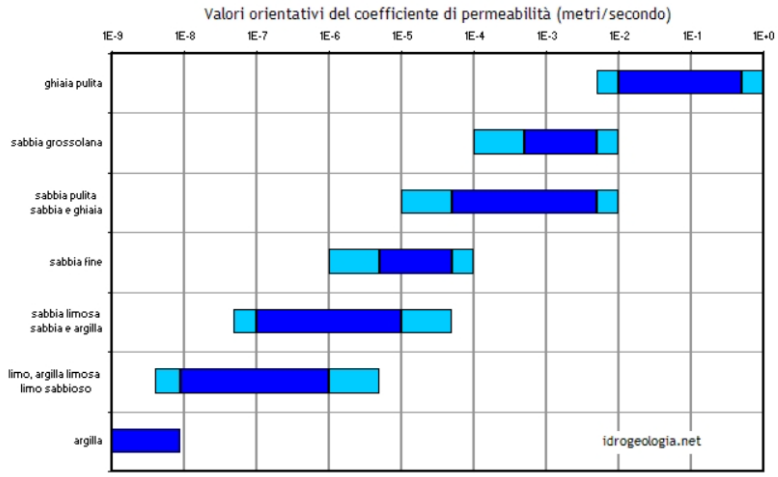


Figura 11: valori orientativi di permeabilità dei terreni

Analisi di laboratorio geotecnico

Sono stati prelevati n. 2 campioni geotecnici indisturbati durante la perforazione del sondaggio, entrambi i campioni sono stati consegnati al laboratorio geotecnico Geodata SRL di Ponte San Nicolò (PD). Le analisi geotecniche svolte sui n. 2 campioni indisturbati prelevati durante il sondaggio hanno visto le seguenti determinazioni geotecniche:

Tabella 4: campioni geotecnici prelevati dal sondaggio S1 (prof. 10 m)

Tipo di prova	**Sondaggio S1 (Area Ex Configliachi) Esecuzione sondaggio: 26/02/2026**	
Campione indisturbato	**CI1**	**CI2**
Profondità camp. (m da p.c.)	**3,20-3,80**	**6,00-6,50**
Classificazione geotecnica	limo con argilla grigio	limo con argilla grigio
Pocket Penetrometer	P.P. kPa 235-245	49-137
Torvane	Torv. KPa 60	22-33
Contenuto naturale d'acqua	W % 23,7	23,5
Massa volumica naturale	γ kN/m3 20,19	20,73
Massa volumica dei granuli solidi	γs kN/m 327,15	27,04
Limiti di Atterberg • WL • WP • IP	 38 22 16	 39 21 18
Analisi granulometrica % • Ciottoli • Ghiaia • Sabbia • Limo • Argilla	 0 0 1.16 68.52 30.32	 0 0 0.65 57.15 42.20
Classificazione UNI 11531-1 • Classe • Ig	 A6 10	 A6 11
Prova di compressione edometrica • σ kPa • cv m2/sec • kED m/sec	 100 9,38E-08 2,36E-10	 100 3,93E-08 1,25E-10
Prova di compressione edometrica • σ kPa • cv m2/sec • kED m/sec	 200 7,52E-08 1,10E-10	 200 6,86E-08 1,11E-10

7. VALUTAZIONE DELL'AZIONE SISMICA

Ai fini della definizione dell'azione sismica di progetto, secondo la normativa vigente, si rende necessario valutare l'effetto della risposta sismica locale mediante specifiche analisi, che nel caso specifico sono consistite nell'elaborazione delle velocità sismiche registrate durante la SCPTU spinta a 30 m di profondità oltre alla misura dell'amplificazione sismica con metodo HVSR (Tromino).

Il valore medio del parametro Vs30, determinato con l'elaborazione dei dati ottenuti con SCPTU è risultato pari a 226,91 m/s.

Dall'analisi dei risultati ottenuti dalle prove SCPTU, ai fini delle prescrizioni della vigente normativa in materia (O.P.C.M 3274/2003 e successive modifiche ed integrazioni e D.M. 17.01.2018) e alla luce di quanto sopra è possibile verificare come il suolo di fondazione del sito, oggetto di studio, vada a ricadere in categoria sismica C (vedi tabella che segue).

Tab. 3.2.II – *Categorie di sottosuolo che permettono l'utilizzo dell'approccio semplificato*

Categoria	Descrizione
A	*Ammassi rocciosi affioranti o terreni molto rigidi* caratterizzati da valori di velocità delle onde di taglio superiori a 800 m/s, eventualmente comprendenti in superficie terreni di caratteristiche meccaniche più scadenti con spessore massimo pari a 3 m.
B	*Rocce tenere e depositi di terreni a grana grossa molto addensati o terreni a grana fina molto consistenti,* caratterizzati da un miglioramento delle proprietà meccaniche con la profondità e da valori di velocità equivalente compresi tra 360 m/s e 800 m/s.
C	*Depositi di terreni a grana grossa mediamente addensati o terreni a grana fina mediamente consistenti* con profondità del substrato superiori a 30 m, caratterizzati da un miglioramento delle proprietà meccaniche con la profondità e da valori di velocità equivalente compresi tra 180 m/s e 360 m/s.
D	*Depositi di terreni a grana grossa scarsamente addensati o di terreni a grana fina scarsamente consistenti,* con profondità del substrato superiori a 30 m, caratterizzati da un miglioramento delle proprietà meccaniche con la profondità e da valori di velocità equivalente compresi tra 100 e 180 m/s.
E	*Terreni con caratteristiche e valori di velocità equivalente riconducibili a quelle definite per le categorie C o D,* con profondità del substrato non superiore a 30 m.

Dal punto di vista sismico il comune di Padova viene definito secondo il nuovo elenco dei comuni sismici del Veneto, approvato con deliberazione della Giunta Regionale n. 244 in data 9 marzo 2021 (BUR 38 del 16 marzo 2021) ed in vigore dal 15 maggio 2021, in zona sismica di classe più bassa ovverosia classe 3.

Sulla base delle mappe interattive dell'I.N.G.V., il valore di pericolosità sismica (secondo ordinanza PCM del 28 aprile 2006 n.3519, All. 1b) espresso in termini di accelerazione massima del suolo con probabilità di eccedenza del 10% in 50 anni riferita a suoli rigidi (Vs30>800 m/s cat. A) riferita al Comune è rappresentato da un valore di g compreso tra 0,075-0,100 vedi Figura 12.

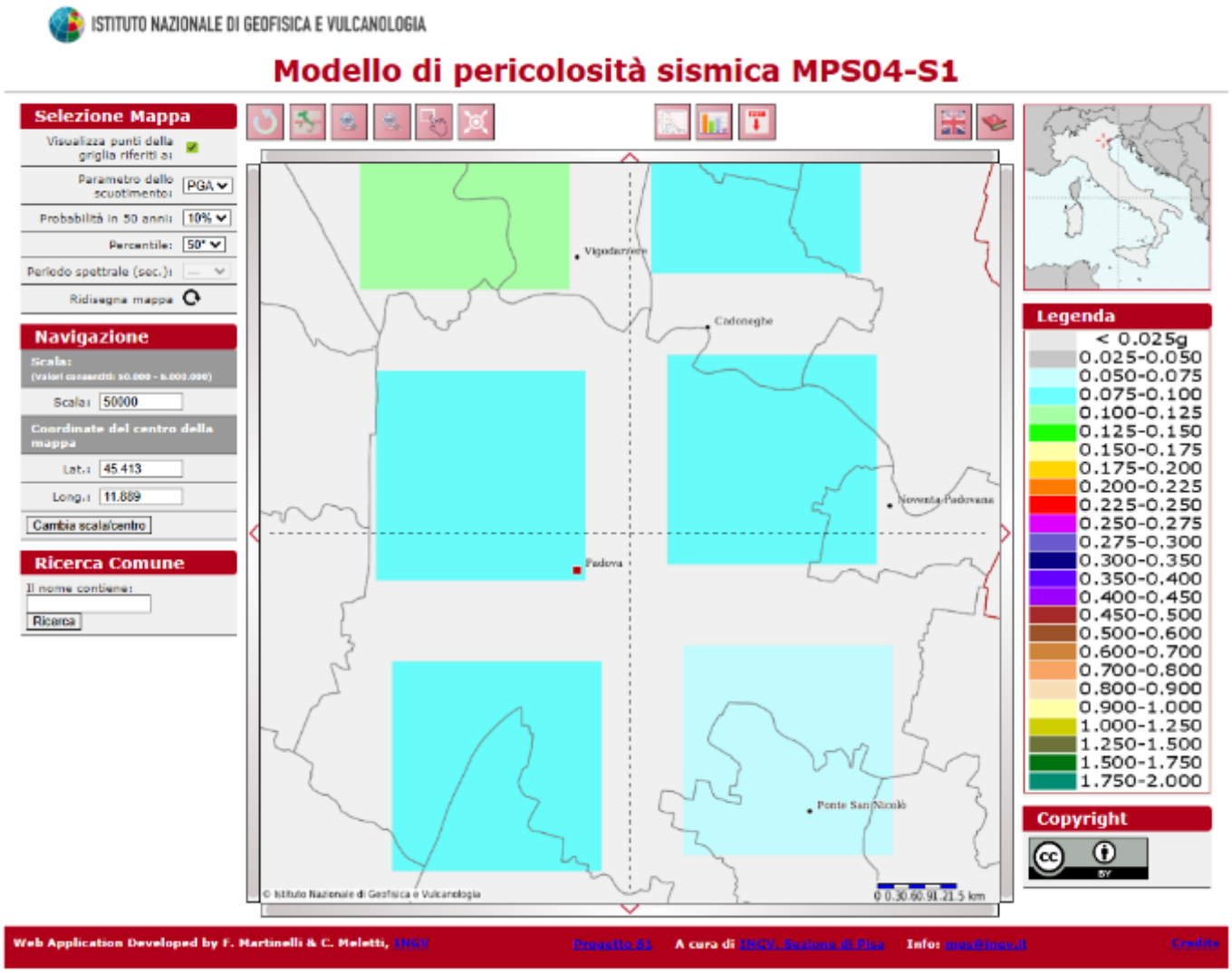


Figura 12: mappa di pericolosità sismica – particolare del comune di Padova

La tabella 1 dell'allegato B del D.M. 14/01/08 permette di stimare i parametri necessari per la definizione dell'azione sismica in progetto per il sito in esame, utilizzando come riferimento le informazioni disponibili nel reticolo di riferimento.

In relazione alla specificità dell'edificio ed alla sua classe d'uso, come previsto è stata redatta l'analisi Risposta Sismica Locale, essa viene proposta in Allegato 5.

I parametri sismici caratteristici del sito sono riportati nella pagina seguente.

Parametri sismici

Tipo di elaborazione: Stabilità dei pendii
Muro rigido: 0

Sito in esame.
latitudine: 45,413023
longitudine: 11,889178
Classe: 3
Vita nominale: 50

Siti di riferimento
Sito 1 ID: 12742 Lat: 45,4238 Lon: 11,8535 Distanza: 3032,698

Sito 2 ID: 12743 Lat: 45,4247 Lon: 11,9246 Distanza: 3052,047
Sito 3 ID: 12965 Lat: 45,3747 Lon: 11,9259 Distanza: 5134,392
Sito 4 ID: 12964 Lat: 45,3738 Lon: 11,8549 Distanza: 5121,291

Parametri sismici

Categoria sottosuolo: C
Categoria topografica: T1
Periodo di riferimento: 75anni
Coefficiente cu: 1,5

Operatività (SLO):
Probabilità di superamento: 81 %
Tr: 45 [anni]
ag: 0,035 g
Fo: 2,539
Tc*: 0,240 [s]

Danno (SLD):
Probabilità di superamento: 63 %
Tr: 75 [anni]
ag: 0,042 g
Fo: 2,533
Tc*: 0,278 [s]

Salvaguardia della vita (SLV):
Probabilità di superamento: 10 %
Tr: 712 [anni]
ag: 0,095 g
Fo: 2,621
Tc*: 0,345 [s]

Prevenzione dal collasso (SLC):
Probabilità di superamento: 5 %
Tr: 1462 [anni]
ag: 0,122 g
Fo: 2,610
Tc*: 0,358 [s]

Coefficienti Sismici Stabilità dei pendii

SLO:
Ss: 1,500
Cc: 1,680
St: 1,000
Kh: 0,011
Kv: 0,005
Amax: 0,520
Beta: 0,200

SLD:
Ss: 1,500
Cc: 1,600
St: 1,000
Kh: 0,013
Kv: 0,006
Amax: 0,624
Beta: 0,200

SLV:
Ss: 1,500
Cc: 1,490
St: 1,000
Kh: 0,029
Kv: 0,014
Amax: 1,403
Beta: 0,200

SLC:
Ss: 1,500
Cc: 1,470
St: 1,000
Kh: 0,044
Kv: 0,022
Amax: 1,789
Beta: 0,240

Le coordinate espresse in questo file sono in ED50
Geostru

Coordinate WGS84
latitudine: 45.412112
longitudine: 11.888182

8. CONCLUSIONI

I terreni di fondazione presenti nel sito oggetto di indagine verificano caratteristiche geotecniche discrete nei riguardi della qualità come terreni di fondazione, essi risultano infatti del tutto coerenti con quelli diffusi in zona, non verificando caratteristiche anomale rispetto ai terreni presenti nell'area vasta in cui ricade il progetto.

E' pertanto ipotizzabile l'utilizzo di fondazioni superficiali (se di tipo rigido secondo quanto di seguito specificato), ciò ovviamente se la tipologia di edificio da realizzare non necessiti di diversa soluzione.

Nell'area interessata dal sedime dell'edifico demolito sono presenti spessori variabili di materiale antropico residuo. Che dovranno ovviamente essere rimossi e correttamente smaltiti/riutilizzati.

Si segnala che, essendo prevista la realizzazione di un nuovo edificio parte su area vergine e parte su area di sedime del vecchio edificio demolito, in quest'ultima i terreni risulteranno preconsolidati a causa del carico imposto dall'edificio preesistente. A causa di questa situazione potrebbero verificarsi cedimenti differenziale che si esprimeranno però in parte già in fase di costruzione e potranno essere mitigati con fondazioni di tipo rigido.

La modesta profondità del livello di falda impone l'uso di impianti di tipo Well Poit nel caso si preveda lo scavo di locali interrati; come sempre sarà necessario impiegare tale dispositivo con cautela, deprimendo il livello di falda del minimo necessario per il minor tempo possibile, onde evitare cedimenti significativi nei terreni adiacenti. A tale proposito si consiglia di conservare il piezometro installato ed utilizzarlo per monitorare il livello di falda sotto emungimento.

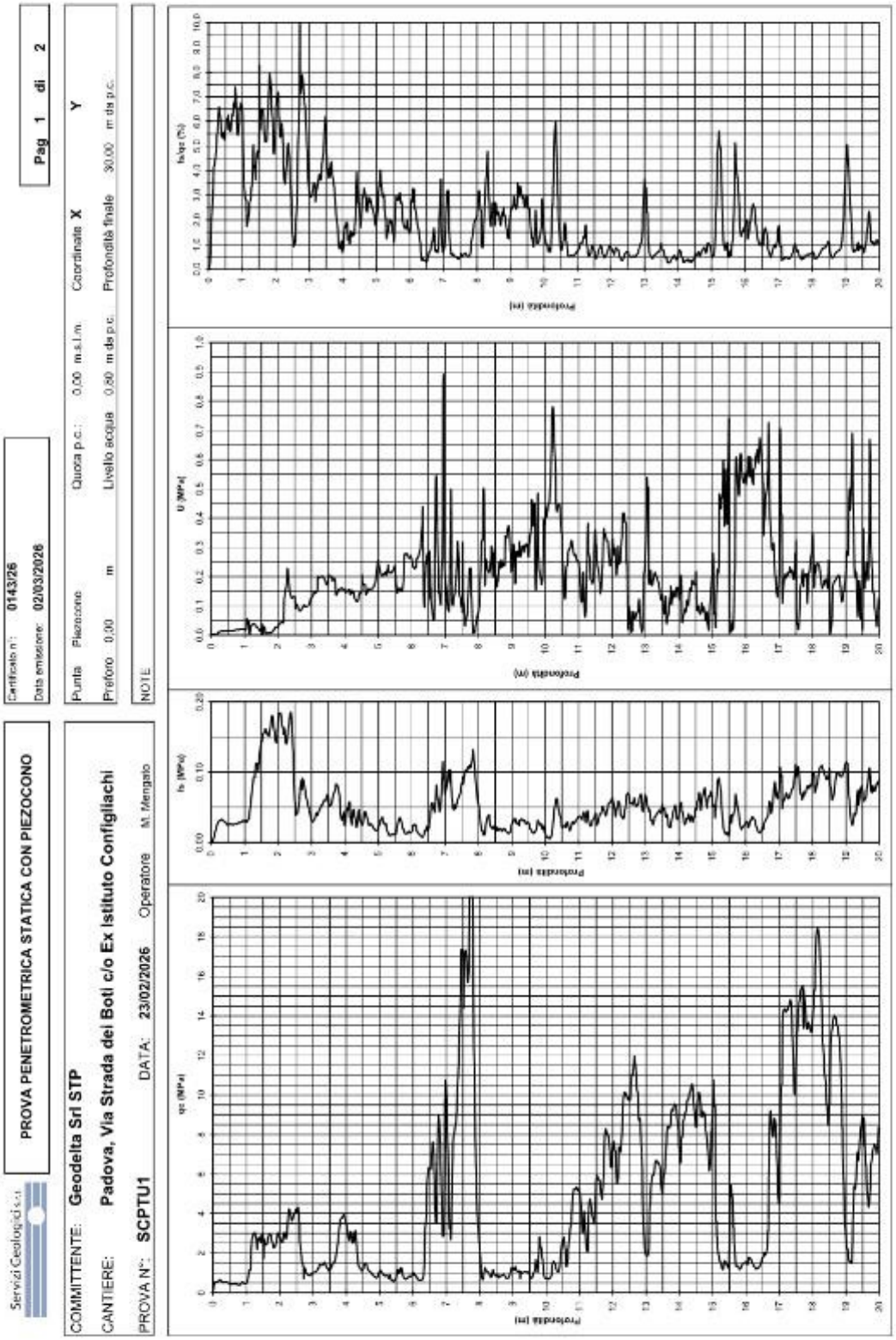
Limena, marzo 2026

Geol. Jacopo De Rossi



ALLEGATO 1: CPTU E SCPTU

SCPTU1


Servizi Geologici s.r.l.
PROVA PENETROMETRICA STATICA CON PIEZOCONO
Certificato n°: 0143/26
Data emissione: 02/03/2026
Pag 1 di 2
COMMITTENTE: Geodelta Srl STP
CANTIERE: Padova, Via Strada dei Boti c/o Ex Istituto Configliachi
PROVA N°: SCPTU1 DATA: 23/02/2026 Operatore M. Mengato
Punta Piezocono Quota p.c.: 0,00 m s.l.m. Coordinate X Y
Preforo 0,90 m Livello acqua 0,80 m da p.c. Profondità finale 30,00 m da p.c.
NOTE
qc (MPa)
fs (MPa)
u (MPa)
fs/qc (%)
Profondità (m)

Servizi Geologici s.r.l.

PROVA PENETROMETRICA STATICA MECCANICA CON PIEZOCONO

Certificato n°: **0143/26**
Data emissione: **02/03/2026**

COMMITTENTE: **Geodelta Srl STP**

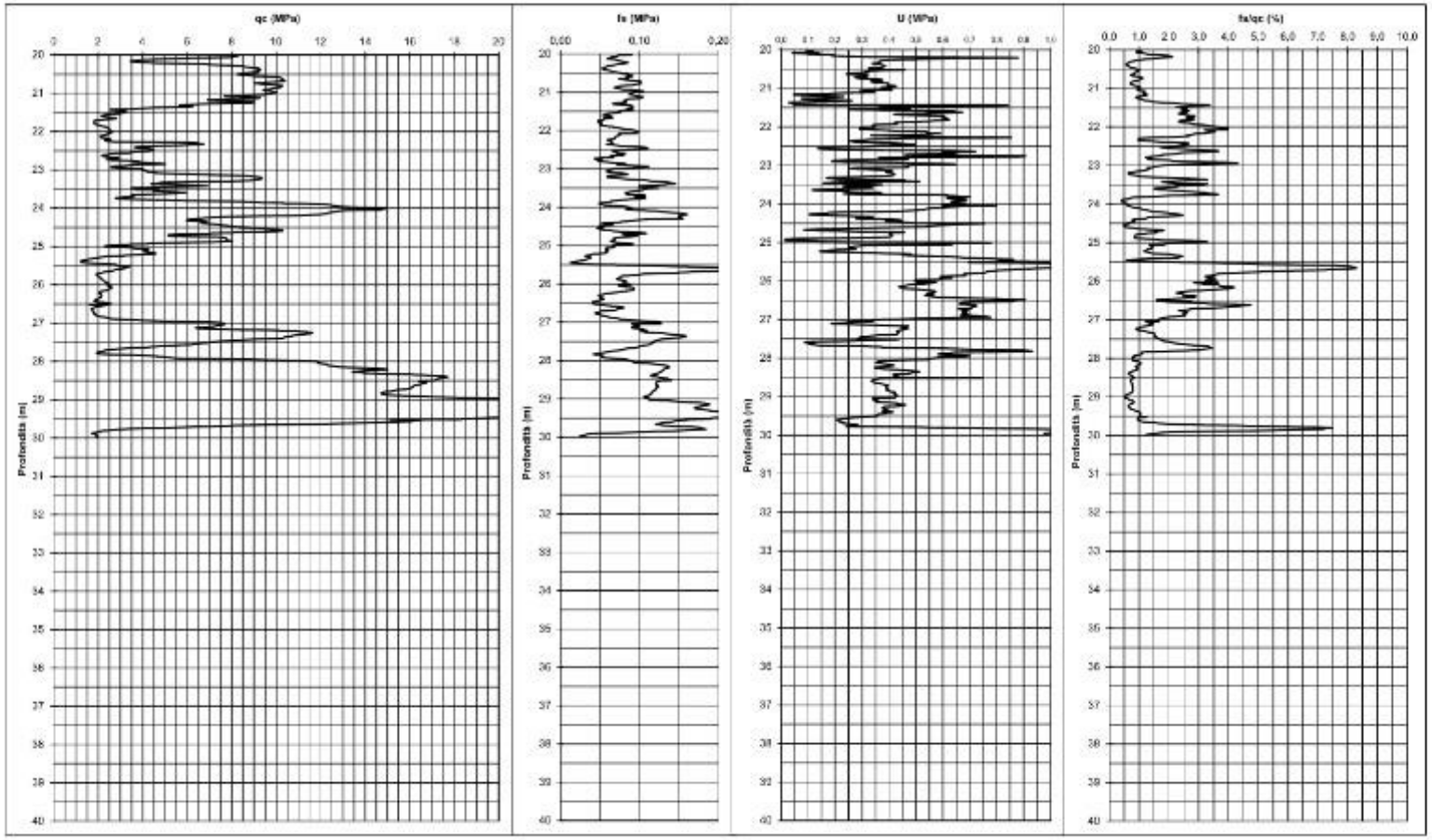
CANTIERE: **Padova, Via Strada dei Boti c/o Ex Istituto Configliachi**

PROVA N°: **SCPTU1** DATA: **23/02/2026** Operatore M. Mongato

Punta Piezocono Quota p.c.: 0,00 m.s.l.m. Coordinate X Y

Preforo 0,00 m Livello acqua 0,60 m da p.c. Profondità finale 30,00 m da p.c.

NOTE

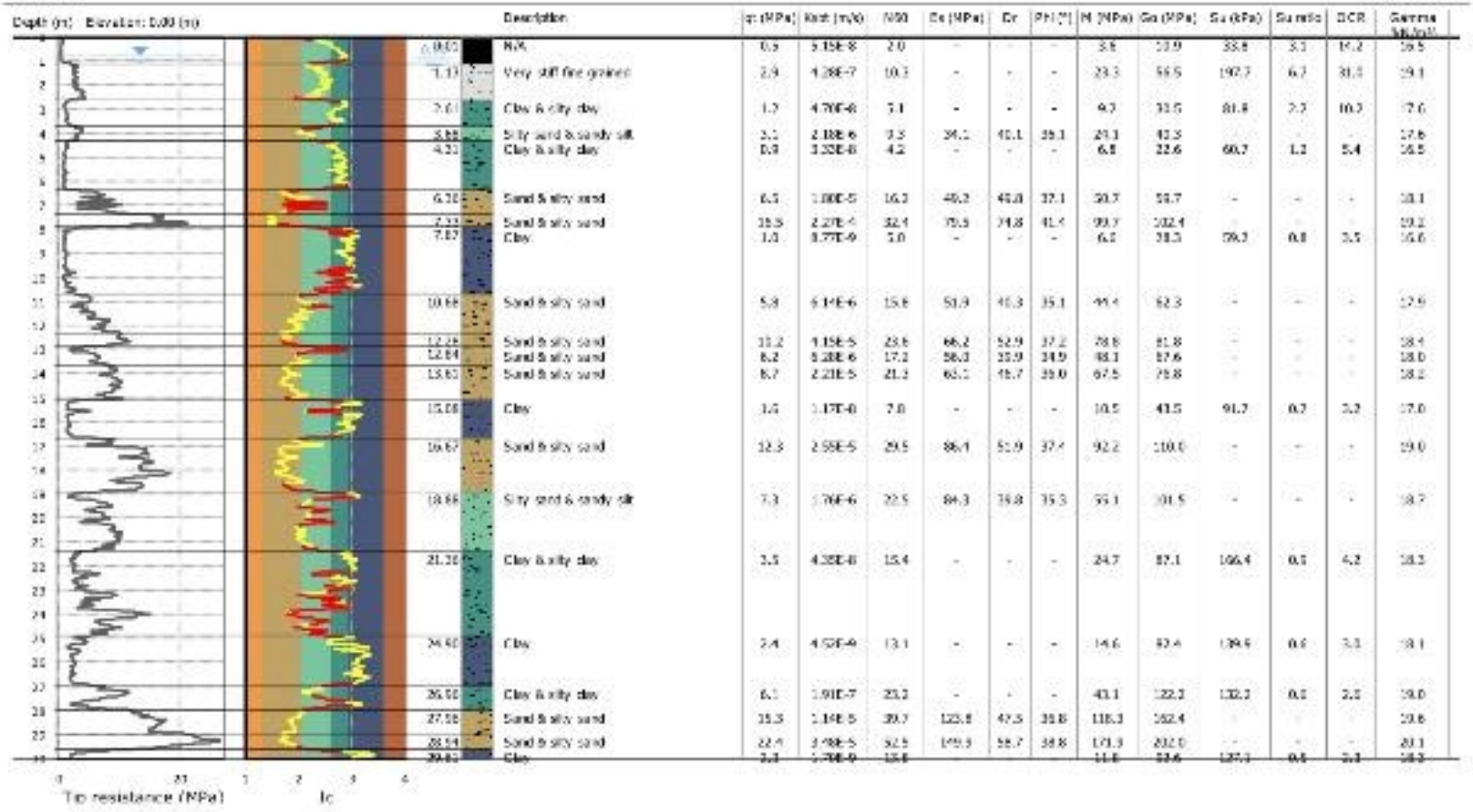


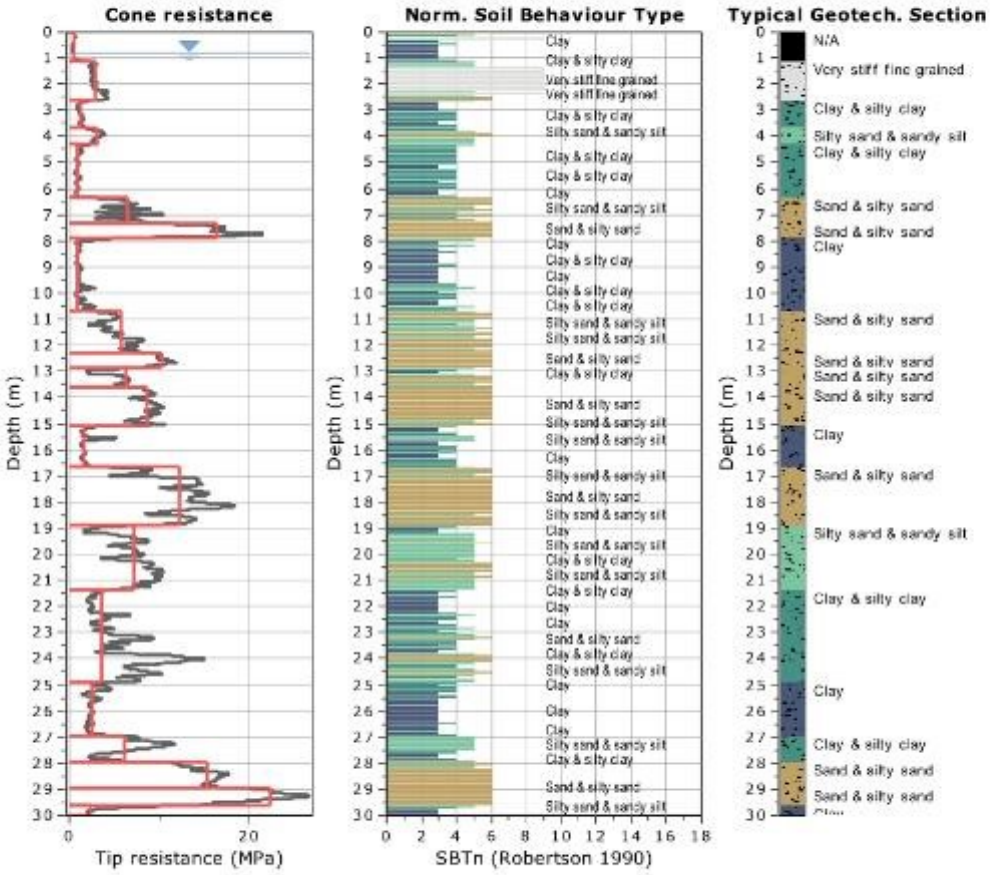
GeoLogismiki
Geotechnical Engineers
Marathon 56
http://www.geologismiki.gr

CPT: SCPTU1

Total depth: 30.00 m, Date: 06/03/2026
Surface Elevation: 0.00 m, Est. GWL: -0.80 m
Coords: X:0.00, Y:0.00
Cone Type:
Cone Operator:

Project:
Location:





Tabular results

.:: Layer No: 1 ::.

Code: Layer_1 **Start depth:** 0.01 (m), **End depth:** 1.13 (m)

Description: N/A

Basic results

Total cone resistance: 0.48 ±0.07 MPa
Sleeve friction: 0.00 ±27.95 kPa
Ic: 0.00 ±2.70
σ_v': 7.40 ±4.07 kPa
SBT_n: 0
SBT description: N/A
Schneider zone: Zone 3
Schneider desc.: Transitional soils

Estimation results

Permeability: 5.15E-08 ±1.26E-07 m/s
N_{60}: 1.98 ±0.11 blows
Es: 0.00 ±0.00 MPa
Dr (%): 0.00 ±0.00
φ (degrees): 0.00 ±0.00 °
Unit weight: 16.53 ±0.43 kN/m³
Constrained Mod.: 3.63 ±0.68 MPa
Go: 10.86 ±2.02 MPa
Su: 33.80 ±4.64 kPa
Su ratio: 3.07 ±1.45
O.C.R.: 14.19 ±6.68

.:: Layer No: 2 ::.

Code: Layer_2 **Start depth:** 1.13 (m), **End depth:** 2.61 (m)

Description: Very stiff fine grained

Basic results	Estimation results	
Total cone resistance: 2.95 ±0.58 MPa	Permeability: 4.28E-07 ±1.55E-06 m/s	Constrained Mod.: 23.33 ±4.61 MPa
Sleeve friction: 136.17 ±35.47 kPa	N_{60}: 10.31 ±1.54 blows	Go: 56.47 ±8.62 MPa
Ic: 2.40 ±0.14	Es: 0.00 ±0.00 MPa	Su: 197.73 ±30.90 kPa
σ_v': 21.61 ±3.70 kPa	Dr (%): 0.00 ±0.00	Su ratio: 6.72 ±0.48
SBT_n: 9	φ (degrees): 0.00 ±0.00 °	O.C.R.: 31.04 ±2.21
SBTn description: Very stiff fine grained	Unit weight: 19.06 ±0.35 kN/m³	
Schneider zone: Zone 2		
Schneider desc.: Essentially drained sands		

.:: Layer No: 3 ::.

Code: Layer_3 **Start depth:** 2.61 (m), **End depth:** 3.68 (m)

Description: Clay & silty clay

Basic results	Estimation results	
Total cone resistance: 1.20 ±0.22 MPa	Permeability: 4.70E-08 ±3.70E-08 m/s	Constrained Mod.: 9.16 ±1.70 MPa
Sleeve friction: 50.78 ±14.58 kPa	N_{60}: 5.13 ±0.85 blows	Go: 30.48 ±4.27 MPa
Ic: 2.72 ±0.11	Es: 0.00 ±0.00 MPa	Su: 81.75 ±15.18 kPa
σ_v': 33.35 ±2.03 kPa	Dr (%): 0.00 ±0.00	Su ratio: 2.21 ±0.27
SBT_n: 4	φ (degrees): 0.00 ±0.00 °	O.C.R.: 10.19 ±1.26
SBTn description: Clay & silty clay	Unit weight: 17.58 ±0.34 kN/m³	
Schneider zone: Zone 1a		
Schneider desc.: Silts and low Ir clays		

.:: Layer No: 4 ::.

Code: Layer_4 **Start depth:** 3.68 (m), **End depth:** 4.31 (m)

Description: Silty sand & sandy silt

Basic results	Estimation results	
Total cone resistance: 3.09 ±0.43 MPa	Permeability: 2.18E-06 ±2.15E-06 m/s	Constrained Mod.: 24.14 ±3.45 MPa
Sleeve friction: 38.84 ±9.69 kPa	N_{60}: 9.33 ±0.91 blows	Go: 40.30 ±3.54 MPa
Ic: 2.17 ±0.10	Es: 34.08 ±2.53 MPa	Su: 0.00 ±0.00 kPa
σ_v': 40.58 ±0.80 kPa	Dr (%): 40.14 ±2.45	Su ratio: 0.00 ±0.00
SBT_n: 5	φ (degrees): 36.09 ±0.65 °	O.C.R.: 0.00 ±0.00
SBTn description: Silty sand & sandy silt	Unit weight: 17.64 ±0.26 kN/m³	
Schneider zone: Zone 3		
Schneider desc.: Transitional soils		

.:: Layer No: 5 ::.

Code: Layer_5 **Start depth:** 4.31 (m), **End depth:** 6.36 (m)

Description: Clay & silty clay

Basic results	Estimation results	
Total cone resistance: 0.95 ±0.21 MPa	Permeability: 3.33E-08 ±3.47E-08 m/s	Constrained Mod.: 6.79 ±1.70 MPa
Sleeve friction: 20.88 ±8.77 kPa	N_{60}: 4.23 ±0.76 blows	Go: 22.55 ±4.39 MPa
Ic: 2.77 ±0.10	Es: 0.00 ±0.00 MPa	Su: 60.66 ±15.20 kPa
σ_v': 48.95 ±3.32 kPa	Dr (%): 0.00 ±0.00	Su ratio: 1.18 ±0.32
SBT_n: 4	φ (degrees): 0.00 ±0.00 °	O.C.R.: 5.44 ±1.49
SBTn description: Clay & silty clay	Unit weight: 16.46 ±0.51 kN/m³	
Schneider zone: Zone 1a		
Schneider desc.: Silts and low Ir clays		

.:: Layer No: 6 ::.

Code: Layer_6 **Start depth:** 6.36 (m), **End depth:** 7.33 (m)

Description: Sand & silty sand

Basic results	Estimation results	
Total cone resistance: 6.51 ±1.83 MPa	Permeability: 1.80E-05 ±2.49E-05 m/s	Constrained Mod.: 50.71 ±14.12 MPa
Sleeve friction: 45.11 ±16.38 kPa	N_{60}: 16.18 ±3.31 blows	Go: 59.66 ±10.42 MPa
Ic: 1.87 ±0.18	Es: 49.19 ±7.41 MPa	Su: 0.00 ±0.00 kPa
σ_v': 58.93 ±2.43 kPa	Dr (%): 49.85 ±6.20	Su ratio: 0.00 ±0.00
SBT_n: 6	φ (degrees): 37.12 ±1.08 °	O.C.R.: 0.00 ±0.00
SBTn description: Sand & silty sand	Unit weight: 18.09 ±0.48 kN/m³	
Schneider zone: N/A		
Schneider desc.: N/A		

.:: Layer No: 7 ::.

Code: Layer_7 **Start depth:** 7.33 (m), **End depth:** 7.87 (m)

Description: Sand & silty sand

Basic results	Estimation results	
Total cone resistance: 16.47 ±2.90 MPa	Permeability: 2.27E-04 ±1.09E-04 m/s	Constrained Mod.: 99.68 ±11.97 MPa
Sleeve friction: 86.72 ±19.73 kPa	N_{60}: 32.44 ±4.70 blows	Go: 102.38 ±13.96 MPa
Ic: 1.51 ±0.07	Es: 79.53 ±9.55 MPa	Su: 0.00 ±0.00 kPa
σ_v': 66.21 ±1.35 kPa	Dr (%): 74.82 ±6.18	Su ratio: 0.00 ±0.00
SBT_n: 6	φ (degrees): 41.41 ±1.18 °	O.C.R.: 0.00 ±0.00
SBTn description: Sand & silty sand	Unit weight: 19.20 ±0.34 kN/m³	
Schneider zone: N/A		
Schneider desc.: N/A		

.:: Layer No: 8 ::.

Code: Layer_8 **Start depth:** 7.87 (m), **End depth:** 10.68 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 0.99 ±0.16 MPa	Permeability: 8.77E-09 ±9.53E-09 m/s	Constrained Mod.: 6.61 ±1.25 MPa
Sleeve friction: 23.80 ±10.96 kPa	N_{60}: 4.96 ±0.83 blows	Go: 28.29 ±5.63 MPa
Ic: 2.96 ±0.09	Es: 0.00 ±0.00 MPa	Su: 59.19 ±10.95 kPa
σ_v': 77.10 ±3.80 kPa	Dr (%): 0.00 ±0.00	Su ratio: 0.77 ±0.13
SBT_n: 3	φ (degrees): 0.00 ±0.00 °	O.C.R.: 3.54 ±0.61
SBTn description: Clay	Unit weight: 16.63 ±0.46 kN/m³	
Schneider zone: Zone 1a		
Schneider desc.: Silts and low Ir clays		

.:: Layer No: 9 ::.

Code: Layer_9 **Start depth:** 10.68 (m), **End depth:** 12.28 (m)

Description: Sand & silty sand

Basic results	Estimation results	
Total cone resistance: 5.75 ±1.46 MPa	Permeability: 6.14E-06 ±7.57E-06 m/s	Constrained Mod.: 44.37 ±11.66 MPa
Sleeve friction: 40.07 ±10.78 kPa	N_{60}: 15.77 ±2.93 blows	Go: 62.33 ±9.69 MPa
Ic: 2.02 ±0.13	Es: 51.91 ±7.02 MPa	Su: 0.00 ±0.00 kPa
σ_v': 95.72 ±3.39 kPa	Dr (%): 40.32 ±4.92	Su ratio: 0.00 ±0.00
SBT_n: 6	φ (degrees): 35.09 ±0.98 °	O.C.R.: 0.00 ±0.00
SBTn description: Sand & silty sand	Unit weight: 17.91 ±0.37 kN/m³	
Schneider zone: Zone 3		
Schneider desc.: Transitional soils		

.:: Layer No: 10 ::.

Code: Layer_10 **Start depth:** 12.28 (m), **End depth:** 12.84 (m)

Description: Sand & silty sand

Basic results	Estimation results	
Total cone resistance: 10.21 ±0.76 MPa	Permeability: 4.15E-05 ±1.81E-05 m/s	Constrained Mod.: 78.78 ±5.74 MPa
Sleeve friction: 52.38 ±11.95 kPa	N_{60}: 23.56 ±1.53 blows	Go: 81.85 ±7.30 MPa
Ic: 1.75 ±0.06	Es: 66.21 ±4.96 MPa	Su: 0.00 ±0.00 kPa
σ_v': 102.74 ±0.97 kPa	Dr (%): 52.88 ±1.90	Su ratio: 0.00 ±0.00
SBT_n: 6	φ (degrees): 37.20 ±0.46 °	O.C.R.: 0.00 ±0.00
SBTn description: Sand & silty sand	Unit weight: 18.43 ±0.28 kN/m³	
Schneider zone: N/A		
Schneider desc.: N/A		

.:: Layer No: 11 ::.

Code: Layer_11 **Start depth:** 12.84 (m), **End depth:** 13.61 (m)

Description: Sand & silty sand

Basic results	Estimation results	
Total cone resistance: 6.25 ±0.62 MPa	Permeability: 6.28E-06 ±4.03E-06 m/s	Constrained Mod.: 48.08 ±4.96 MPa
Sleeve friction: 41.66 ±5.77 kPa	N_{60}: 17.15 ±1.01 blows	Go: 67.56 ±2.84 MPa
Ic: 2.02 ±0.09	Es: 56.02 ±1.95 MPa	Su: 0.00 ±0.00 kPa
σ_v': 110.76 ±0.91 kPa	Dr (%): 39.95 ±2.15	Su ratio: 0.00 ±0.00
SBT_n: 6	φ (degrees): 34.87 ±0.30 °	O.C.R.: 0.00 ±0.00
SBTn description: Sand & silty sand	Unit weight: 17.98 ±0.15 kN/m³	
Schneider zone: N/A		
Schneider desc.: N/A		

.:: Layer No: 12 ::.

Code: Layer_12 **Start depth:** 13.61 (m), **End depth:** 15.08 (m)

Description: Sand & silty sand

Basic results	Estimation results	
Total cone resistance: 8.75 ±1.04 MPa	Permeability: 2.21E-05 ±2.18E-05 m/s	Constrained Mod.: 67.49 ±7.80 MPa
Sleeve friction: 43.62 ±15.33 kPa	N_{60}: 21.34 ±1.70 blows	Go: 76.82 ±9.03 MPa
Ic: 1.84 ±0.12	Es: 63.07 ±6.12 MPa	Su: 0.00 ±0.00 kPa
σ_v': 117.98 ±3.41 kPa	Dr (%): 46.69 ±3.12	Su ratio: 0.00 ±0.00
SBT_n: 6	φ (degrees): 36.02 ±0.55 °	O.C.R.: 0.00 ±0.00
SBTn description: Sand & silty sand	Unit weight: 18.16 ±0.37 kN/m³	
Schneider zone: Zone 2		
Schneider desc.: Essentially drained sands		

.:: Layer No: 13 ::.

Code: Layer_13 **Start depth:** 15.08 (m), **End depth:** 16.67 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 1.60 ±0.50 MPa	Permeability: 1.17E-08 ±3.08E-07 m/s	Constrained Mod.: 10.49 ±4.04 MPa
Sleeve friction: 28.33 ±20.20 kPa	N_{60}: 7.82 ±1.28 blows	Go: 43.50 ±9.42 MPa
Ic: 2.92 ±0.18	Es: 0.00 ±0.00 MPa	Su: 91.73 ±13.98 kPa
σ_v': 130.82 ±3.01 kPa	Dr (%): 0.00 ±0.00	Su ratio: 0.70 ±0.11
SBT_n: 3	φ (degrees): 0.00 ±0.00 °	O.C.R.: 3.25 ±0.50
SBTn description: Clay	Unit weight: 17.02 ±0.60 kN/m³	
Schneider zone: Zone 1a		
Schneider desc.: Silts and low Ir clays		

.:: Layer No: 14 ::.

Code: Layer_14 **Start depth:** 16.67 (m), **End depth:** 18.88 (m)

Description: Sand & silty sand

Basic results	Estimation results	
Total cone resistance: 12.27 ±3.18 MPa	Permeability: 2.55E-05 ±4.39E-05 m/s	Constrained Mod.: 92.23 ±21.59 MPa
Sleeve friction: 79.39 ±16.32 kPa	N_{60}: 29.49 ±4.76 blows	Go: 110.00 ±11.88 MPa
Ic: 1.81 ±0.19	Es: 86.41 ±8.22 MPa	Su: 0.00 ±0.00 kPa
σ_v': 145.30 ±4.94 kPa	Dr (%): 51.94 ±7.60	Su ratio: 0.00 ±0.00
SBT_n: 6	φ (degrees): 37.44 ±1.05 °	O.C.R.: 0.00 ±0.00
SBTn description: Sand & silty sand	Unit weight: 18.98 ±0.26 kN/m³	
Schneider zone: Zone 2		
Schneider desc.: Essentially drained sands		

.:: Layer No: 15 ::.

Code: Layer_15 **Start depth:** 18.88 (m), **End depth:** 21.36 (m)

Description: Silty sand & sandy silt

Basic results	Estimation results	
Total cone resistance: 7.31 ±2.47 MPa	Permeability: 1.76E-06 ±3.36E-06 m/s	Constrained Mod.: 55.05 ±19.80 MPa
Sleeve friction: 76.62 ±17.76 kPa	N_{60}: 22.52 ±5.16 blows	Go: 101.52 ±16.49 MPa
Ic: 2.19 ±0.31	Es: 84.25 ±7.86 MPa	Su: 0.00 ±0.00 kPa
σ_v': 168.05 ±6.25 kPa	Dr (%): 39.78 ±3.10	Su ratio: 0.00 ±0.00
SBT_n: 5	φ (degrees): 35.30 ±0.61 °	O.C.R.: 0.00 ±0.00
SBTn description: Silty sand & sandy silt	Unit weight: 18.74 ±0.40 kN/m³	
Schneider zone: Zone 3		
Schneider desc.: Transitional soils		

.:: Layer No: 16 ::.

Code: Layer_16 **Start depth:** 21.36 (m), **End depth:** 24.90 (m)

Description: Clay & silty clay

Basic results	Estimation results	
Total cone resistance: 3.54 ±3.06 MPa	Permeability: 4.35E-08 ±6.56E-06 m/s	Constrained Mod.: 24.70 ±24.44 MPa
Sleeve friction: 68.94 ±18.30 kPa	N_{60}: 15.39 ±5.76 blows	Go: 87.06 ±15.25 MPa
Ic: 2.71 ±0.38	Es: 0.00 ±0.00 MPa	Su: 166.40 ±48.86 kPa
σ_v': 188.48 ±8.03 kPa	Dr (%): 0.00 ±0.00	Su ratio: 0.90 ±0.26
SBT_n: 4	φ (degrees): 0.00 ±0.00 °	O.C.R.: 4.17 ±1.20
SBTn description: Clay & silty clay	Unit weight: 18.34 ±0.35 kN/m³	
Schneider zone: N/A		
Schneider desc.: N/A		

.:: Layer No: 17 ::.

Code: Layer_17 **Start depth:** 24.90 (m), **End depth:** 26.96 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 2.44 ±0.72 MPa	Permeability: 4.52E-09 ±3.53E-08 m/s	Constrained Mod.: 14.63 ±6.55 MPa
Sleeve friction: 64.11 ±44.27 kPa	N_{60}: 13.11 ±2.34 blows	Go: 82.40 ±20.07 MPa
Ic: 3.05 ±0.20	Es: 0.00 ±0.00 MPa	Su: 139.93 ±52.02 kPa
σ_v': 217.99 ±4.64 kPa	Dr (%): 0.00 ±0.00	Su ratio: 0.64 ±0.26
SBT_n: 3	φ (degrees): 0.00 ±0.00 °	O.C.R.: 2.98 ±1.22
SBTn description: Clay	Unit weight: 18.12 ±0.63 kN/m³	
Schneider zone: Zone 1a		
Schneider desc.: Silts and low Ir clays		

.:: Layer No: 18 ::.

Code: Layer_18 **Start depth:** 26.96 (m), **End depth:** 27.96 (m)

Description: Clay & silty clay

Basic results	Estimation results	
Total cone resistance: 6.12 ±3.77 MPa	Permeability: 1.91E-07 ±1.66E-06 m/s	Constrained Mod.: 43.11 ±31.08 MPa
Sleeve friction: 97.39 ±28.79 kPa	N_{60}: 23.20 ±8.49 blows	Go: 122.18 ±29.30 MPa
Ic: 2.49 ±0.41	Es: 0.00 ±0.00 MPa	Su: 132.25 ±18.99 kPa
σ_v': 230.37 ±2.49 kPa	Dr (%): 0.00 ±0.00	Su ratio: 0.57 ±0.08
SBT_n: 4	φ (degrees): 0.00 ±0.00 °	O.C.R.: 2.61 ±0.38
SBTn description: Clay & silty clay	Unit weight: 18.95 ±0.56 kN/m³	
Schneider zone: Zone 3		
Schneider desc.: Transitional soils		

.:: Layer No: 19 ::.

Code: Layer_19 **Start depth:** 27.96 (m), **End depth:** 28.94 (m)

Description: Sand & silty sand

Basic results	Estimation results	
Total cone resistance: 15.30 ±1.65 MPa	Permeability: 1.14E-05 ±6.46E-06 m/s	Constrained Mod.: 118.30 ±13.16 MPa
Sleeve friction: 121.70 ±9.57 kPa	N_{60}: 39.71 ±2.53 blows	Go: 162.37 ±6.35 MPa
Ic: 1.94 ±0.08	Es: 123.79 ±4.21 MPa	Su: 0.00 ±0.00 kPa
σ_v': 240.88 ±2.61 kPa	Dr (%): 47.53 ±3.13	Su ratio: 0.00 ±0.00
SBT_n: 6	φ (degrees): 36.83 ±0.61 °	O.C.R.: 0.00 ±0.00
SBTn description: Sand & silty sand	Unit weight: 19.56 ±0.11 kN/m³	
Schneider zone: Zone 2		
Schneider desc.: Essentially drained sands		

.:: Layer No: 20 ::.

Code: Layer_20 **Start depth:** 28.94 (m), **End depth:** 29.61 (m)

Description: Sand & silty sand

Basic results	Estimation results	
Total cone resistance: 22.45 ±2.85 MPa	Permeability: 3.48E-05 ±2.48E-05 m/s	Constrained Mod.: 171.95 ±19.77 MPa
Sleeve friction: 170.63 ±35.27 kPa	N_{60}: 52.49 ±4.66 blows	Go: 201.98 ±20.26 MPa
Ic: 1.78 ±0.10	Es: 149.89 ±13.18 MPa	Su: 0.00 ±0.00 kPa
σ_v': 248.33 ±1.81 kPa	Dr (%): 58.71 ±4.68	Su ratio: 0.00 ±0.00
SBT_n: 6	φ (degrees): 38.78 ±0.70 °	O.C.R.: 0.00 ±0.00
SBTn description: Sand & silty sand	Unit weight: 20.09 ±0.27 kN/m³	
Schneider zone: Zone 2		
Schneider desc.: Essentially drained sands		

.:: Layer No: 21 ::.

Code: Layer_21 **Start depth:** 29.61 (m), **End depth:** 30.00 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 2.33 ±0.49 MPa	Permeability: 1.70E-09 ±2.13E-09 m/s	Constrained Mod.: 11.77 ±5.16 MPa
Sleeve friction: 75.27 ±68.32 kPa	N_{60}: 13.84 ±2.96 blows	Go: 92.57 ±32.31 MPa
Ic: 3.22 ±0.15	Es: 0.00 ±0.00 MPa	Su: 127.09 ±35.40 kPa
σ_v': 254.62 ±0.62 kPa	Dr (%): 0.00 ±0.00	Su ratio: 0.50 ±0.14
SBT_n: 3	φ (degrees): 0.00 ±0.00 °	O.C.R.: 2.31 ±0.65
SBTn description: Clay	Unit weight: 18.29 ±0.96 kN/m³	
Schneider zone: Zone 1a		
Schneider desc.: Silts and low Ir clays		

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_D (MPa)	D_r (%)	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_0 (MPa)	Undrained strength, S_u (kPa)	Unchained strength ratio	OCR	Unit weight (kN/m³)
0.01	1.12	5.15E-05	2.0	0.0	0.0	0.0	3.0	10.9	33.8	3.1	14.2	16.5
1.13		(±1.26E-07)	(±0.1)	(±0.0)	(±0.0)	(±0.0)	(±0.7)	(±2.5)	(±4.6)	(±1.4)	(±0.7)	(±0.4)
1.13	1.48	4.28E-07	10.3	0.0	0.0	0.0	23.3	56.5	192.7	6.7	31.0	19.1
2.61		(±1.33E-06)	(±1.5)	(±0.0)	(±0.0)	(±0.0)	(±4.6)	(±8.5)	(±30.9)	(±0.5)	(±2.2)	(±0.3)
2.61	1.07	4.70E-05	5.1	0.0	0.0	0.0	9.2	30.5	81.8	2.2	10.2	17.6
3.68		(±1.70E-08)	(±0.9)	(±0.0)	(±0.0)	(±0.0)	(±1.7)	(±4.1)	(±15.2)	(±0.3)	(±1.3)	(±0.3)
3.68	0.63	2.10E-05	9.3	34.1	40.1	36.1	24.1	40.3	0.0	0.0	0.0	17.6
4.31		(±2.15E-06)	(±0.3)	(±2.5)	(±2.4)	(±0.6)	(±3.5)	(±3.5)	(±0.0)	(±0.0)	(±0.0)	(±0.3)
4.31	2.05	3.33E-08	4.2	0.0	0.0	0.0	6.8	22.6	60.7	1.2	5.4	16.5
6.36		(±3.47E-08)	(±0.8)	(±0.0)	(±0.0)	(±0.0)	(±1.7)	(±4.1)	(±15.2)	(±0.3)	(±1.5)	(±0.5)
6.36	0.97	1.80E-05	16.2	49.2	49.8	37.1	50.7	93.7	0.0	0.0	0.0	18.1
7.33		(±2.49E-05)	(±1.3)	(±7.4)	(±7.2)	(±1.1)	(±14.1)	(±19.4)	(±0.0)	(±0.0)	(±0.0)	(±0.5)
7.33	0.54	2.27E-04	32.4	79.5	74.8	41.4	99.7	102.4	0.0	0.0	0.0	19.2
7.87		(±1.09E-04)	(±4.7)	(±9.6)	(±8.2)	(±1.2)	(±12.1)	(±14.0)	(±0.0)	(±0.0)	(±0.0)	(±0.3)
7.87	2.81	8.77E-09	5.0	0.0	0.0	0.0	6.6	28.3	59.2	0.8	3.5	16.6
10.68		(±5.53E-09)	(±0.8)	(±0.0)	(±0.0)	(±0.0)	(±1.2)	(±5.5)	(±10.5)	(±0.1)	(±0.6)	(±0.5)
10.68	1.80	6.14E-06	15.8	51.9	40.3	35.1	111.1	62.3	0.0	0.0	0.0	17.9
12.28		(±7.32E-06)	(±7.9)	(±7.0)	(±4.9)	(±1.0)	(±11.7)	(±9.7)	(±0.0)	(±0.0)	(±0.0)	(±0.4)
12.28	0.56	4.15E-05	23.0	66.2	52.9	37.2	78.8	81.8	0.0	0.0	0.0	18.4
12.84		(±1.81E-05)	(±1.5)	(±5.0)	(±1.9)	(±0.5)	(±5.7)	(±7.3)	(±0.0)	(±0.0)	(±0.0)	(±0.3)
12.84	0.77	6.28E-05	17.2	56.0	39.8	34.9	48.1	67.6	0.0	0.0	0.0	18.0
13.61		(±1.03E-06)	(±1.3)	(±2.0)	(±2.1)	(±0.3)	(±5.0)	(±2.8)	(±0.0)	(±0.0)	(±0.0)	(±0.1)
13.61	1.47	2.21E-05	21.3	63.1	46.7	36.0	67.5	76.8	0.0	0.0	0.0	18.2
15.08		(±2.10E-05)	(±1.7)	(±6.1)	(±3.1)	(±0.5)	(±7.0)	(±9.1)	(±0.0)	(±0.0)	(±0.0)	(±0.4)

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CPT: SCPTU1
Total depth: 30.00 m, Date: 06/03/2026
Surface Elevation: 0.00 m, Est. GWL: 0.80 m
Coords: X:0.00, Y:0.00
Cone Type:
Cone Operator:

Project:
Location:

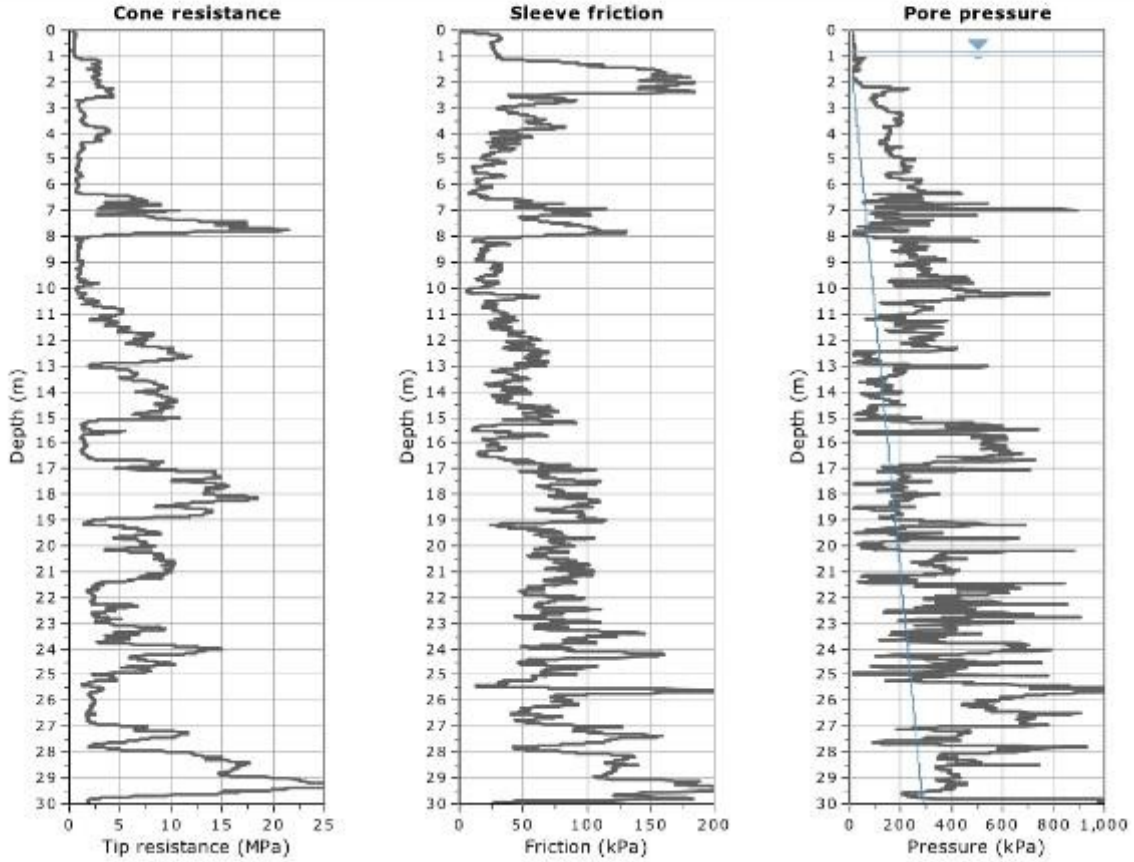
Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_D (MPa)	D_r (%)	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_0 (MPa)	Undrained strength, S_u (kPa)	Unchained strength ratio	OCR	Unit weight (kN/m³)
15.08	1.59	1.17E-05	7.8	0.0	0.0	0.0	10.5	43.5	91.7	0.7	3.2	17.0
16.67		(±3.08E-07)	(±1.3)	(±0.0)	(±0.0)	(±0.0)	(±4.0)	(±9.4)	(±14.2)	(±0.1)	(±0.5)	(±0.6)
16.67	2.21	2.55E-05	26.5	86.4	51.9	37.4	92.2	110.0	0.0	0.0	0.0	19.0
18.88		(±4.39E-05)	(±4.8)	(±8.2)	(±7.6)	(±1.1)	(±21.6)	(±11.9)	(±0.0)	(±0.0)	(±0.0)	(±0.3)
18.88	3.48	1.76E-05	22.5	84.3	39.8	35.3	55.1	101.5	0.0	0.0	0.0	18.7
21.36		(±1.30E-06)	(±5.7)	(±7.9)	(±3.1)	(±0.5)	(±19.8)	(±10.5)	(±0.0)	(±0.0)	(±0.0)	(±0.4)
21.36	3.54	4.35E-08	15.4	0.0	0.0	0.0	24.7	87.1	165.4	0.9	4.2	18.3
24.90		(±6.36E-06)	(±5.8)	(±0.0)	(±0.0)	(±0.0)	(±29.4)	(±15.2)	(±48.1)	(±0.3)	(±1.2)	(±0.4)
24.90	2.06	4.52E-09	13.1	0.0	0.0	0.0	14.6	82.4	130.9	0.6	3.0	18.1
26.96		(±3.33E-08)	(±2.3)	(±0.0)	(±0.0)	(±0.0)	(±45.5)	(±21.1)	(±52.0)	(±0.2)	(±1.2)	(±0.6)
26.96	1.00	1.91E-07	23.2	0.0	0.0	0.0	43.1	122.2	132.2	0.6	2.6	19.0
27.96		(±1.03E-06)	(±6.5)	(±0.0)	(±0.0)	(±0.0)	(±31.1)	(±29.3)	(±49.2)	(±0.1)	(±0.4)	(±0.6)
27.96	0.98	1.14E-05	39.7	123.8	47.5	36.8	118.3	102.4	0.0	0.0	0.0	19.6
28.94		(±6.46E-06)	(±2.5)	(±4.2)	(±3.1)	(±0.6)	(±13.2)	(±6.4)	(±0.0)	(±0.0)	(±0.0)	(±0.1)
28.94	0.67	3.48E-05	52.5	140.9	58.7	38.8	171.9	202.0	0.0	0.0	0.0	20.1
29.61		(±2.48E-05)	(±1.7)	(±13.2)	(±1.7)	(±0.7)	(±19.8)	(±21.3)	(±0.0)	(±0.0)	(±0.0)	(±0.3)
29.61	0.39	1.70E-09	13.8	0.0	0.0	0.0	11.8	92.6	127.1	0.5	2.3	18.3
30.00		(±7.13E-09)	(±3.0)	(±0.0)	(±0.0)	(±0.0)	(±5.2)	(±17.3)	(±35.4)	(±0.1)	(±0.6)	(±1.0)

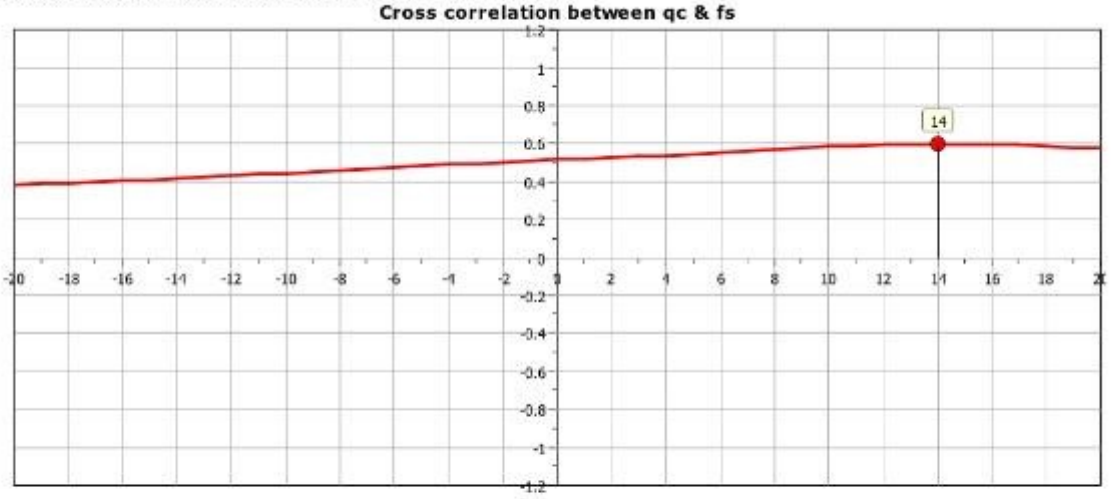
Depth values presented in this table are measured from free ground surface

CPT: SCPTU1
Total depth: 30.00 m, Date: 06/03/2026
Surface Elevation: 0.00 m, Est. GWL: 0.80 m
Coords: X:0.00, Y:0.00
Cone Type:
Cone Operator:

Project:
Location:



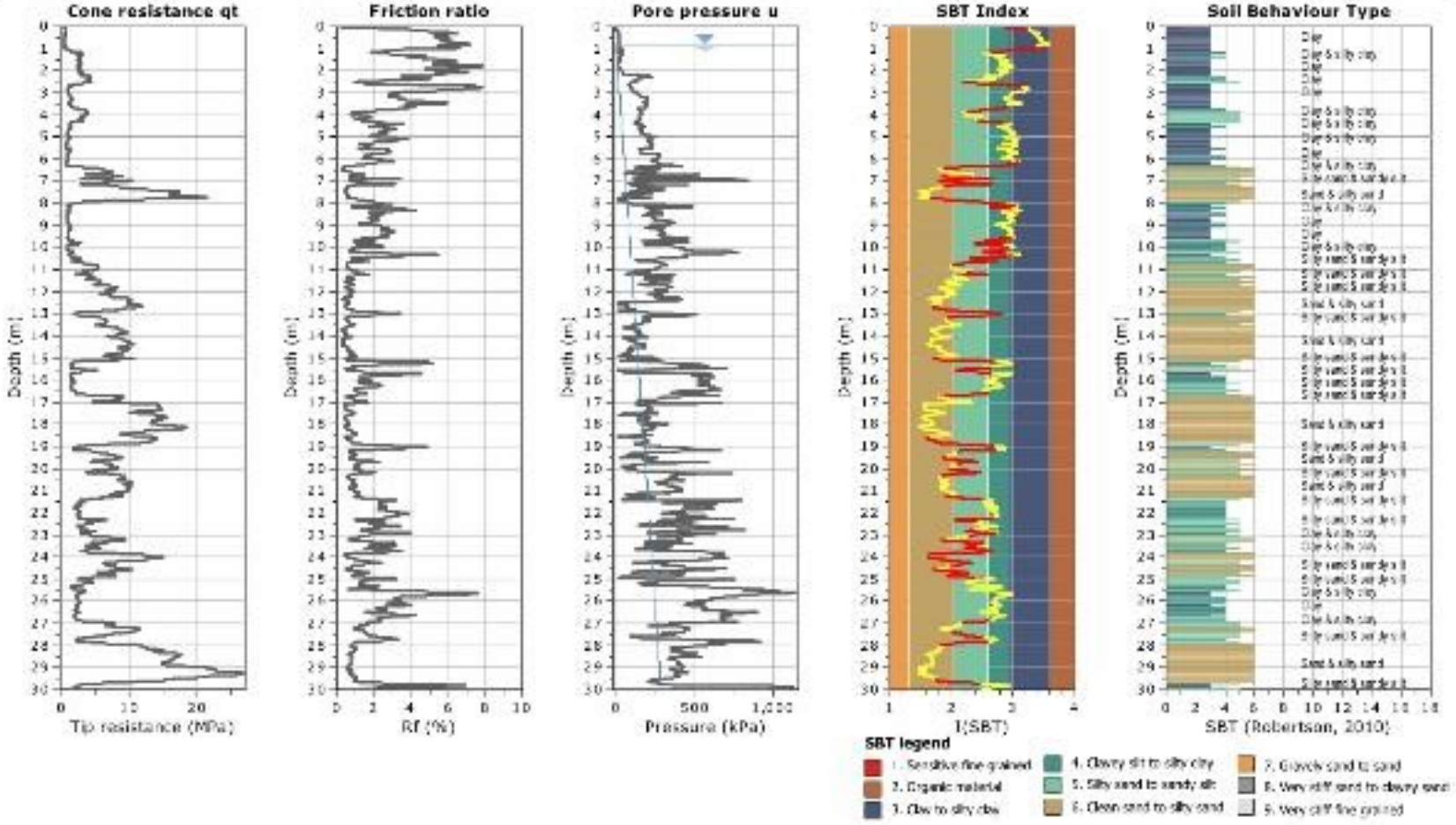
The plot below presents the cross correlation coeficient between the raw qc and fs values (as measured on the field). X axes presents the lag distance (one lag is the distance between two sucessive CPT measurements).



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Project:
Location:

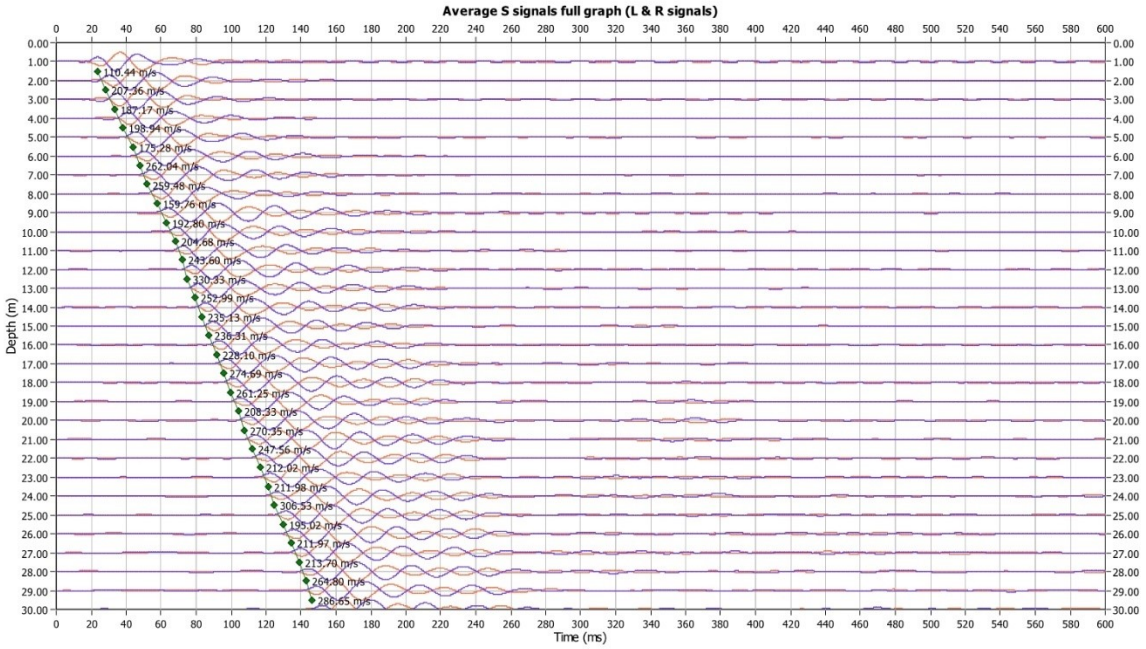
CPT: SCPTU1
Total depth: 30.00 m, Date: 06/03/2026
Surface Elevation: 0.00 m, Est. GWL: 0.80 m
Coords: X:0.00, Y:0.00
Cone Type:
Cone Operator:



ANALISI SISMICA OTTENUTA DA SCPTU1

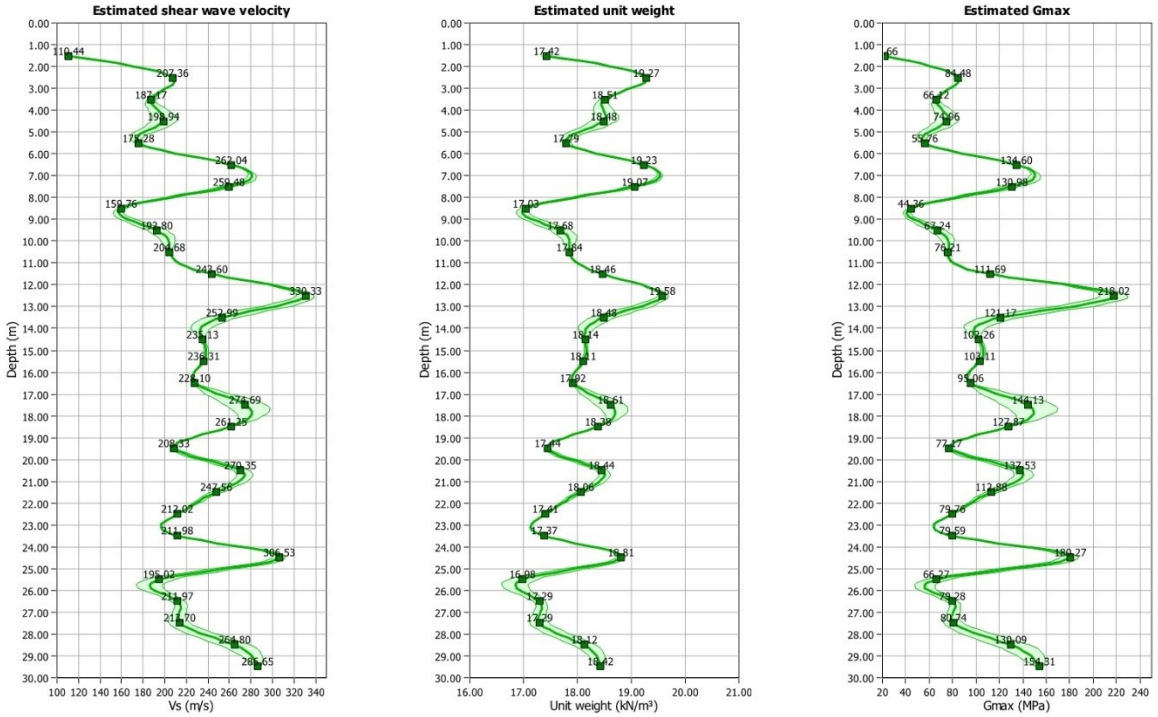
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Project: **Borehole ID: SCPTU1**



This software is licensed to: Servizi Geologici Sas di Morbin Francesco & C.

Detailed result plots over depth



Servizi Geologici s.r.l.

PROVA PENETROMETRICA STATICA CON PIEZOCONO

Certificato n°: 0144/26
Data emissione: 02/03/2026

COMMITTENTE: **Geodelta Srl STP**

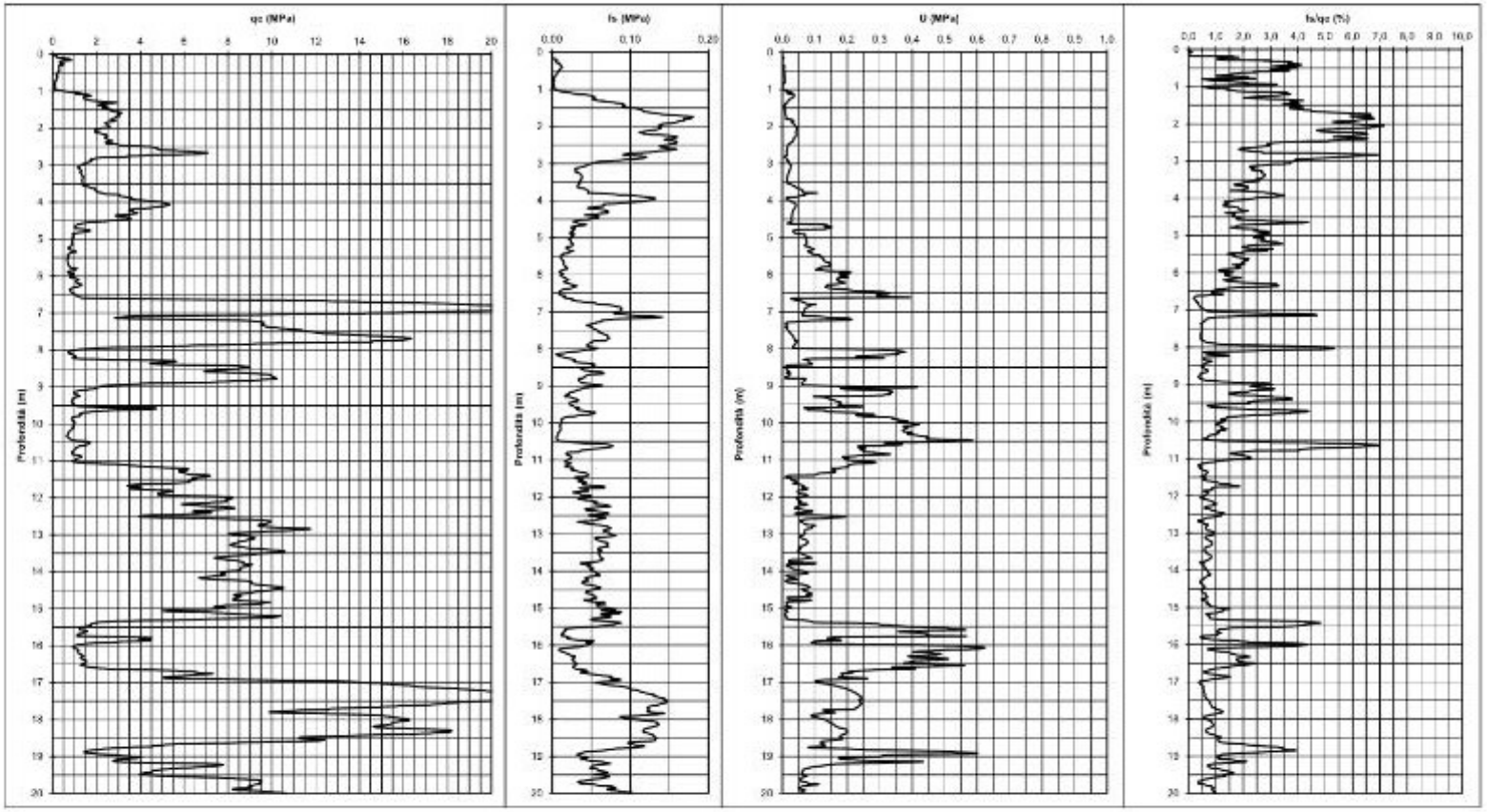
CANTIERE: **Padova, Via Strada dei Boti c/o Ex Istituto Configliachi**

PROVA N°: **CPTU2** DATA: **23/02/2026** Operatore M. Mengato

Punta Piezocono Quota p.c.: 0,00 m.s.l.m. Coordinate X Y

Preforo 0,00 m Livello acqua n.r. m da p.c. Profondità finale 20,00 m da p.c.

NOTE



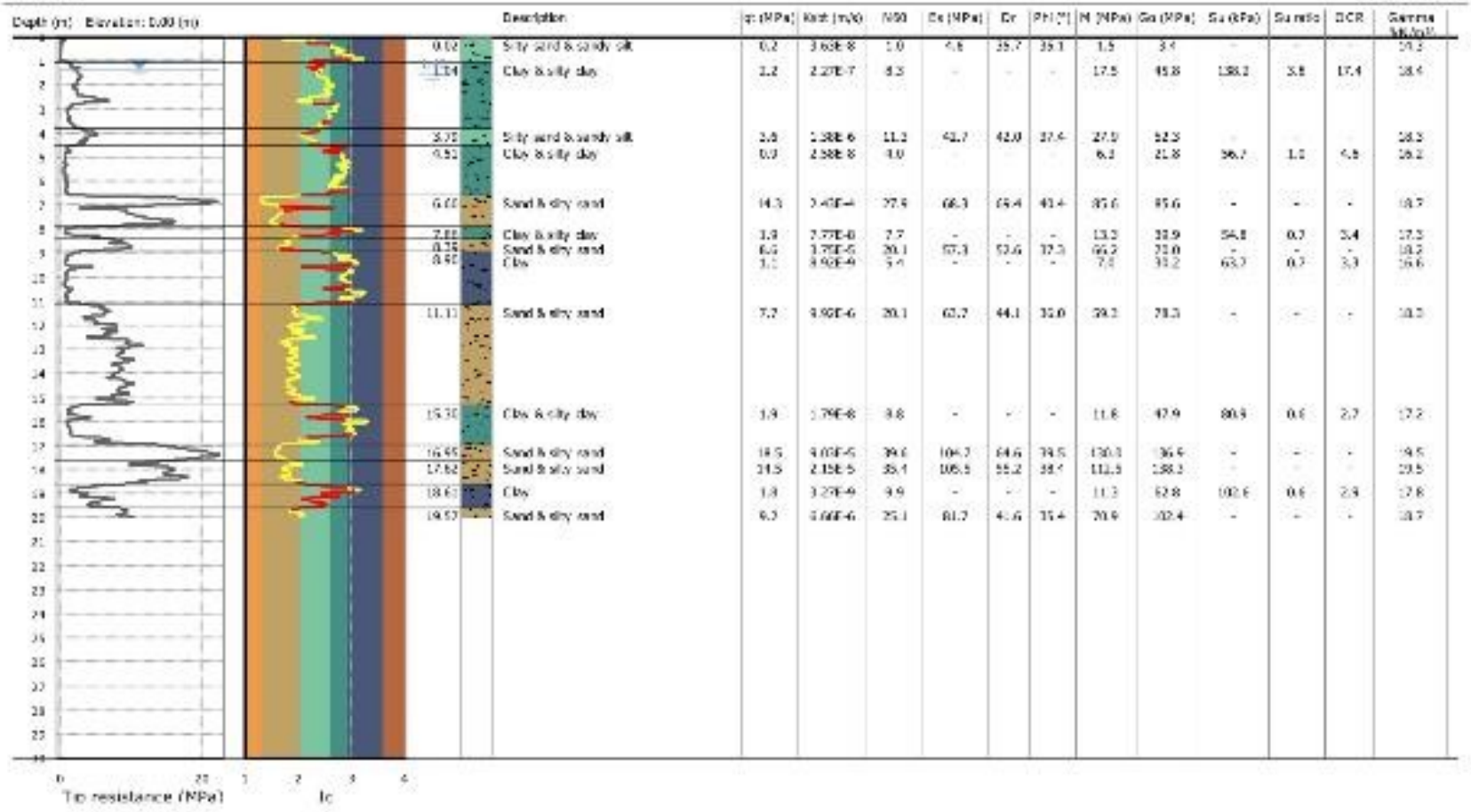
CPTU2

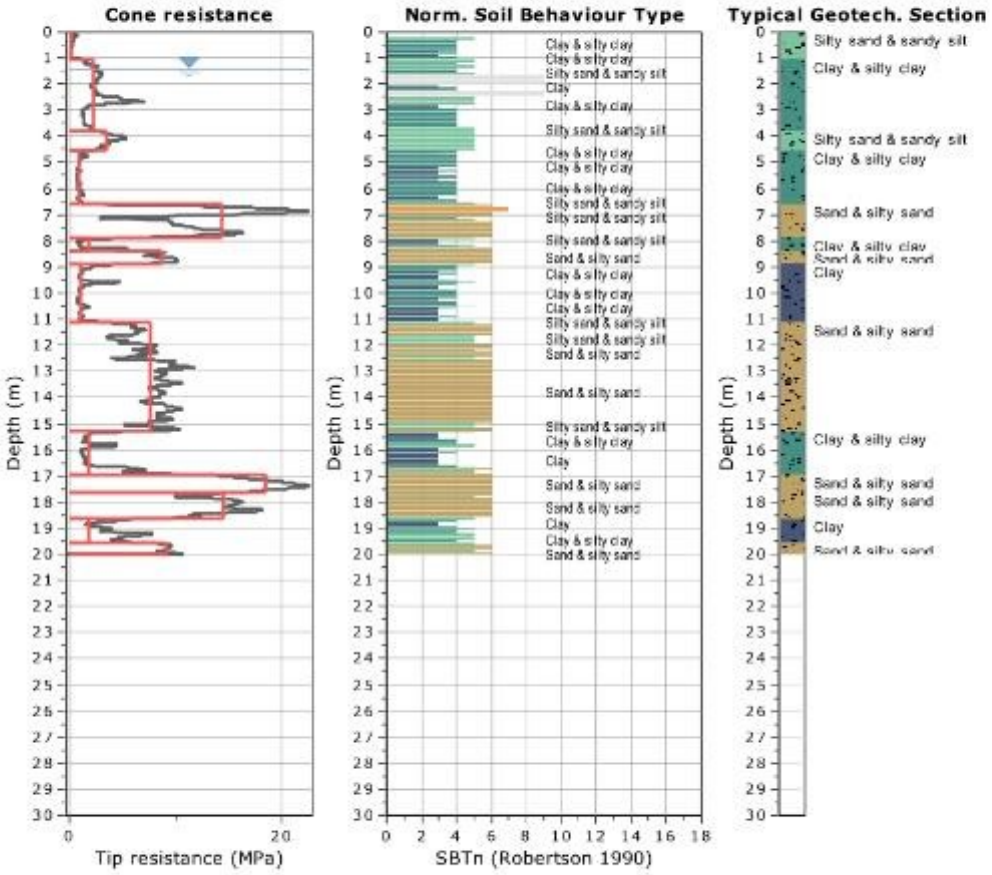
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CPT: CPTU2

Total depth: 20.00 m, Date: 06/03/2026
Surface Elevation: 0.00 m, Est. GWL: 1.40 m
Coords: X:0.00, Y:0.00
Cone Type:
Cone Operator:

Project:
Location:





Tabular results

.:: Layer No: 1 ::.

Code: Layer_1 **Start depth:** 0.02 (m), **End depth:** 1.04 (m)

Description: Silty sand & sandy silt

Basic results

Total cone resistance: 0.21 ±0.16 MPa
Sleeve friction: 0.00 ±5.57 kPa
Ic: 0.00 ±2.63
σ_v': 5.77 +4.41 kPa
SBT_n: 5
SBTn description: Silty sand & sandy silt
Schneider zone: Zone 3
Schneider desc.: Transitional soils

Estimation results

Permeability: 3.63E-08 ±1.18E-06 m/s
N_{60}: 1.04 ±0.23 blows
Es: 4.58 ±0.28 MPa
Dr (%): 35.66 +0.52
φ (degrees): 35.07 ±1.01 °
Unit weight: 14.30 ±0.94 kN/m³

Constrained Mod.: 1.46 ±1.40 MPa
Go: 3.43 ±1.52 MPa
Su: 0.00 ±0.00 kPa
Su ratio: 0.00 +0.00
O.C.R.: 0.00 ±0.00

.:: Layer No: 2 ::.

Code: Layer_2 **Start depth:** 1.04 (m), **End depth:** 3.79 (m)

Description: Clay & silty clay

Basic results	Estimation results	
Total cone resistance: 2.24 ±1.31 MPa	Permeability: 2.27E-07 ±1.28E-06 m/s	Constrained Mod.: 17.50 ±10.53 MPa
Sleeve friction: 83.91 ±54.22 kPa	N_{60}: 8.30 ±3.52 blows	Go: 45.81 ±16.93 MPa
Ic: 2.49 ±0.17	Es: 0.00 ±0.00 MPa	Su: 138.21 ±46.25 kPa
σ_v': 30.72 ±6.34 kPa	Dr (%): 0.00 ±0.00	Su ratio: 3.77 ±1.68
SBT_n: 4	φ (degrees): 0.00 ±0.00 °	O.C.R.: 17.41 ±7.75
SBTn description: Clay & silty clay	Unit weight: 18.39 ±0.89 kN/m³	
Schneider zone: Zone 2		
Schneider desc.: Essentially drained sands		

.:: Layer No: 3 ::.

Code: Layer_3 **Start depth:** 3.79 (m), **End depth:** 4.51 (m)

Description: Silty sand & sandy silt

Basic results	Estimation results	
Total cone resistance: 3.56 ±0.54 MPa	Permeability: 1.38E-06 ±1.20E-06 m/s	Constrained Mod.: 27.88 ±4.29 MPa
Sleeve friction: 63.44 ±15.81 kPa	N_{60}: 11.28 ±1.16 blows	Go: 52.28 ±5.13 MPa
Ic: 2.24 ±0.09	Es: 42.71 ±3.60 MPa	Su: 0.00 ±0.00 kPa
σ_v': 45.24 ±1.81 kPa	Dr (%): 42.01 ±2.65	Su ratio: 0.00 ±0.00
SBT_n: 5	φ (degrees): 37.38 ±0.91 °	O.C.R.: 0.00 ±0.00
SBTn description: Silty sand & sandy silt	Unit weight: 18.25 ±0.26 kN/m³	
Schneider zone: Zone 2		
Schneider desc.: Essentially drained sands		

.:: Layer No: 4 ::.

Code: Layer_4 **Start depth:** 4.51 (m), **End depth:** 6.60 (m)

Description: Clay & silty clay

Basic results	Estimation results	
Total cone resistance: 0.89 ±0.17 MPa	Permeability: 2.58E-08 ±2.54E-08 m/s	Constrained Mod.: 6.35 ±1.31 MPa
Sleeve friction: 17.66 ±5.64 kPa	N_{60}: 3.98 ±0.66 blows	Go: 21.78 ±3.16 MPa
Ic: 2.81 ±0.09	Es: 0.00 ±0.00 MPa	Su: 56.67 ±11.69 kPa
σ_v': 55.58 ±2.62 kPa	Dr (%): 0.00 ±0.00	Su ratio: 0.99 ±0.17
SBT_n: 4	φ (degrees): 0.00 ±0.00 °	O.C.R.: 4.57 ±0.78
SBTn description: Clay & silty clay	Unit weight: 16.25 ±0.39 kN/m³	
Schneider zone: Zone 1a		
Schneider desc.: Silts and low Ir clays		

.:: Layer No: 5 ::.

Code: Layer_5 **Start depth:** 6.60 (m), **End depth:** 7.86 (m)

Description: Sand & silty sand

Basic results	Estimation results	
Total cone resistance: 14.33 ±4.03 MPa	Permeability: 2.43E-04 ±3.35E-04 m/s	Constrained Mod.: 85.64 ±13.04 MPa
Sleeve friction: 58.58 ±18.78 kPa	N_{60}: 27.94 ±5.75 blows	Go: 85.63 ±15.07 MPa
Ic: 1.50 ±0.13	Es: 68.33 ±10.40 MPa	Su: 0.00 ±0.00 kPa
σ_v': 67.29 ±3.56 kPa	Dr (%): 69.41 ±9.32	Su ratio: 0.00 ±0.00
SBT_n: 6	φ (degrees): 40.35 ±1.83 °	O.C.R.: 0.00 ±0.00
SBTn description: Sand & silty sand	Unit weight: 18.69 ±0.48 kN/m³	
Schneider zone: Zone 2		
Schneider desc.: Essentially drained sands		

.:: Layer No: 6 ::.

Code: Layer_6 **Start depth:** 7.86 (m), **End depth:** 8.39 (m)

Description: Clay & silty clay

Basic results	Estimation results	
Total cone resistance: 1.86 ±2.22 MPa	Permeability: 7.77E-08 ±5.31E-06 m/s	Constrained Mod.: 13.31 ±17.92 MPa
Sleeve friction: 35.78 ±10.62 kPa	N_{60}: 7.66 ±4.51 blows	Go: 39.94 ±10.78 MPa
Ic: 2.59 ±0.57	Es: 0.00 ±0.00 MPa	Su: 54.79 ±10.61 kPa
σ_v': 75.23 ±1.09 kPa	Dr (%): 0.00 ±0.00	Su ratio: 0.74 ±0.15
SBT_n: 4	φ (degrees): 0.00 ±0.00 °	O.C.R.: 3.40 ±0.67
SBTn description: Clay & silty clay	Unit weight: 17.34 ±0.41 kN/m³	
Schneider zone: Zone 3		
Schneider desc.: Transitional soils		

.:: Layer No: 7 ::.

Code: Layer_7 **Start depth:** 8.39 (m), **End depth:** 8.90 (m)

Description: Sand & silty sand

Basic results	Estimation results	
Total cone resistance: 8.64 ±1.24 MPa	Permeability: 3.75E-05 ±2.72E-05 m/s	Constrained Mod.: 66.19 ±8.29 MPa
Sleeve friction: 46.61 ±9.24 kPa	N_{60}: 20.07 ±2.11 blows	Go: 70.03 ±5.91 MPa
Ic: 1.77 ±0.09	Es: 57.26 ±4.15 MPa	Su: 0.00 ±0.00 kPa
σ_v': 78.54 ±1.09 kPa	Dr (%): 52.56 ±3.60	Su ratio: 0.00 ±0.00
SBT_n: 6	φ (degrees): 37.29 ±0.57 °	O.C.R.: 0.00 ±0.00
SBTn description: Sand & silty sand	Unit weight: 18.23 ±0.23 kN/m³	
Schneider zone: Zone 2		
Schneider desc.: Essentially drained sands		

.:: Layer No: 8 ::.

Code: Layer_8 **Start depth:** 8.90 (m), **End depth:** 11.11 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 1.07 ±0.23 MPa	Permeability: 8.92E-09 ±1.34E-08 m/s	Constrained Mod.: 7.04 ±1.94 MPa
Sleeve friction: 22.41 ±18.59 kPa	N_{60}: 5.39 ±1.03 blows	Go: 30.24 ±8.79 MPa
Ic: 2.96 ±0.14	Es: 0.00 ±0.00 MPa	Su: 63.66 ±16.62 kPa
σ_v': 88.67 ±4.15 kPa	Dr (%): 0.00 ±0.00	Su ratio: 0.72 ±0.20
SBT_n: 3	φ (degrees): 0.00 ±0.00 °	O.C.R.: 3.31 ±0.95
SBTn description: Clay	Unit weight: 16.59 ±0.76 kN/m³	
Schneider zone: Zone 1a		
Schneider desc.: Silts and low Ir clays		

.:: Layer No: 9 ::.

Code: Layer_9 **Start depth:** 11.11 (m), **End depth:** 15.30 (m)

Description: Sand & silty sand

Basic results	Estimation results	
Total cone resistance: 7.65 ±1.73 MPa	Permeability: 9.92E-06 ±1.11E-05 m/s	Constrained Mod.: 59.34 ±13.74 MPa
Sleeve friction: 52.90 ±13.04 kPa	N_{60}: 20.12 ±3.23 blows	Go: 78.28 ±10.60 MPa
Ic: 1.95 ±0.14	Es: 63.67 ±7.61 MPa	Su: 0.00 ±0.00 kPa
σ_v': 113.24 ±9.79 kPa	Dr (%): 44.12 ±4.94	Su ratio: 0.00 ±0.00
SBT_n: 6	φ (degrees): 36.00 ±0.84 °	O.C.R.: 0.00 ±0.00
SBTn description: Sand & silty sand	Unit weight: 18.33 ±0.32 kN/m³	
Schneider zone: N/A		
Schneider desc.: N/A		

.:: Layer No: 10 ::.

Code: Layer_10 **Start depth:** 15.30 (m), **End depth:** 16.95 (m)

Description: Clay & silty clay

Basic results	Estimation results	
Total cone resistance: 1.87 ±2.38 MPa	Permeability: 1.79E-08 ±2.79E-06 m/s	Constrained Mod.: 11.81 ±19.27 MPa
Sleeve friction: 31.16 ±25.54 kPa	N_{60}: 8.79 ±5.52 blows	Go: 47.88 ±21.79 MPa
Ic: 2.84 ±0.35	Es: 0.00 ±0.00 MPa	Su: 80.86 ±14.73 kPa
σ_v': 137.84 ±3.39 kPa	Dr (%): 0.00 ±0.00	Su ratio: 0.59 ±0.11
SBT_n: 4	φ (degrees): 0.00 ±0.00 °	O.C.R.: 2.73 ±0.53
SBTn description: Clay & silty clay	Unit weight: 17.19 ±0.93 kN/m³	
Schneider zone: N/A		
Schneider desc.: N/A		

.:: Layer No: 11 ::.

Code: Layer_11 **Start depth:** 16.95 (m), **End depth:** 17.62 (m)

Description: Sand & silty sand

Basic results	Estimation results	
Total cone resistance: 18.50 ±2.82 MPa	Permeability: 9.03E-05 ±3.75E-05 m/s	Constrained Mod.: 130.04 ±16.64 MPa
Sleeve friction: 108.42 ±29.60 kPa	N_{60}: 39.56 ±5.16 blows	Go: 136.87 ±19.31 MPa
Ic: 1.64 ±0.07	Es: 104.68 ±12.85 MPa	Su: 0.00 ±0.00 kPa
σ_v': 147.13 ±1.93 kPa	Dr (%): 64.65 ±5.16	Su ratio: 0.00 ±0.00
SBT_n: 6	φ (degrees): 39.53 ±1.00 °	O.C.R.: 0.00 ±0.00
SBTn description: Sand & silty sand	Unit weight: 19.50 ±0.38 kN/m³	
Schneider zone: Zone 2		
Schneider desc.: Essentially drained sands		

.:: Layer No: 12 ::.

Code: Layer_12 **Start depth:** 17.62 (m), **End depth:** 18.61 (m)

Description: Sand & silty sand

Basic results	Estimation results	
Total cone resistance: 14.46 ±2.18 MPa	Permeability: 2.15E-05 ±2.06E-05 m/s	Constrained Mod.: 112.47 ±16.50 MPa
Sleeve friction: 122.29 ±12.66 kPa	N_{60}: 35.40 ±2.94 blows	Go: 138.33 ±6.48 MPa
Ic: 1.85 ±0.12	Es: 105.54 ±4.35 MPa	Su: 0.00 ±0.00 kPa
σ_v': 154.90 ±2.63 kPa	Dr (%): 55.24 ±4.76	Su ratio: 0.00 ±0.00
SBT_n: 6	φ (degrees): 38.35 ±0.64 °	O.C.R.: 0.00 ±0.00
SBTn description: Sand & silty sand	Unit weight: 19.54 ±0.12 kN/m³	
Schneider zone: Zone 2		
Schneider desc.: Essentially drained sands		

.:: Layer No: 13 ::.

Code: Layer_13 **Start depth:** 18.61 (m), **End depth:** 19.57 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 1.77 ±0.25 MPa	Permeability: 3.27E-09 ±1.41E-09 m/s	Constrained Mod.: 11.31 ±2.13 MPa
Sleeve friction: 55.40 ±14.87 kPa	N_{60}: 9.86 ±1.05 blows	Go: 62.84 ±8.62 MPa
Ic: 3.10 ±0.05	Es: 0.00 ±0.00 MPa	Su: 102.55 ±17.59 kPa
σ_v': 162.21 ±0.26 kPa	Dr (%): 0.00 ±0.00	Su ratio: 0.63 ±0.11
SBT_n: 3	φ (degrees): 0.00 ±0.00 °	O.C.R.: 2.92 ±0.51
SBTn description: Clay	Unit weight: 17.83 ±0.34 kN/m³	
Schneider zone: Zone 1a		
Schneider desc.: Silts and low Ir clays		

.:: Layer No: 14 ::.

Code: Layer_14 **Start depth:** 19.57 (m), **End depth:** 20.00 (m)

Description: Sand & silty sand

Basic results

Total cone resistance: 9.22 ±0.56 MPa
Sleeve friction: 66.81 ±20.54 kPa
Ic: 2.01 ±0.09
σ_v': 170.52 ±0.79 kPa
SBT_n: 6
SBTn description: Sand & silty sand
Schneider zone: Zone 3
Schneider desc.: Transitional soils

Estimation results

Permeability: 6.66E-06 ±6.74E-06 m/s
N_{60}: 25.11 ±1.72 blows
Es: 81.74 ±8.38 MPa
Dr (%): 41.64 ±1.49
φ (degrees): 35.36 ±0.37 °
Unit weight: 18.67 ±0.38 kN/m³
Constrained Mod.: 70.91 ±4.52 MPa
Go: 102.36 ±12.47 MPa
Su: 0.00 ±0.00 kPa
Su ratio: 0.00 ±0.00
O.C.R.: 0.00 ±0.00

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_D (MPa)	D_r (%)	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_0 (MPa)	Undrained strength, S_u (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
0.02 1.04	1.02	3.03E-05 (±3.18E-06)	1.0 (±0.2)	4.0 (±2.3)	35.7 (±12.5)	35.1 (±1.3)	1.5 (±1.4)	3.4 (±1.5)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	14.3 (±0.9)
1.04 3.70	2.75	2.77E-07 (±1.28E-06)	8.3 (±3.5)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	17.5 (±10.5)	45.8 (±15.9)	138.2 (±96.2)	3.8 (±1.7)	17.4 (±7.8)	18.4 (±0.9)
3.79 4.51	0.72	1.38E-05 (±1.30E-06)	11.3 (±1.2)	42.7 (±3.6)	42.0 (±3.7)	37.4 (±0.9)	27.9 (±4.3)	52.3 (±5.1)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	18.3 (±0.3)
4.51 6.60	2.09	2.50E-05 (±2.54E-08)	4.0 (±0.7)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	0.1 (±1.3)	21.8 (±3.2)	56.7 (±11.7)	1.0 (±0.2)	4.0 (±0.8)	16.2 (±0.4)
6.60 7.86	1.26	2.43E-04 (±3.39E-07)	27.0 (±5.7)	68.3 (±10.1)	69.4 (±9.3)	40.4 (±1.8)	85.6 (±13.1)	85.6 (±15.1)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	18.7 (±0.5)
7.86 8.39	0.53	7.77E-08 (±5.31E-09)	7.7 (±4.5)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	13.3 (±17.9)	39.9 (±10.6)	54.8 (±10.6)	0.7 (±0.1)	3.4 (±0.7)	17.3 (±0.4)
8.39 8.90	0.51	3.75E-05 (±2.72E-05)	20.1 (±2.1)	57.3 (±4.2)	52.6 (±3.6)	37.3 (±0.5)	66.2 (±8.3)	70.0 (±5.5)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	18.2 (±0.2)
8.90 11.11	2.21	8.92E-09 (±1.31E-08)	5.4 (±1.3)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	7.0 (±1.9)	35.7 (±8.8)	63.7 (±16.6)	0.7 (±0.2)	3.3 (±0.9)	16.6 (±0.8)
11.11 15.30	4.19	9.92E-06 (±1.11E-05)	20.1 (±7.7)	63.7 (±7.6)	54.1 (±4.9)	36.0 (±0.5)	59.3 (±13.7)	78.3 (±10.6)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	18.3 (±0.3)
15.30 15.95	1.65	1.79E-08 (±2.79E-06)	8.8 (±5.5)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	11.0 (±19.3)	47.9 (±21.0)	80.9 (±14.7)	0.6 (±0.1)	2.7 (±0.5)	17.2 (±0.9)
15.95 17.62	0.67	9.03E-05 (±1.75E-05)	35.5 (±5.2)	104.7 (±12.3)	64.6 (±5.2)	39.5 (±1.0)	130.0 (±16.1)	136.9 (±13.3)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	19.5 (±0.4)
17.62 18.61	0.99	2.15E-05 (±2.03E-05)	35.4 (±2.9)	105.5 (±4.3)	65.2 (±4.0)	38.4 (±0.5)	112.5 (±16.5)	138.3 (±6.5)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	19.5 (±0.1)

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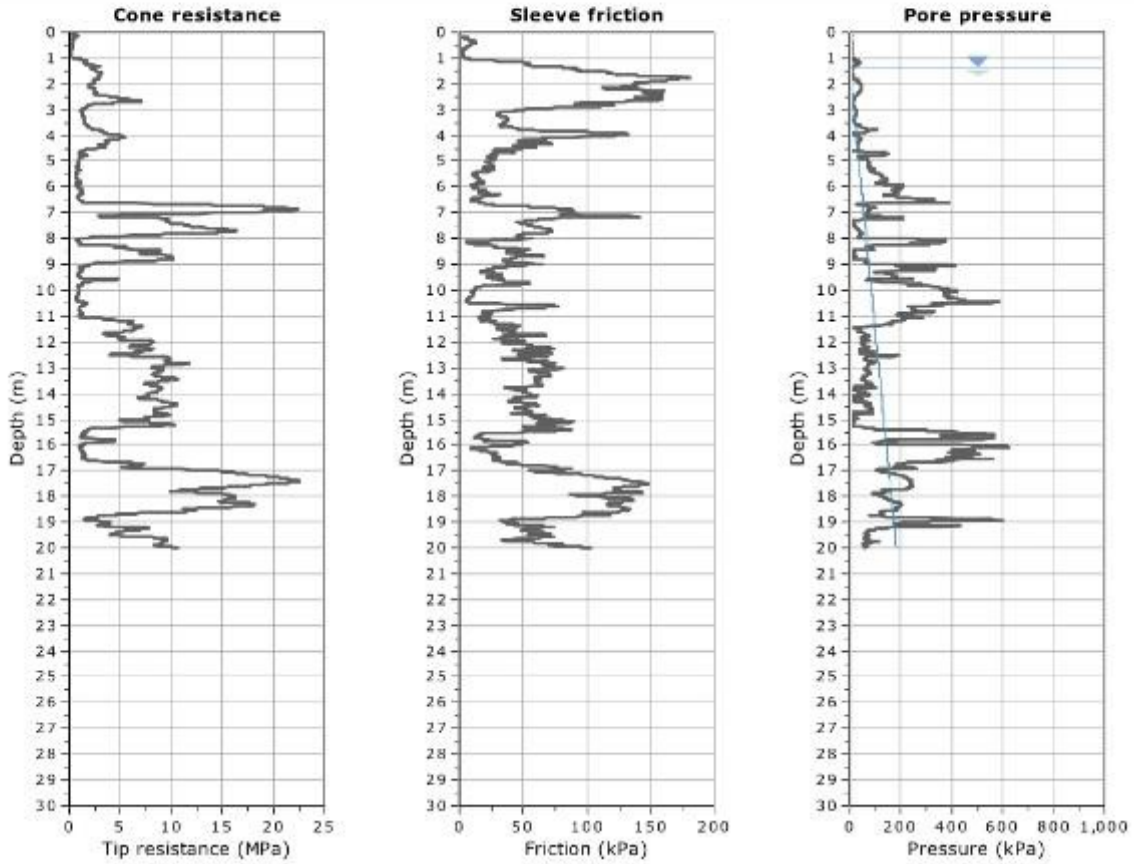
CPT: CPTU2
Total depth: 20.00 m, Date: 06/03/2026
Surface Elevation: 0.00 m, Est. GWL: 1.40 m
Coords: X:0.00, Y:0.00
Cone Type:
Cone Operator:

Project:
Location:

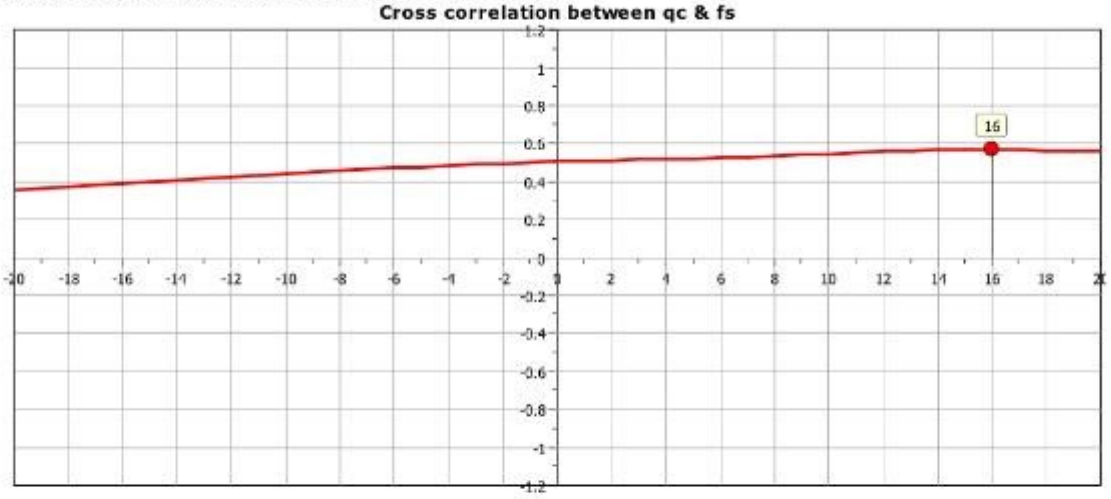
Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_D (MPa)	D_r (%)	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_0 (MPa)	Undrained strength, S_u (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
18.61 19.57	0.96	3.27E-09 (±1.41E-09)	9.9 (±1.0)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	31.3 (±2.1)	62.8 (±8.8)	102.6 (±17.8)	0.6 (±0.1)	2.9 (±0.5)	17.8 (±0.3)
19.57 20.00	0.43	6.86E-05 (±6.74E-06)	25.1 (±1.7)	81.7 (±4.4)	41.6 (±1.5)	35.4 (±0.4)	70.9 (±4.5)	102.4 (±12.5)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	18.7 (±0.4)

Depth values presented in this table are measured from free ground surface



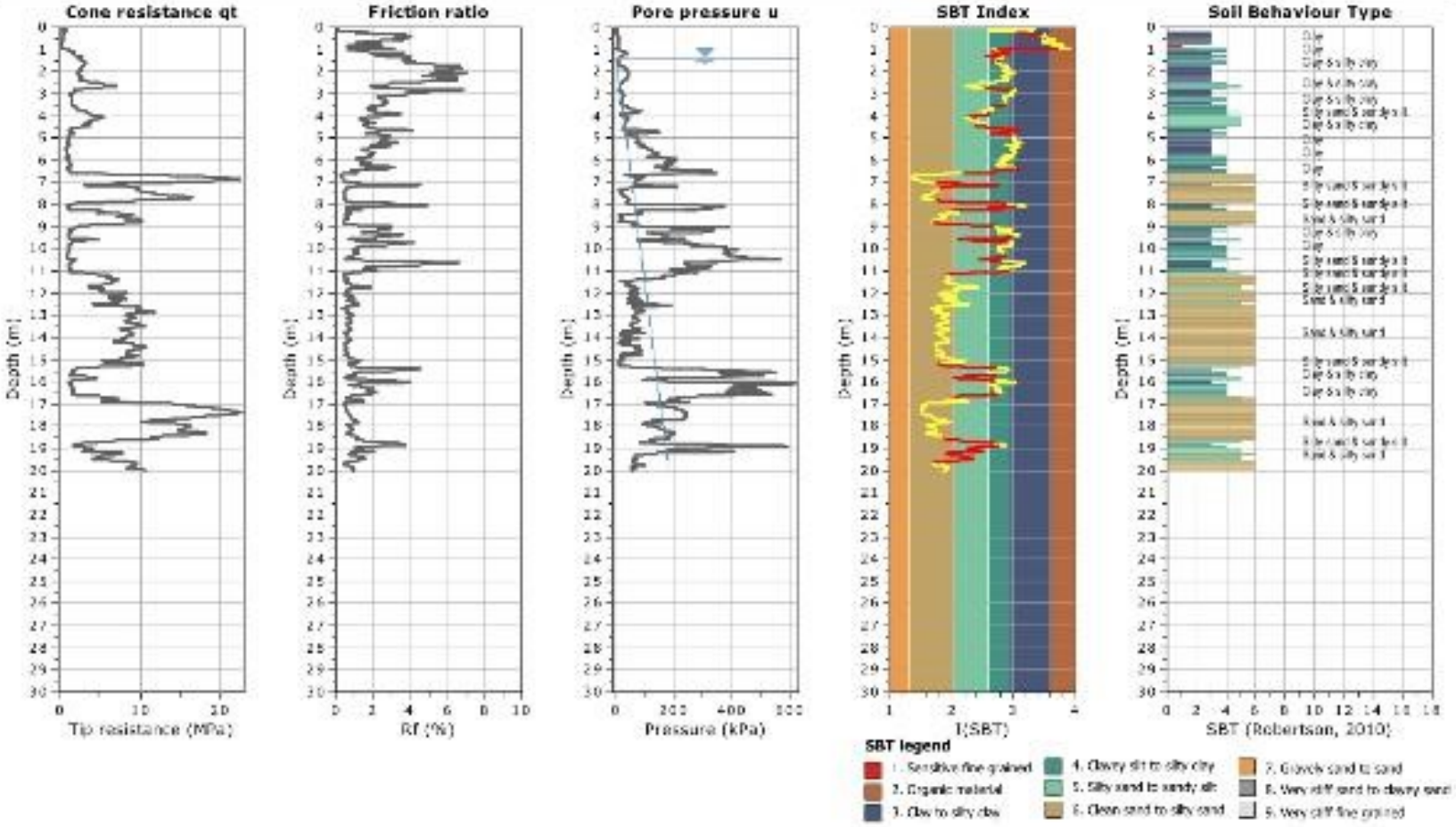
The plot below presents the cross correlation coeficient between the raw qc and fs values (as measured on the field). X axes presents the lag distance (one lag is the distance between two sucessive CPT measurements).



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Project:
Location:

CPT: CPTU2
Total depth: 20.00 m, Date: 06/03/2026
Surface Elevation: 0.00 m, Est. GWL: 1.40 m
Coords: X:0.00, Y:0.00
Cone Type:
Cone Operator:



Servizi Geologici S.r.l.

PROVA PENETROMETRICA STATICA CON PIEZOCONO

Certificato n°: **0145/26**
Data emissione: **06/03/2026**

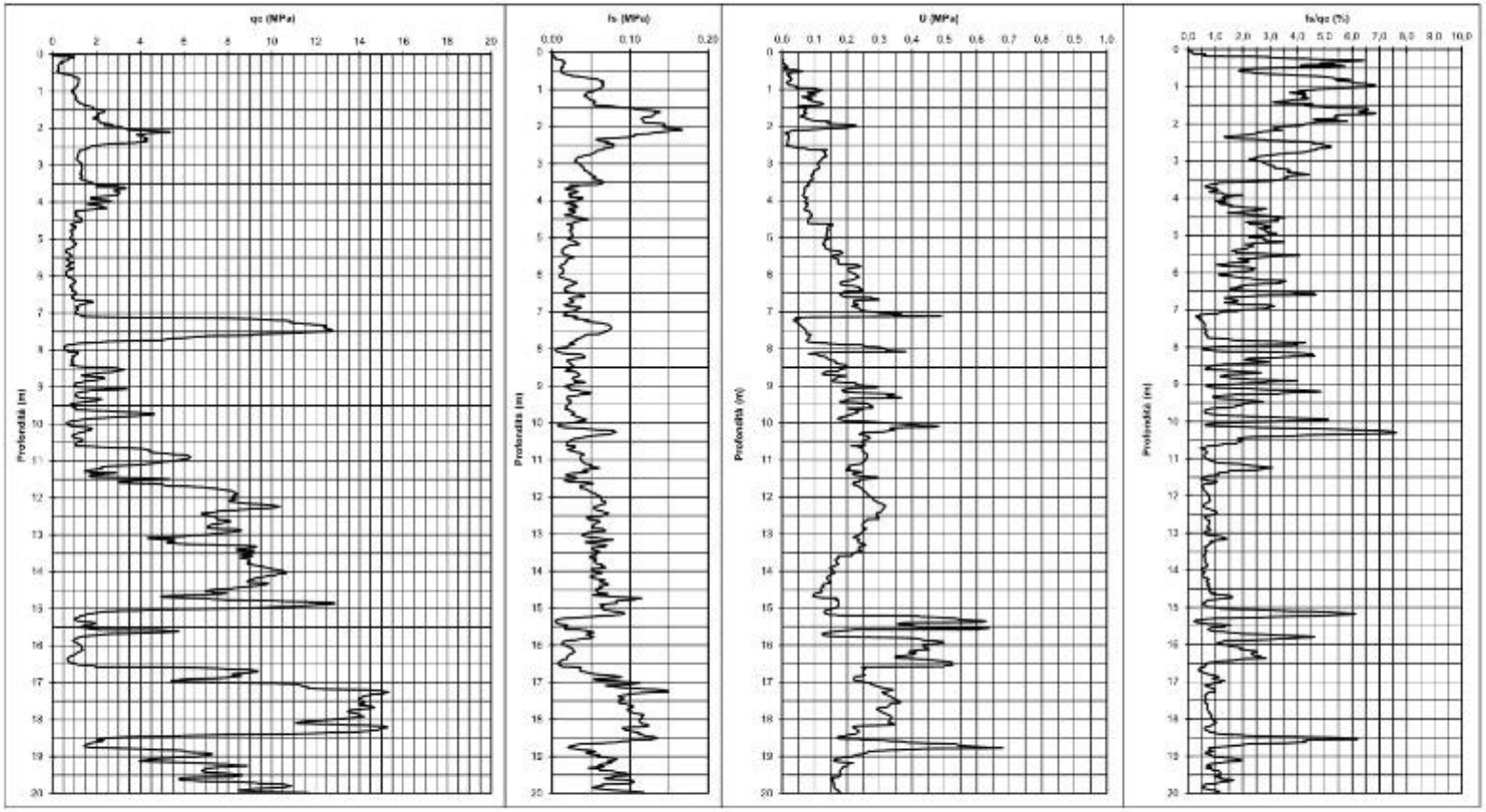
COMMITTENTE: **Geodelta Srl STP**

CANTIERE: **Padova, Via Strada dei Boti c/o Ex Istituto Configliachi**

PROVA N°: **CPTU3** DATA: **05/03/2026** Operatore M. Mengato

Punta	Piezocono		Quota p.c.:	0,00	m.s.l.m.	Coordinate X	Y
Preforo	0,00	m	Livello acqua	1,40	m da p.c.	Profondità finale	20,00 m da p.c.

NOTE



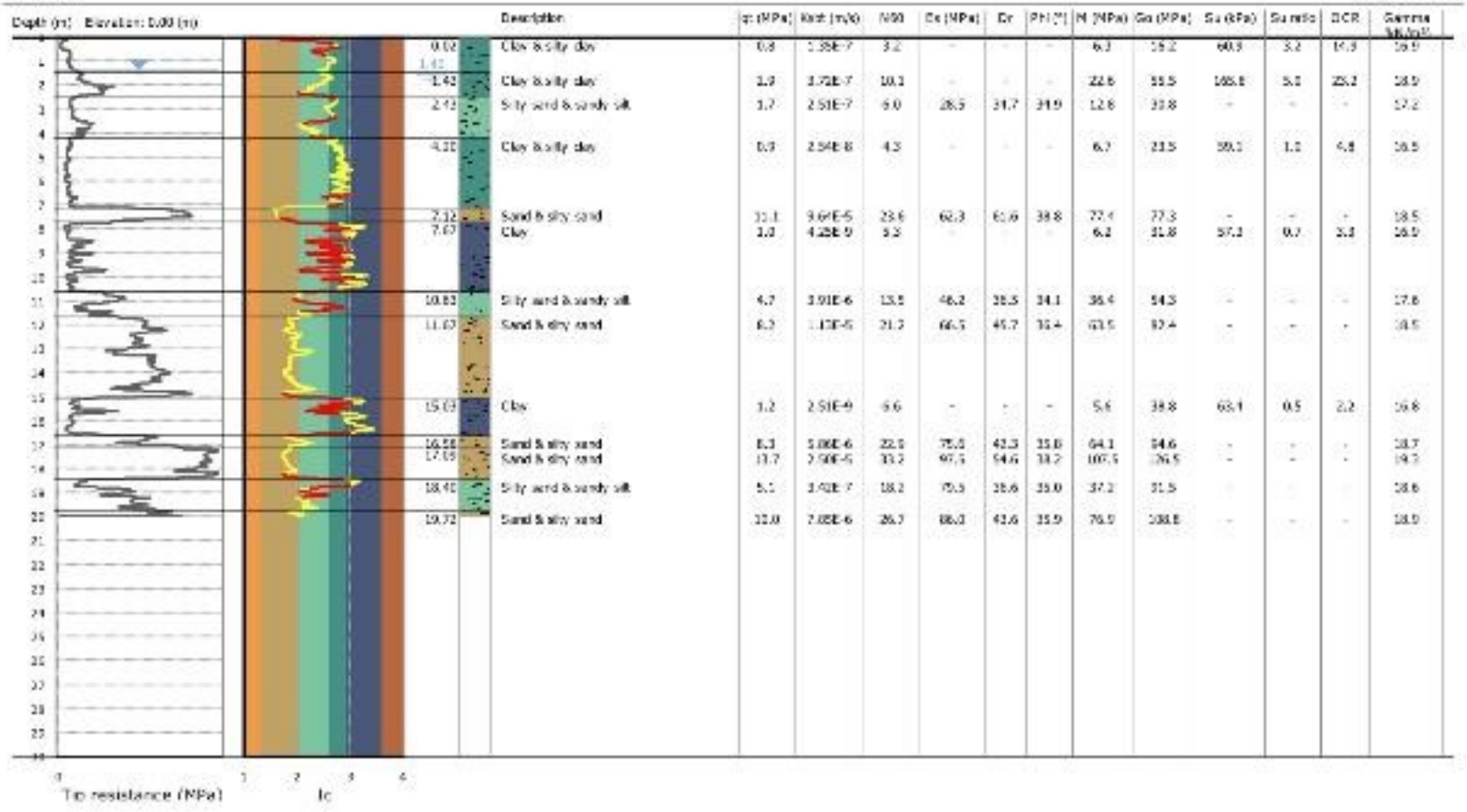
CPTU3

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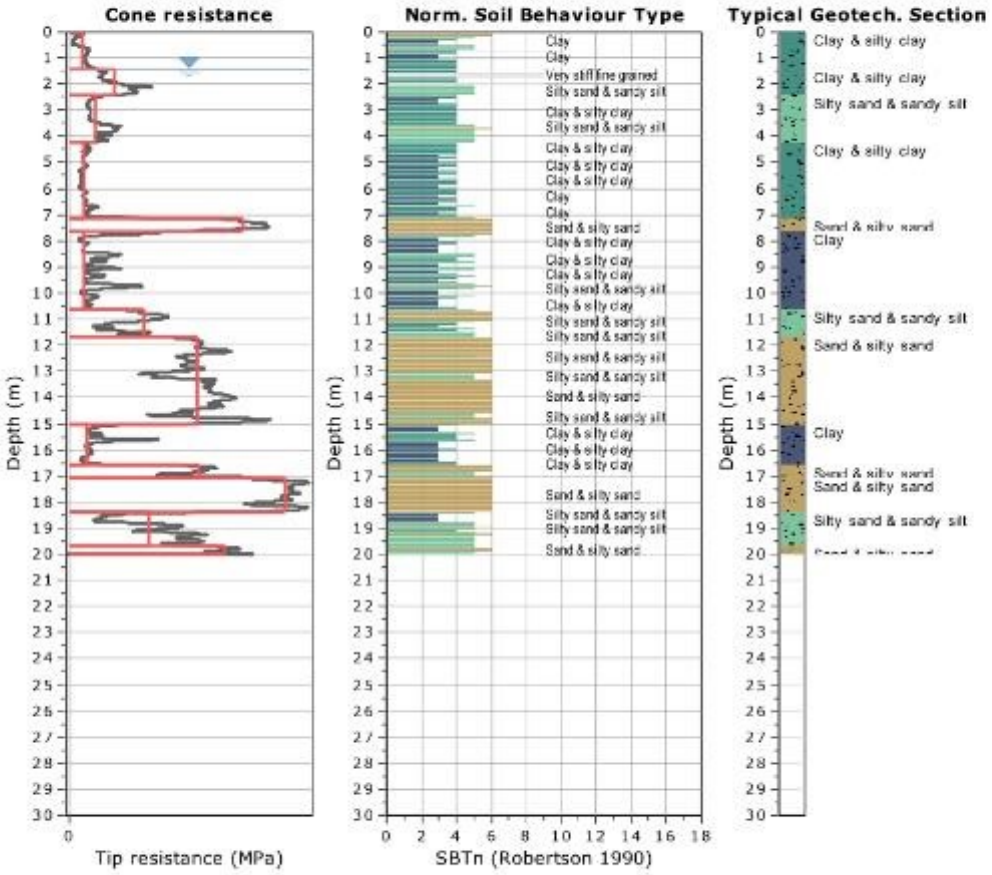
CPT: CPTU3

Total depth: 20.00 m, Date: 06/03/2026
Surface Elevation: 0.00 m, Est. GWL: 1.40 m
Coords: X:0.00, Y:0.00
Cone Type:
Cone Operator:

Project:
Location:



Depth (m)	Description	qc (MPa)	Rint (m/kPa)	N60	Qtn (MPa)	Qtn	Fr (%)	N (MPa)	Go (MPa)	Su (kPa)	Su ratio	OCR	Gamma (kN/m³)
0.12	Clay & silty clay	0.8	1.38E-7	3.2	-	-	-	6.3	19.2	60.9	3.2	14.9	19.0
1.43	Clay & silty clay	1.9	3.72E-7	10.1	-	-	-	22.6	55.5	165.8	5.3	25.2	18.9
2.12	Silty sand & sandy silt	1.7	2.51E-7	9.0	28.5	31.7	31.9	12.8	33.8	-	-	-	17.2
4.22	Clay & silty clay	0.9	2.54E-8	4.5	-	-	-	6.7	23.5	99.1	1.1	4.8	18.5
7.12	Sand & silty sand	11.1	9.69E-5	23.6	62.3	61.6	38.8	77.4	77.3	-	-	-	18.5
7.63	Clay	1.0	4.25E-9	5.3	-	-	-	6.2	31.8	97.3	0.7	3.8	18.9
10.83	Silty sand & sandy silt	4.7	3.91E-6	13.5	46.2	38.5	34.1	38.4	54.3	-	-	-	17.8
11.63	Sand & silty sand	6.2	1.17E-5	21.3	66.5	45.7	31.4	63.5	83.4	-	-	-	18.5
15.03	Clay	1.2	2.51E-9	6.6	-	-	-	5.6	38.8	63.1	0.5	2.2	19.8
16.58	Sand & silty sand	8.3	5.08E-6	22.0	75.0	42.3	35.0	64.1	84.6	-	-	-	18.7
17.08	Sand & silty sand	13.7	2.90E-5	33.2	97.5	54.6	38.2	107.5	126.5	-	-	-	19.3
18.42	Silty sand & sandy silt	5.1	3.42E-7	18.2	75.3	35.6	35.0	37.2	31.5	-	-	-	18.6
19.72	Sand & silty sand	12.0	7.85E-6	26.7	88.3	43.6	35.9	76.9	108.8	-	-	-	18.9



Tabular results

.:: Layer No: 1 ::.

Code: Layer_1 **Start depth:** 0.02 (m), **End depth:** 1.43 (m)

Description: Clay & silty clay

Basic results

Total cone resistance: 0.80 ±0.44 MPa
Sleeve friction: 0.00 ±47.34 kPa
Ic: 2.53 ±0.27
σ_v': 10.83 +7.96 kPa
SBT_n: 4
SBTn description: Clay & silty clay
Schneider zone: Zone 3
Schneider desc.: Transitional soils

Estimation results

Permeability: 1.35E-07 ±2.24E-05 m/s
N_{60}: 3.25 ±1.66 blows
Es: 0.00 ±0.00 MPa
Dr (%): 0.00 +0.00
φ (degrees): 0.00 ±0.00 °
Unit weight: 16.88 ±1.31 kN/m³
Constrained Mod.: 6.30 ±3.47 MPa
Go: 16.25 ±10.48 MPa
Su: 60.88 ±29.43 kPa
Su ratio: 3.23 +0.56
O.C.R.: 14.94 ±2.57

.:: Layer No: 2 ::.

Code: Layer_2 **Start depth:** 1.43 (m), **End depth:** 2.43 (m)

Description: Clay & silty clay

Basic results	Estimation results	
Total cone resistance: 2.85 ±1.05 MPa	Permeability: 3.72E-07 ±1.08E-06 m/s	Constrained Mod.: 22.56 ±8.33 MPa
Sleeve friction: 119.05 ±24.93 kPa	N_{60}: 10.11 ±2.58 blows	Go: 55.51 ±10.02 MPa
Ic: 2.42 ±0.17	Es: 0.00 ±0.00 MPa	Su: 165.82 ±36.69 kPa
σ_v': 27.36 ±2.45 kPa	Dr (%): 0.00 ±0.00	Su ratio: 5.02 ±0.69
SBT_n: 4	φ (degrees): 0.00 ±0.00 °	O.C.R.: 23.18 ±3.18
SBTn description: Clay & silty clay	Unit weight: 18.89 ±0.31 kN/m³	
Schneider zone: Zone 3		
Schneider desc.: Transitional soils		

.:: Layer No: 3 ::.

Code: Layer_3 **Start depth:** 2.43 (m), **End depth:** 4.20 (m)

Description: Silty sand & sandy silt

Basic results	Estimation results	
Total cone resistance: 1.66 ±0.66 MPa	Permeability: 2.51E-07 ±1.49E-06 m/s	Constrained Mod.: 12.79 ±5.27 MPa
Sleeve friction: 34.04 ±10.96 kPa	N_{60}: 6.04 ±1.40 blows	Go: 30.84 ±3.26 MPa
Ic: 2.47 ±0.23	Es: 28.48 ±2.56 MPa	Su: 0.00 ±0.00 kPa
σ_v': 39.47 ±3.66 kPa	Dr (%): 34.71 ±3.22	Su ratio: 0.00 ±0.00
SBT_n: 5	φ (degrees): 34.86 ±0.56 °	O.C.R.: 0.00 ±0.00
SBTn description: Silty sand & sandy silt	Unit weight: 17.24 ±0.28 kN/m³	
Schneider zone: Zone 3		
Schneider desc.: Transitional soils		

.:: Layer No: 4 ::.

Code: Layer_4 **Start depth:** 4.20 (m), **End depth:** 7.12 (m)

Description: Clay & silty clay

Basic results	Estimation results	
Total cone resistance: 0.94 ±0.35 MPa	Permeability: 2.54E-08 ±7.79E-07 m/s	Constrained Mod.: 6.75 ±2.77 MPa
Sleeve friction: 20.97 ±8.24 kPa	N_{60}: 4.26 ±1.00 blows	Go: 23.54 ±4.49 MPa
Ic: 2.81 ±0.13	Es: 0.00 ±0.00 MPa	Su: 59.10 ±12.35 kPa
σ_v': 54.82 ±4.99 kPa	Dr (%): 0.00 ±0.00	Su ratio: 1.05 ±0.24
SBT_n: 4	φ (degrees): 0.00 ±0.00 °	O.C.R.: 4.84 ±1.12
SBTn description: Clay & silty clay	Unit weight: 16.47 ±0.47 kN/m³	
Schneider zone: Zone 1a		
Schneider desc.: Silts and low Ir clays		

.:: Layer No: 5 ::.

Code: Layer_5 **Start depth:** 7.12 (m), **End depth:** 7.67 (m)

Description: Sand & silty sand

Basic results	Estimation results	
Total cone resistance: 11.08 ±1.72 MPa	Permeability: 9.64E-05 ±2.98E-05 m/s	Constrained Mod.: 77.41 ±12.17 MPa
Sleeve friction: 54.83 ±18.35 kPa	N_{60}: 23.58 ±3.57 blows	Go: 77.30 ±12.80 MPa
Ic: 1.63 ±0.06	Es: 62.26 ±8.87 MPa	Su: 0.00 ±0.00 kPa
σ_v': 67.21 ±1.11 kPa	Dr (%): 61.64 ±4.98	Su ratio: 0.00 ±0.00
SBT_n: 6	φ (degrees): 38.81 ±1.02 °	O.C.R.: 0.00 ±0.00
SBTn description: Sand & silty sand	Unit weight: 18.52 ±0.47 kN/m³	
Schneider zone: N/A		
Schneider desc.: N/A		

.:: Layer No: 6 ::.

Code: Layer_6 **Start depth:** 7.67 (m), **End depth:** 10.63 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.96 ±0.21 MPa	Permeability: 4.25E-09 ±7.15E-09 m/s	Constrained Mod.: 6.20 ±1.87 MPa
Sleeve friction: 31.03 ±18.17 kPa	N_{60}: 5.25 ±0.98 blows	Go: 31.84 ±8.17 MPa
Ic: 3.07 ±0.15	Es: 0.00 ±0.00 MPa	Su: 57.31 ±14.67 kPa
σ_v': 81.20 ±6.71 kPa	Dr (%): 0.00 ±0.00	Su ratio: 0.71 ±0.15
SBT_n: 3	φ (degrees): 0.00 ±0.00 °	O.C.R.: 3.26 ±0.70
SBTn description: Clay	Unit weight: 16.92 ±0.58 kN/m³	
Schneider zone: Zone 1a		
Schneider desc.: Silts and low Ir clays		

.:: Layer No: 7 ::.

Code: Layer_7 **Start depth:** 10.63 (m), **End depth:** 11.67 (m)

Description: Silty sand & sandy silt

Basic results	**Estimation results**	
Total cone resistance: 4.74 ±0.99 MPa	Permeability: 3.91E-06 ±3.14E-06 m/s	Constrained Mod.: 36.37 ±7.96 MPa
Sleeve friction: 31.37 ±11.11 kPa	N_{60}: 13.48 ±2.04 blows	Go: 54.33 ±8.65 MPa
Ic: 2.09 ±0.10	Es: 46.17 ±6.21 MPa	Su: 0.00 ±0.00 kPa
σ_v': 95.41 ±3.06 kPa	Dr (%): 36.54 ±4.22	Su ratio: 0.00 ±0.00
SBT_n: 5	φ (degrees): 34.09 ±1.05 °	O.C.R.: 0.00 ±0.00
SBTn description: Silty sand & sandy silt	Unit weight: 17.55 ±0.45 kN/m³	
Schneider zone: Zone 3		
Schneider desc.: Transitional soils		

.:: Layer No: 8 ::.

Code: Layer_8 **Start depth:** 11.67 (m), **End depth:** 15.03 (m)

Description: Sand & silty sand

Basic results	**Estimation results**	
Total cone resistance: 8.17 ±1.53 MPa	Permeability: 1.13E-05 ±9.88E-06 m/s	Constrained Mod.: 63.51 ±12.21 MPa
Sleeve friction: 58.37 ±12.28 kPa	N_{60}: 21.19 ±2.69 blows	Go: 82.40 ±8.83 MPa
Ic: 1.94 ±0.12	Es: 66.51 ±6.26 MPa	Su: 0.00 ±0.00 kPa
σ_v': 112.67 ±8.07 kPa	Dr (%): 45.71 ±4.39	Su ratio: 0.00 ±0.00
SBT_n: 6	φ (degrees): 36.36 ±0.75 °	O.C.R.: 0.00 ±0.00
SBTn description: Sand & silty sand	Unit weight: 18.47 ±0.25 kN/m³	
Schneider zone: N/A		
Schneider desc.: N/A		

.:: Layer No: 9 ::.

Code: Layer_9 **Start depth:** 15.03 (m), **End depth:** 16.58 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.18 ±0.27 MPa	Permeability: 2.51E-09 ±3.95E-09 m/s	Constrained Mod.: 5.61 ±3.14 MPa
Sleeve friction: 26.19 ±23.58 kPa	N_{60}: 6.61 ±1.34 blows	Go: 38.80 ±12.11 MPa
Ic: 3.15 ±0.15	Es: 0.00 ±0.00 MPa	Su: 63.40 ±19.89 kPa
σ_v': 134.66 ±2.82 kPa	Dr (%): 0.00 ±0.00	Su ratio: 0.47 ±0.16
SBT_n: 3	φ (degrees): 0.00 ±0.00 °	O.C.R.: 2.18 ±0.72
SBTn description: Clay	Unit weight: 16.81 ±0.77 kN/m³	
Schneider zone: Zone 1a		
Schneider desc.: Silts and low Ir clays		

.:: Layer No: 10 ::.

Code: Layer_10 **Start depth:** 16.58 (m), **End depth:** 17.09 (m)

Description: Sand & silty sand

Basic results	Estimation results	
Total cone resistance: 8.31 ±1.71 MPa	Permeability: 5.86E-06 ±8.93E-06 m/s	Constrained Mod.: 64.08 ±13.70 MPa
Sleeve friction: 68.40 ±22.02 kPa	N_{60}: 22.94 ±3.32 blows	Go: 94.63 ±13.39 MPa
Ic: 2.03 ±0.14	Es: 75.61 ±9.12 MPa	Su: 0.00 ±0.00 kPa
σ_v': 141.62 ±1.06 kPa	Dr (%): 42.30 ±4.79	Su ratio: 0.00 ±0.00
SBT_n: 6	φ (degrees): 35.82 ±0.86 °	O.C.R.: 0.00 ±0.00
SBTn description: Sand & silty sand	Unit weight: 18.66 ±0.38 kN/m³	
Schneider zone: Zone 3		
Schneider desc.: Transitional soils		

.:: Layer No: 11 ::.

Code: Layer_11 **Start depth:** 17.09 (m), **End depth:** 18.40 (m)

Description: Sand & silty sand

Basic results	Estimation results	
Total cone resistance: 13.75 ±1.10 MPa	Permeability: 2.50E-05 ±1.08E-05 m/s	Constrained Mod.: 107.49 ±8.83 MPa
Sleeve friction: 103.98 ±16.70 kPa	N_{60}: 33.16 ±1.94 blows	Go: 126.47 ±8.97 MPa
Ic: 1.83 ±0.06	Es: 97.53 ±5.97 MPa	Su: 0.00 ±0.00 kPa
σ_v': 148.82 ±3.17 kPa	Dr (%): 54.64 ±2.55	Su ratio: 0.00 ±0.00
SBT_n: 6	φ (degrees): 38.19 ±0.46 °	O.C.R.: 0.00 ±0.00
SBTn description: Sand & silty sand	Unit weight: 19.34 ±0.19 kN/m³	
Schneider zone: Zone 3		
Schneider desc.: Transitional soils		

.:: Layer No: 12 ::.

Code: Layer_12 **Start depth:** 18.40 (m), **End depth:** 19.72 (m)

Description: Silty sand & sandy silt

Basic results	Estimation results	
Total cone resistance: 5.07 ±2.64 MPa	Permeability: 3.42E-07 ±2.03E-06 m/s	Constrained Mod.: 37.24 ±21.27 MPa
Sleeve friction: 74.41 ±26.06 kPa	N_{60}: 18.19 ±5.64 blows	Go: 91.46 ±17.73 MPa
Ic: 2.41 ±0.41	Es: 79.48 ±8.31 MPa	Su: 0.00 ±0.00 kPa
σ_v': 162.59 ±3.59 kPa	Dr (%): 36.64 ±2.75	Su ratio: 0.00 ±0.00
SBT_n: 5	φ (degrees): 34.96 ±0.68 °	O.C.R.: 0.00 ±0.00
SBTn description: Silty sand & sandy silt	Unit weight: 18.57 ±0.48 kN/m³	
Schneider zone: N/A		
Schneider desc.: N/A		

.:: Layer No: 13 ::.

Code: Layer_13 **Start depth:** 19.72 (m), **End depth:** 20.00 (m)

Description: Sand & silty sand

Basic results	Estimation results	
Total cone resistance: 9.96 ±0.89 MPa	Permeability: 7.85E-06 ±6.23E-06 m/s	Constrained Mod.: 76.88 ±7.09 MPa
Sleeve friction: 76.00 ±22.57 kPa	N_{60}: 26.73 ±1.83 blows	Go: 108.78 ±12.23 MPa
Ic: 1.99 ±0.10	Es: 86.04 ±8.17 MPa	Su: 0.00 ±0.00 kPa
σ_v': 168.52 ±0.73 kPa	Dr (%): 43.65 ±2.31	Su ratio: 0.00 ±0.00
SBT_n: 6	φ (degrees): 35.92 ±0.47 °	O.C.R.: 0.00 ±0.00
SBTn description: Sand & silty sand	Unit weight: 18.85 ±0.31 kN/m³	
Schneider zone: Zone 2		
Schneider desc.: Essentially drained sands		

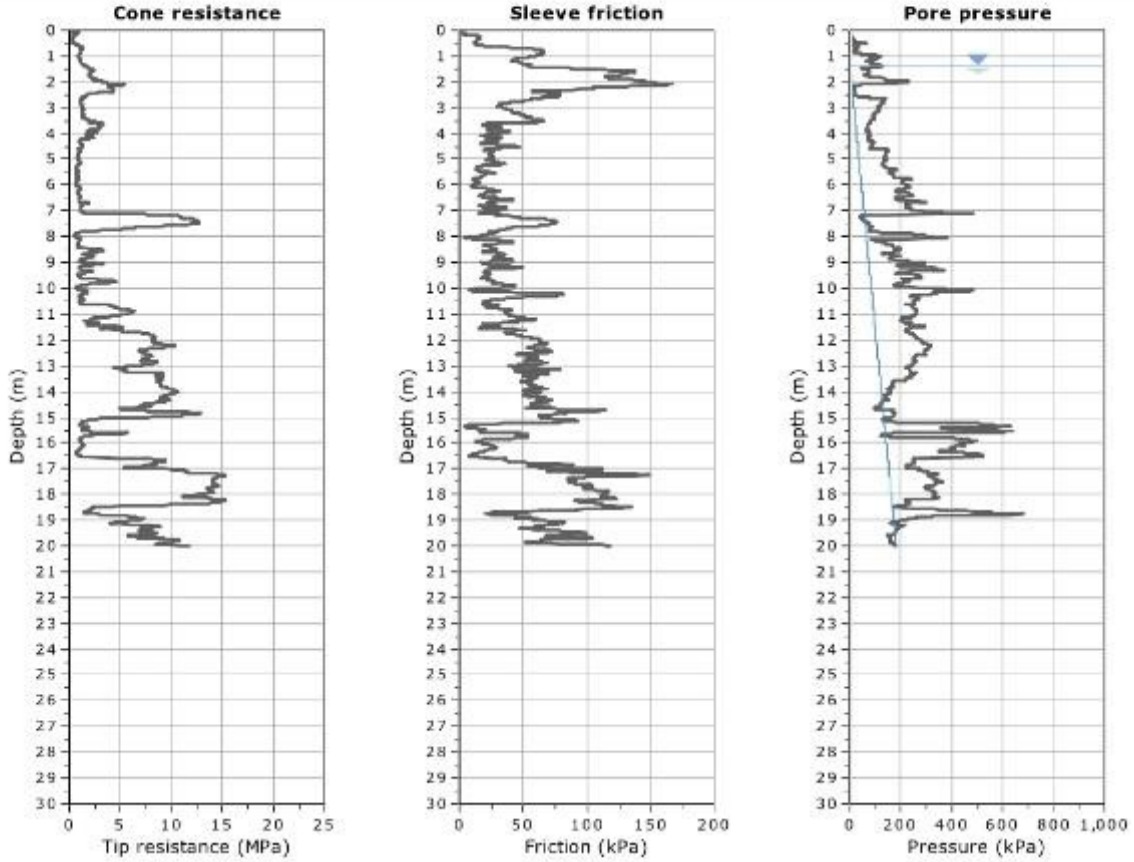
Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_0 (MPa)	D_r (%)	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_0 (MPa)	Undrained strength, S_u (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
0.02 1.41	1.41	1.35E-07 (±2.24E-05)	3.2 (±1.7)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	6.3 (±3.5)	10.2 (±10.5)	50.9 (±29.4)	3.2 (±0.0)	14.9 (±2.6)	16.9 (±1.3)
1.41 2.43	1.00	3.72E-07 (±1.08E-06)	10.1 (±2.6)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	22.6 (±8.3)	55.5 (±13.0)	165.8 (±36.7)	5.0 (±0.7)	13.2 (±3.2)	18.9 (±1.3)
2.43 4.20	1.77	2.51E-07 (±1.49E-06)	6.0 (±1.4)	28.5 (±7.6)	34.7 (±3.2)	34.9 (±0.5)	12.8 (±5.3)	30.8 (±3.1)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	17.2 (±1.3)
4.20 7.12	2.92	2.54E-08 (±7.73E-07)	4.3 (±1.2)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	6.7 (±2.8)	23.5 (±9.5)	59.1 (±12.4)	1.0 (±0.2)	4.8 (±1.1)	16.5 (±1.5)
7.12 7.67	0.55	9.84E-05 (±2.98E-03)	23.6 (±2.6)	62.3 (±6.9)	61.6 (±5.0)	38.8 (±1.0)	77.4 (±12.2)	77.3 (±12.8)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	18.5 (±0.5)
7.67 10.63	2.96	4.25E-09 (±7.12E-08)	5.3 (±1.3)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	6.2 (±1.9)	31.8 (±8.2)	57.3 (±14.7)	0.7 (±0.2)	3.3 (±0.7)	16.9 (±0.6)
10.63 11.67	1.04	3.91E-05 (±3.14E-06)	13.5 (±2.2)	46.2 (±5.2)	36.5 (±4.2)	34.1 (±1.1)	36.4 (±8.0)	54.3 (±8.5)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	17.6 (±0.5)
11.67 15.03	3.36	1.13E-05 (±5.88E-06)	21.7 (±2.7)	66.5 (±6.3)	46.7 (±1.7)	36.4 (±0.7)	63.5 (±12.2)	87.4 (±8.8)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	18.5 (±1.2)
15.03 16.58	1.55	2.51E-09 (±3.93E-09)	6.6 (±1.3)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	5.6 (±1.1)	38.8 (±12.1)	63.4 (±19.5)	0.5 (±0.2)	2.2 (±0.7)	16.8 (±0.8)
16.58 17.09	0.51	5.86E-05 (±8.93E-06)	22.8 (±3.3)	75.6 (±3.1)	42.3 (±4.0)	35.8 (±0.3)	84.1 (±13.7)	94.6 (±11.4)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	18.7 (±0.4)
17.09 18.40	1.31	2.50E-05 (±3.08E-05)	33.2 (±1.3)	97.5 (±9.0)	54.6 (±2.5)	38.2 (±0.5)	107.5 (±9.8)	126.5 (±9.1)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	19.3 (±1.2)
18.40 19.72	1.32	3.42E-07 (±2.03E-06)	18.2 (±5.5)	79.5 (±8.3)	36.6 (±2.8)	35.0 (±0.7)	37.2 (±21.3)	91.5 (±17.7)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	18.6 (±1.5)

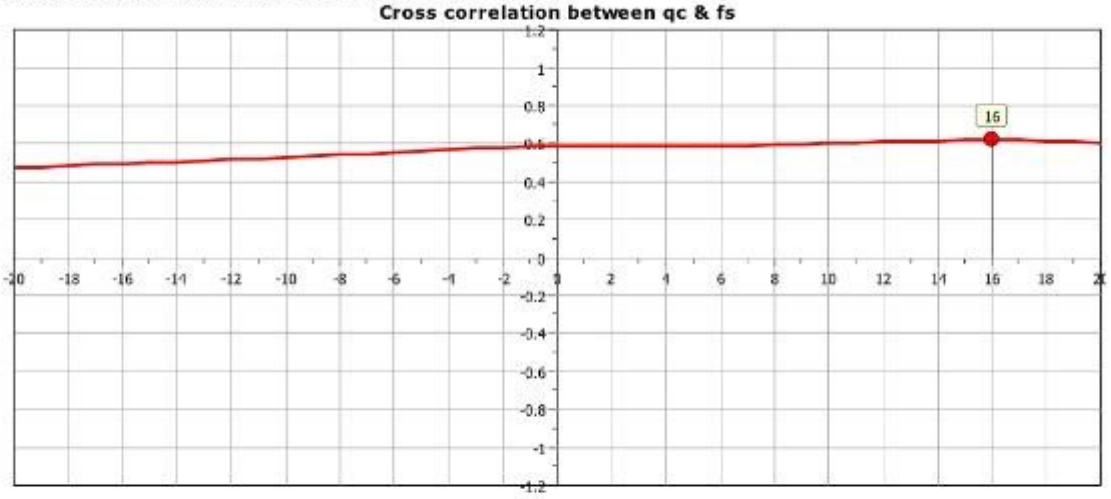
Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_0 (MPa)	D_r (%)	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_0 (MPa)	Undrained strength, S_u (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
19.72 20.00	0.28	7.85E-05 (±6.23E-06)	20.7 (±1.8)	86.0 (±8.2)	43.6 (±2.3)	35.9 (±0.5)	76.9 (±7.1)	100.8 (±12.2)	0.0 (±0.0)	0.0 (±0.0)	0.0 (±0.0)	18.9 (±1.3)

Depth values presented in this table are measured from free ground surface



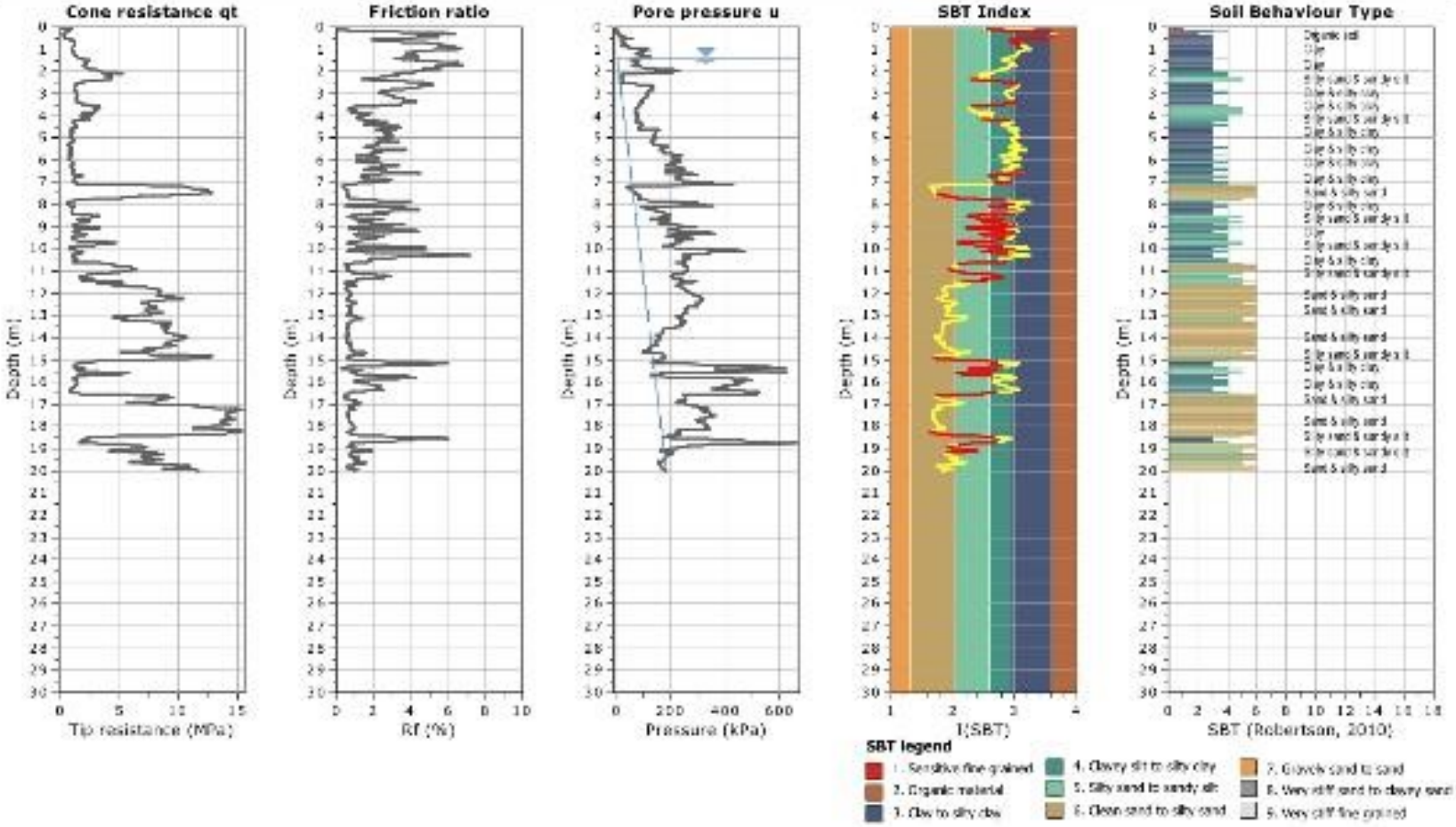
The plot below presents the cross correlation coeficient between the raw qc and fs values (as measured on the field). X axes presents the lag distance (one lag is the distance between two sucessive CPT measurements).



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Project:
Location:

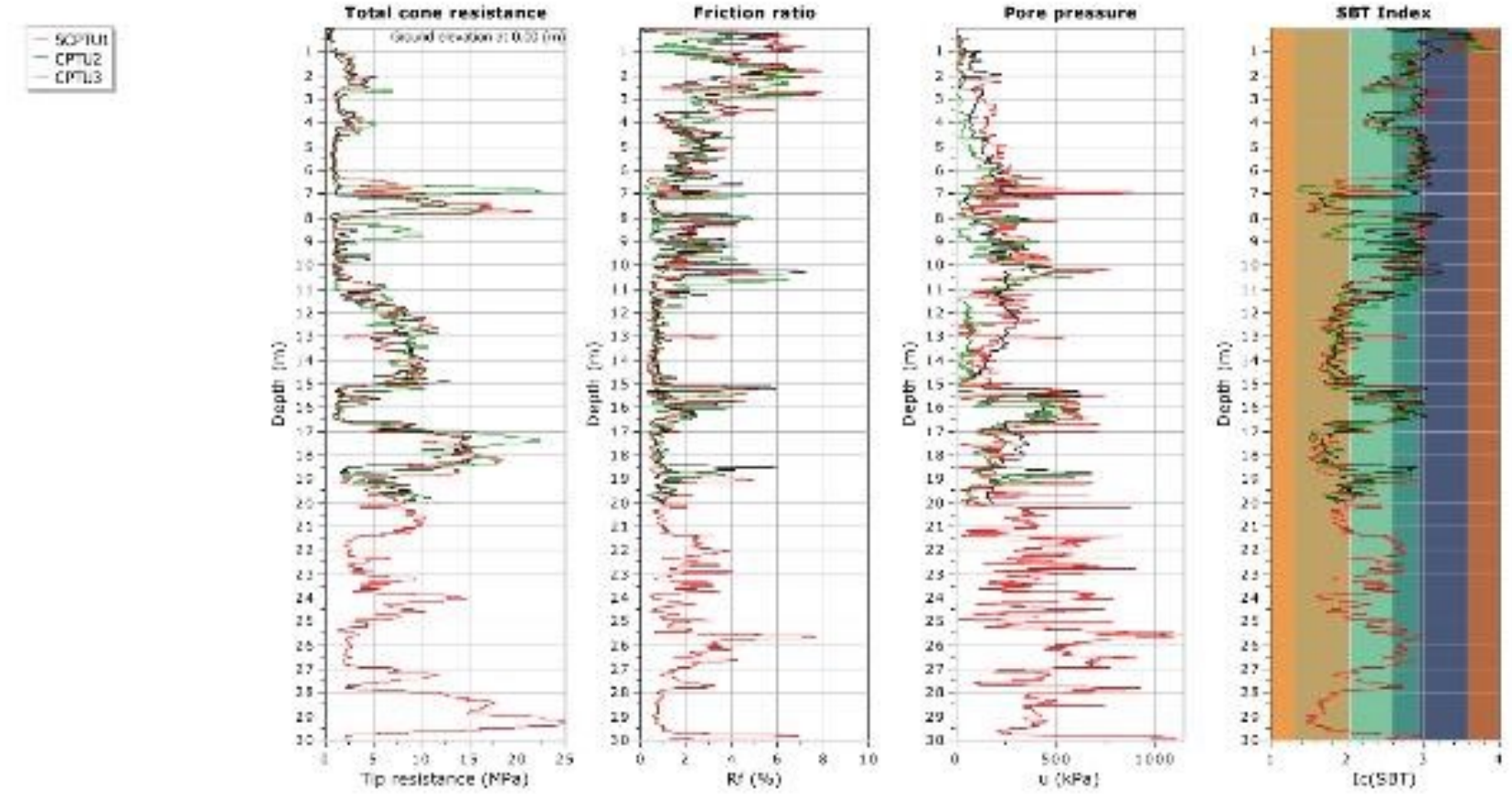
CPT: CPTU3
Total depth: 20.00 m, Date: 06/03/2026
Surface Elevation: 0.00 m, Est. GWL: 1.40 m
Coords: X:0.00, Y:0.00
Cone Type:
Cone Operator:



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Project:
Location:

Overlay basic interpretation plots



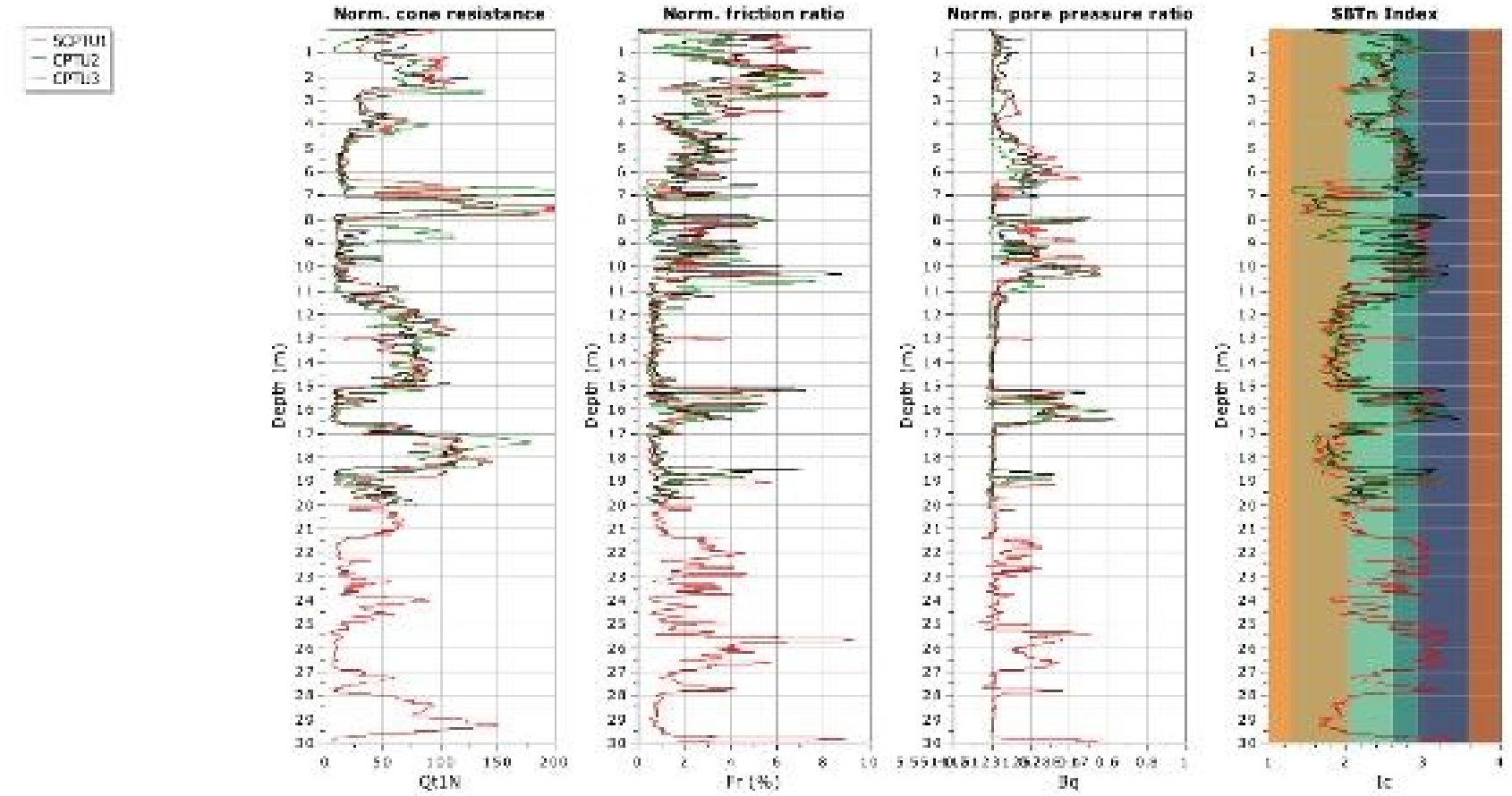
OVERLAY REPORT

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Project:

Location:

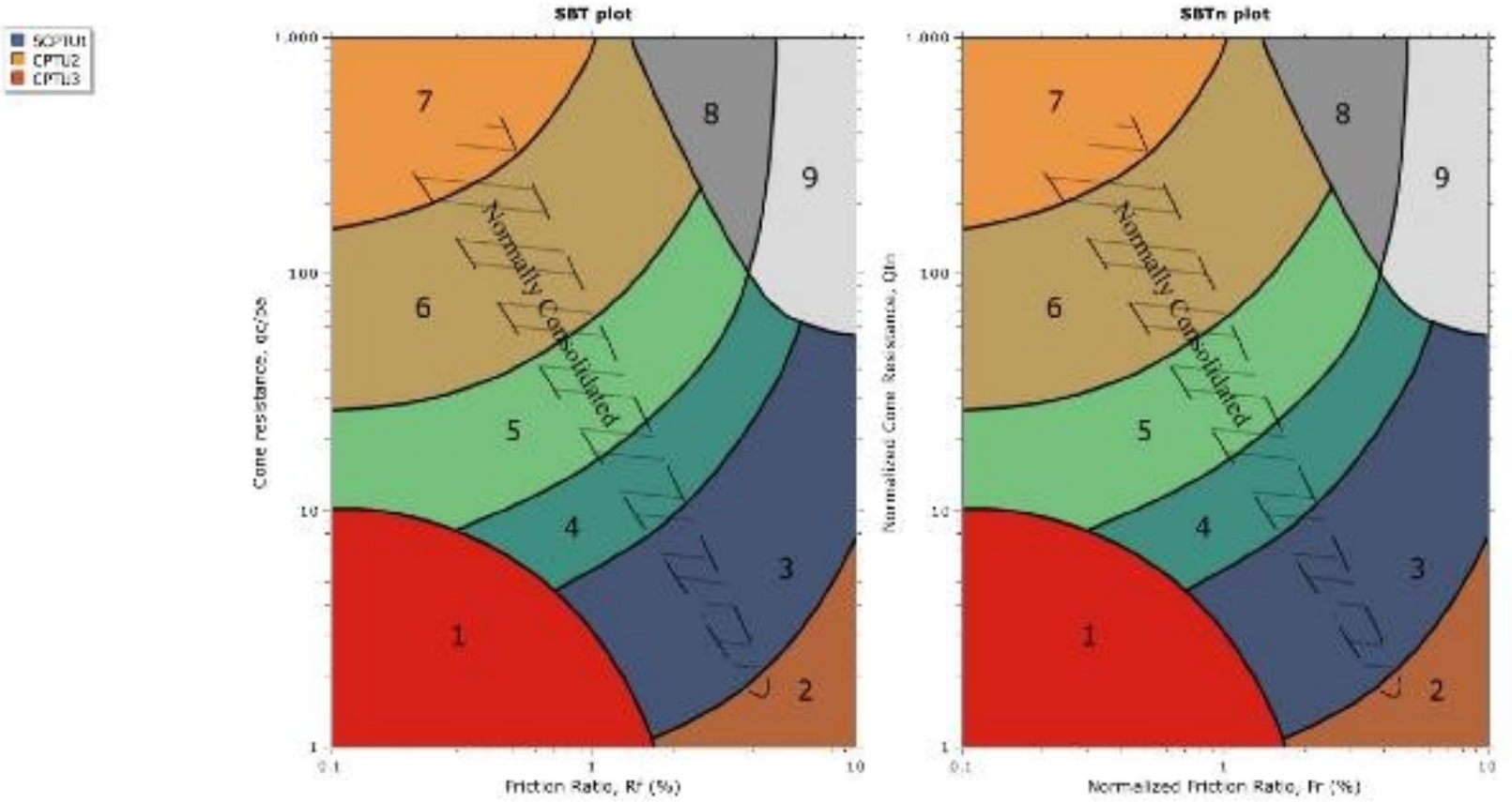
Normalized basic plots



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Project:
Location:

Soil Behavior Type Plots



ALLEGATO 2: LIQUEFAZIONE

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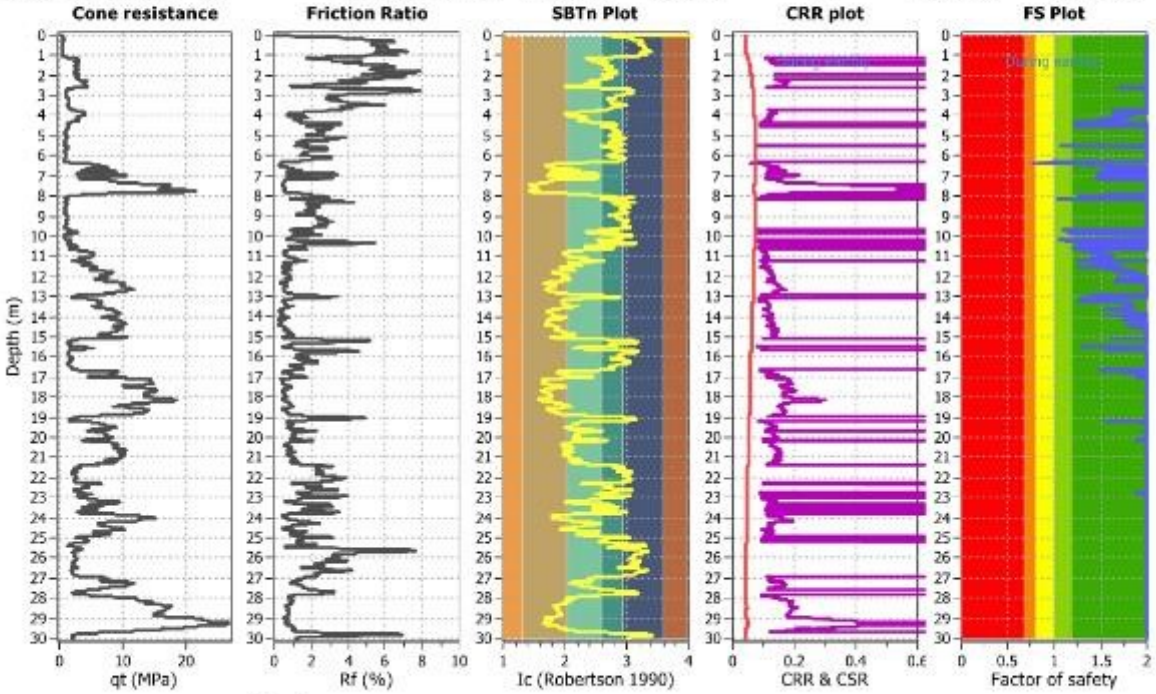
LIQUEFACTION ANALYSIS REPORT

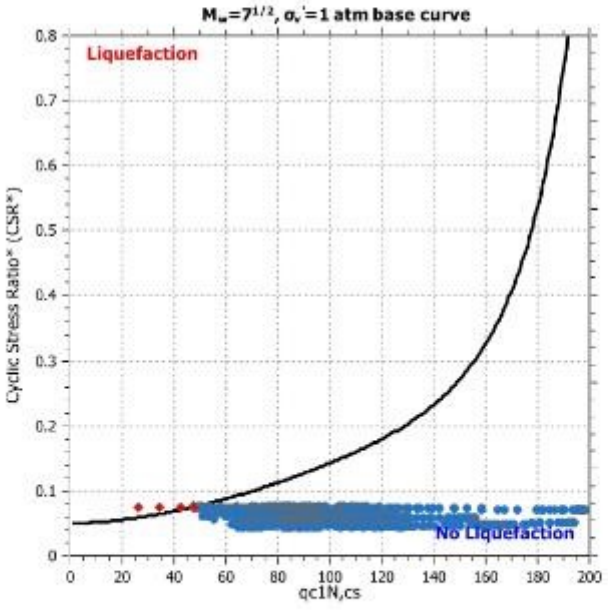
Project title : **Location :**

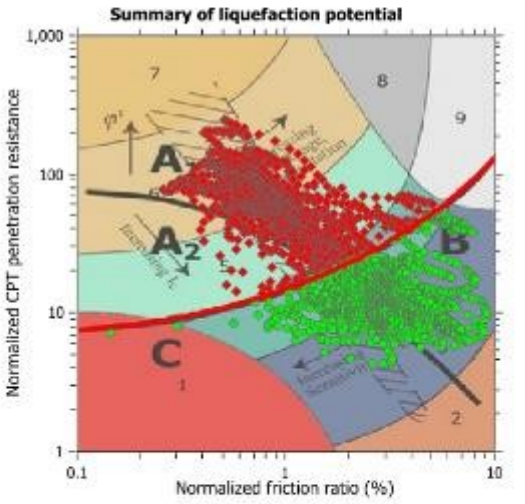
CPT file : SCPTU1 - Basic

Input parameters and analysis data

Analysis method:	I&B (2008)	G.W.T. (in-situ):	0.80 m	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	R&W (1998)	G.W.T. (earthq.):	0.80 m	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	5.45	Ic cut-off value:	2.60	Trans. detect. applied:	No	MSF method:	Method based
Peak ground acceleration:	0.12	Unit weight calculation:	Based on SBT	K_o applied:	Yes		

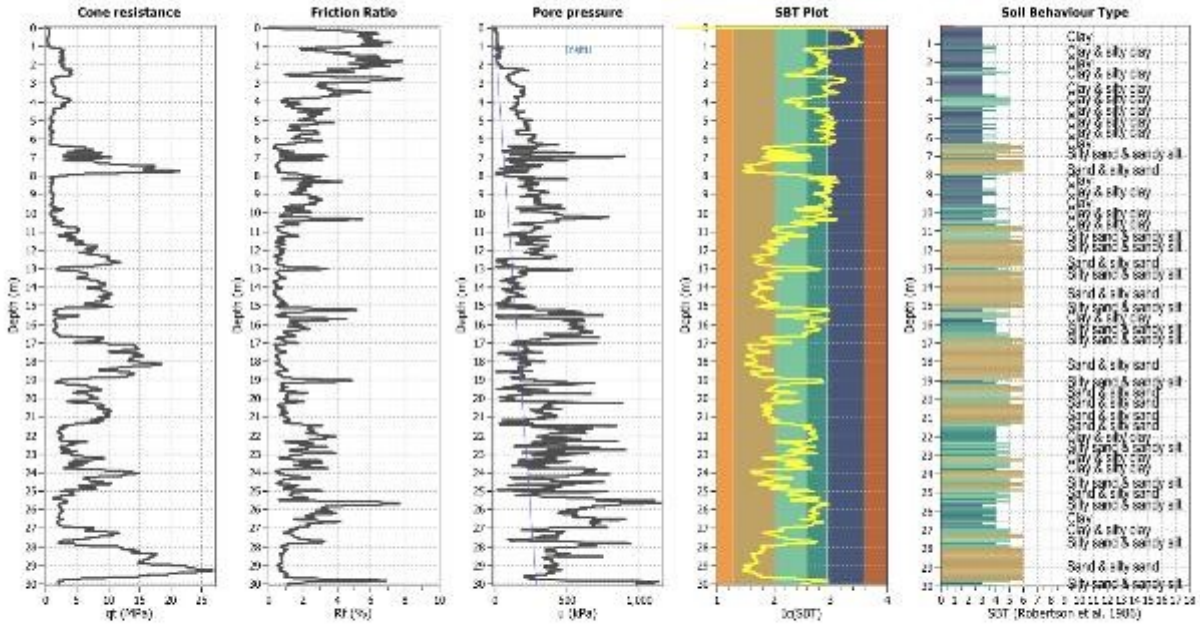






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



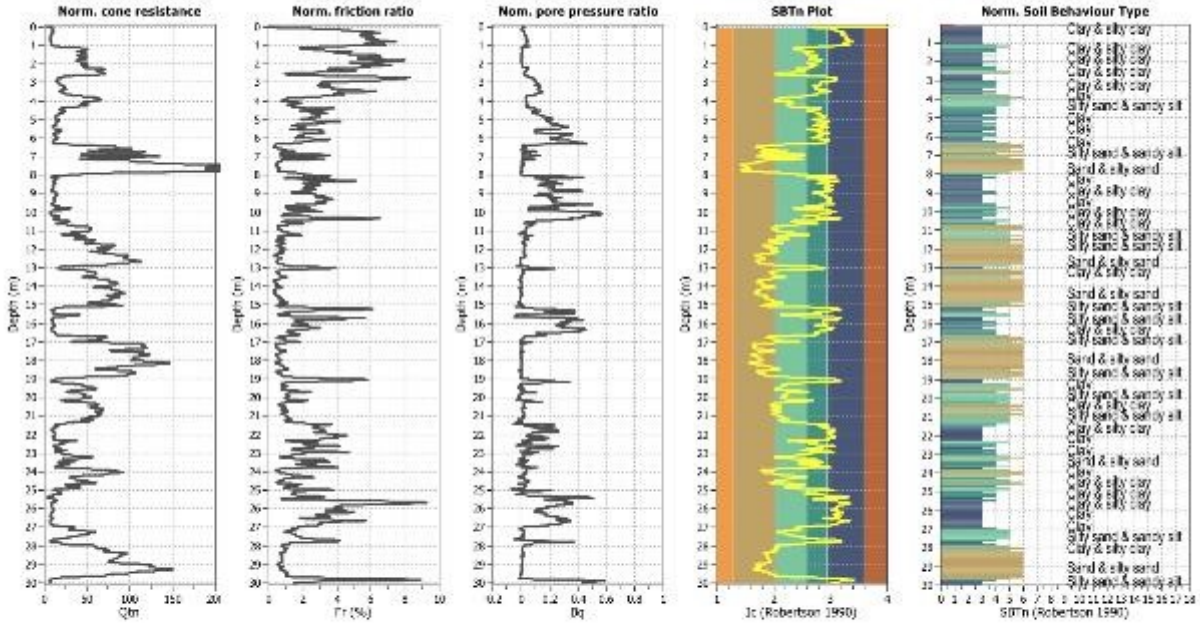
Input parameters and analysis data

Analysis method:	ISBI (2016)	Depth to GWT (erthq.):	0.80 m	Fill weight:	N/A
Flow correction method:	RAW (1998)	Average results interval:	3	Transition layers applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w:	5.45	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.12	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	0.80 m	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained	4. Clayey silt to silty clay	7. Gravelly sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

CPT basic interpretation plots (normalized)



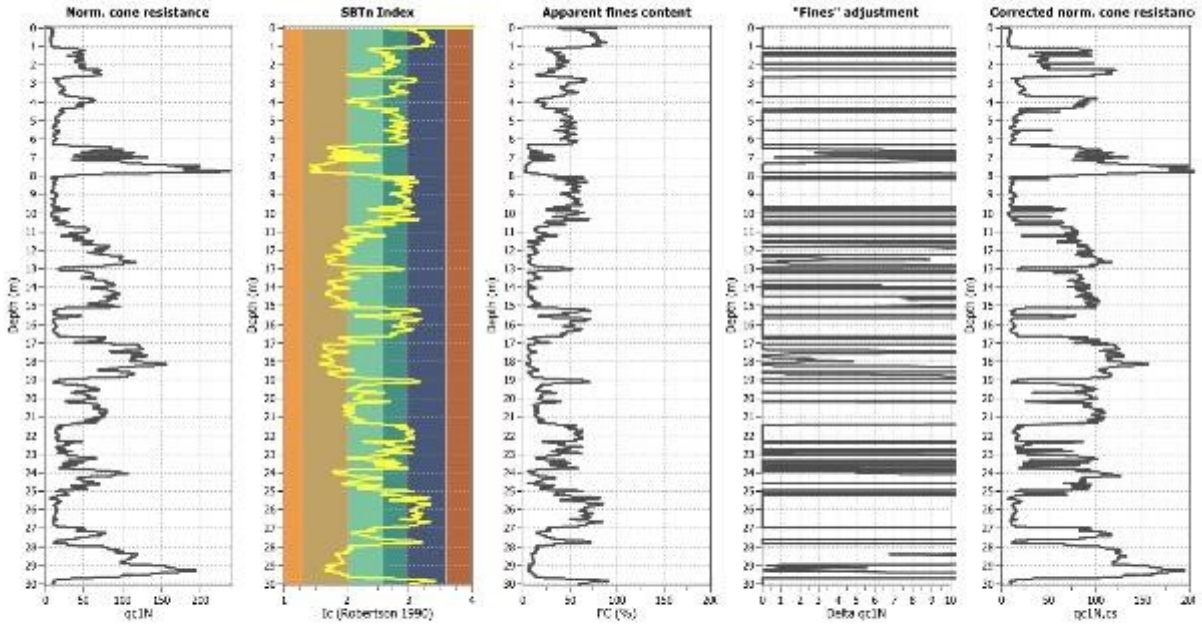
Input parameters and analysis data

Analysis method:	ISBI (2016)	Depth to GWT (erthq.):	0.80 m	Fill weight:	N/A
Flow correction method:	RAW (1998)	Average results interval:	3	Transition layers applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w:	5.45	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.12	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	0.80 m	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained	4. Clayey silt to silty clay	7. Gravelly sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

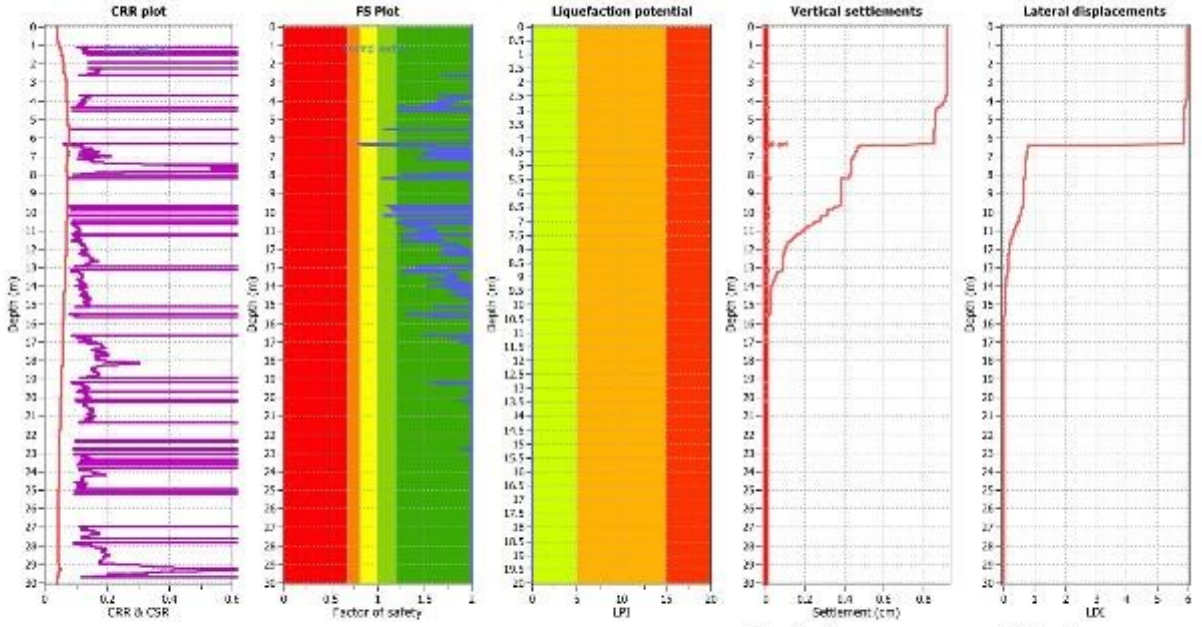
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	IBB (2016)	Depth to GWT (erthq.):	0.80 m	Fill weight:	N/A
Fines correction method:	RAW (1998)	Average results interval:	3	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w:	5.45	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.12	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	0.80 m	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	IBB (2016)	Depth to GWT (erthq.):	0.80 m	Fill weight:	N/A
Fines correction method:	RAW (1998)	Average results interval:	3	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w:	5.45	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.12	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	0.80 m	Fill height:	N/A	Limit depth:	N/A

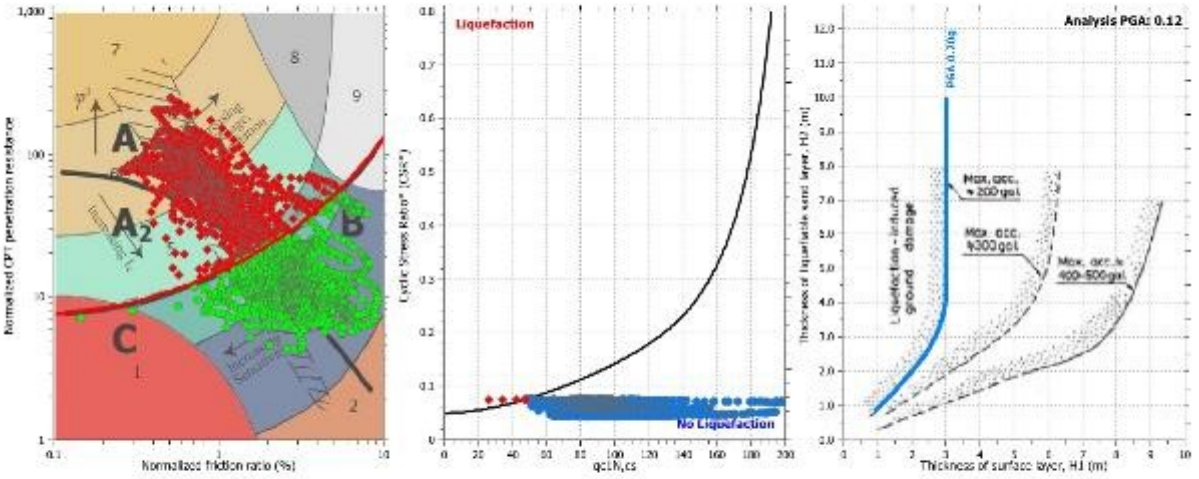
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlikely to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

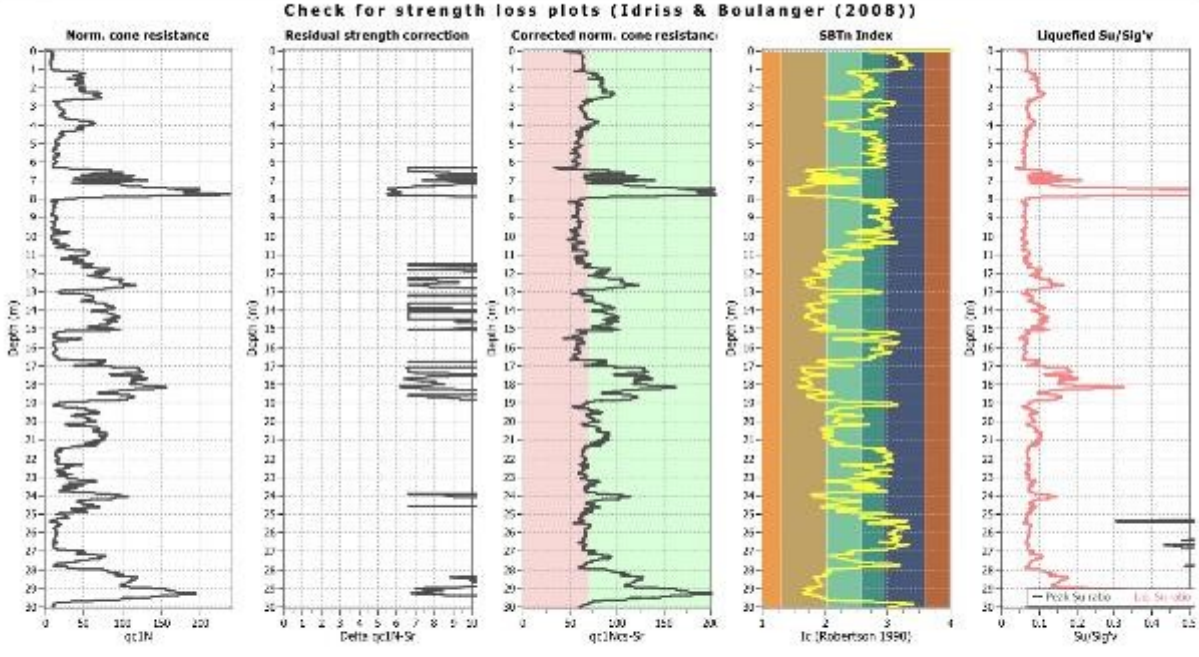
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	ISSMGE (2018)	Depth to GWT (erthq.):	0.80 m	Fill weight:	N/A
Fines correction method:	NAW (1998)	Average results interval:	3	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w:	5.45	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.12	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	0.80 m	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

Analysis method:	ISSMGE (2018)	Depth to GWT (erthq.):	0.80 m	Fill weight:	N/A
Fines correction method:	NAW (1998)	Average results interval:	3	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w:	5.45	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.12	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	0.80 m	Fill height:	N/A	Limit depth:	N/A

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
0.01	2.00	0.00	0.00	0.01	0.00	0.02	2.00	0.00	0.00	0.01	0.00
0.03	2.00	0.00	0.00	0.01	0.00	0.04	2.00	0.00	0.00	0.01	0.00
0.05	2.00	0.00	0.00	0.01	0.00	0.06	2.00	0.00	0.00	0.01	0.00
0.07	2.00	0.00	0.00	0.01	0.00	0.08	2.00	0.00	0.00	0.01	0.00
0.09	2.00	0.00	0.00	0.01	0.00	0.10	2.00	0.00	0.00	0.01	0.00
0.11	2.00	0.00	0.00	0.01	0.00	0.12	2.00	0.00	0.00	0.01	0.00
0.13	2.00	0.00	0.00	0.01	0.00	0.14	2.00	0.00	0.00	0.01	0.00
0.15	2.00	0.00	0.00	0.01	0.00	0.16	2.00	0.00	0.00	0.01	0.00
0.17	2.00	0.00	0.00	0.01	0.00	0.18	2.00	0.00	0.00	0.01	0.00
0.19	2.00	0.00	0.00	0.01	0.00	0.20	2.00	0.00	0.00	0.01	0.00
0.21	2.00	0.00	0.00	0.01	0.00	0.22	2.00	0.00	0.00	0.01	0.00
0.23	2.00	0.00	0.00	0.01	0.00	0.24	2.00	0.00	0.00	0.01	0.00
0.25	2.00	0.00	0.00	0.01	0.00	0.26	2.00	0.00	0.00	0.01	0.00
0.27	2.00	0.00	0.00	0.01	0.00	0.28	2.00	0.00	0.00	0.01	0.00
0.29	2.00	0.00	0.00	0.01	0.00	0.30	2.00	0.00	0.00	0.01	0.00
0.31	2.00	0.00	0.00	0.01	0.00	0.32	2.00	0.00	0.00	0.01	0.00
0.33	2.00	0.00	0.00	0.01	0.00	0.34	2.00	0.00	0.00	0.01	0.00
0.35	2.00	0.00	0.00	0.01	0.00	0.36	2.00	0.00	0.00	0.01	0.00
0.37	2.00	0.00	0.00	0.01	0.00	0.38	2.00	0.00	0.00	0.01	0.00
0.39	2.00	0.00	0.00	0.01	0.00	0.40	2.00	0.00	0.00	0.01	0.00
0.41	2.00	0.00	0.00	0.01	0.00	0.42	2.00	0.00	0.00	0.01	0.00
0.43	2.00	0.00	0.00	0.01	0.00	0.44	2.00	0.00	0.00	0.01	0.00
0.45	2.00	0.00	0.00	0.01	0.00	0.46	2.00	0.00	0.00	0.01	0.00
0.47	2.00	0.00	0.00	0.01	0.00	0.48	2.00	0.00	0.00	0.01	0.00
0.49	2.00	0.00	0.00	0.01	0.00	0.50	2.00	0.00	0.00	0.01	0.00
0.51	2.00	0.00	0.00	0.01	0.00	0.52	2.00	0.00	0.00	0.01	0.00
0.53	2.00	0.00	0.00	0.01	0.00	0.54	2.00	0.00	0.00	0.01	0.00
0.55	2.00	0.00	0.00	0.01	0.00	0.56	2.00	0.00	0.00	0.01	0.00
0.57	2.00	0.00	0.00	0.01	0.00	0.58	2.00	0.00	0.00	0.01	0.00
0.59	2.00	0.00	0.00	0.01	0.00	0.60	2.00	0.00	0.00	0.01	0.00
0.61	2.00	0.00	0.00	0.01	0.00	0.62	2.00	0.00	0.00	0.01	0.00
0.63	2.00	0.00	0.00	0.01	0.00	0.64	2.00	0.00	0.00	0.01	0.00
0.65	2.00	0.00	0.00	0.01	0.00	0.66	2.00	0.00	0.00	0.01	0.00
0.67	2.00	0.00	0.00	0.01	0.00	0.68	2.00	0.00	0.00	0.01	0.00
0.69	2.00	0.00	0.00	0.01	0.00	0.70	2.00	0.00	0.00	0.01	0.00
0.71	2.00	0.00	0.00	0.01	0.00	0.72	2.00	0.00	0.00	0.01	0.00
0.73	2.00	0.00	0.00	0.01	0.00	0.74	2.00	0.00	0.00	0.01	0.00
0.75	2.00	0.00	0.00	0.01	0.00	0.76	2.00	0.00	0.00	0.01	0.00
0.77	2.00	0.00	0.00	0.01	0.00	0.78	2.00	0.00	0.00	0.01	0.00
0.79	2.00	0.00	0.00	0.01	0.00	0.80	2.00	0.00	0.00	0.01	0.00
0.81	2.00	0.00	0.00	0.01	0.00	0.82	2.00	0.00	0.00	0.01	0.00
0.83	2.00	0.00	0.00	0.01	0.00	0.84	2.00	0.00	0.00	0.01	0.00
0.85	2.00	0.00	0.00	0.01	0.00	0.86	2.00	0.00	0.00	0.01	0.00
0.87	2.00	0.00	0.00	0.01	0.00	0.88	2.00	0.00	0.00	0.01	0.00
0.89	2.00	0.00	0.00	0.01	0.00	0.90	2.00	0.00	0.00	0.01	0.00
0.91	2.00	0.00	0.00	0.01	0.00	0.92	2.00	0.00	0.00	0.01	0.00
0.93	2.00	0.00	0.00	0.01	0.00	0.94	2.00	0.00	0.00	0.01	0.00
0.95	2.00	0.00	0.00	0.01	0.00	0.96	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
0.97	2.00	0.00	0.00	0.01	0.00	0.98	2.00	0.00	0.00	0.01	0.00
0.99	2.00	0.00	0.00	0.01	0.00	1.00	2.00	0.00	0.00	0.01	0.00
1.01	2.00	0.00	0.00	0.01	0.00	1.02	2.00	0.00	0.00	0.01	0.00
1.03	2.00	0.00	0.00	0.01	0.00	1.04	2.00	0.00	0.00	0.01	0.00
1.05	2.00	0.00	0.00	0.01	0.00	1.06	2.00	0.00	0.00	0.01	0.00
1.07	2.00	0.00	0.00	0.01	0.00	1.08	2.00	0.00	0.00	0.01	0.00
1.09	2.00	0.00	0.00	0.01	0.00	1.10	2.00	0.00	0.00	0.01	0.00
1.11	2.00	0.00	0.00	0.01	0.00	1.12	2.00	0.00	0.00	0.01	0.00
1.13	2.00	0.00	0.00	0.01	0.00	1.14	2.00	0.00	0.00	0.01	0.00
1.15	2.00	0.00	0.00	0.01	0.00	1.16	2.00	0.00	0.00	0.01	0.00
1.17	2.00	0.00	0.00	0.01	0.00	1.18	2.00	0.00	0.00	0.01	0.00
1.19	2.00	0.00	0.00	0.01	0.00	1.20	2.00	0.00	0.00	0.01	0.00
1.21	2.00	0.00	0.00	0.01	0.00	1.22	2.00	0.00	0.00	0.01	0.00
1.23	2.00	0.00	0.00	0.01	0.00	1.24	2.00	0.00	0.00	0.01	0.00
1.25	2.00	0.00	0.00	0.01	0.00	1.26	2.00	0.00	0.00	0.01	0.00
1.27	2.00	0.00	0.00	0.01	0.00	1.28	2.00	0.00	0.00	0.01	0.00
1.29	2.00	0.00	0.00	0.01	0.00	1.30	2.00	0.00	0.00	0.01	0.00
1.31	2.00	0.00	0.00	0.01	0.00	1.32	2.00	0.00	0.00	0.01	0.00
1.33	2.00	0.00	0.00	0.01	0.00	1.34	2.00	0.00	0.00	0.01	0.00
1.35	2.00	0.00	0.00	0.01	0.00	1.36	2.00	0.00	0.00	0.01	0.00
1.37	2.00	0.00	0.00	0.01	0.00	1.38	2.00	0.00	0.00	0.01	0.00
1.39	2.00	0.00	0.00	0.01	0.00	1.40	2.00	0.00	0.00	0.01	0.00
1.41	2.00	0.00	0.00	0.01	0.00	1.42	2.00	0.00	0.00	0.01	0.00
1.43	2.00	0.00	0.00	0.01	0.00	1.44	2.00	0.00	0.00	0.01	0.00
1.45	2.00	0.00	0.00	0.01	0.00	1.46	2.00	0.00	0.00	0.01	0.00
1.47	2.00	0.00	0.00	0.01	0.00	1.48	2.00	0.00	0.00	0.01	0.00
1.49	2.00	0.00	0.00	0.01	0.00	1.50	2.00	0.00	0.00	0.01	0.00
1.51	2.00	0.00	0.00	0.01	0.00	1.52	2.00	0.00	0.00	0.01	0.00
1.53	2.00	0.00	0.00	0.01	0.00	1.54	2.00	0.00	0.00	0.01	0.00
1.55	2.00	0.00	0.00	0.01	0.00	1.56	2.00	0.00	0.00	0.01	0.00
1.57	2.00	0.00	0.00	0.01	0.00	1.58	2.00	0.00	0.00	0.01	0.00
1.59	2.00	0.00	0.00	0.01	0.00	1.60	2.00	0.00	0.00	0.01	0.00
1.61	2.00	0.00	0.00	0.01	0.00	1.62	2.00	0.00	0.00	0.01	0.00
1.63	2.00	0.00	0.00	0.01	0.00	1.64	2.00	0.00	0.00	0.01	0.00
1.65	2.00	0.00	0.00	0.01	0.00	1.66	2.00	0.00	0.00	0.01	0.00
1.67	2.00	0.00	0.00	0.01	0.00	1.68	2.00	0.00	0.00	0.01	0.00
1.69	2.00	0.00	0.00	0.01	0.00	1.70	2.00	0.00	0.00	0.01	0.00
1.71	2.00	0.00	0.00	0.01	0.00	1.72	2.00	0.00	0.00	0.01	0.00
1.73	2.00	0.00	0.00	0.01	0.00	1.74	2.00	0.00	0.00	0.01	0.00
1.75	2.00	0.00	0.00	0.01	0.00	1.76	2.00	0.00	0.00	0.01	0.00
1.77	2.00	0.00	0.00	0.01	0.00	1.78	2.00	0.00	0.00	0.01	0.00
1.79	2.00	0.00	0.00	0.01	0.00	1.80	2.00	0.00	0.00	0.01	0.00
1.81	2.00	0.00	0.00	0.01	0.00	1.82	2.00	0.00	0.00	0.01	0.00
1.83	2.00	0.00	0.00	0.01	0.00	1.84	2.00	0.00	0.00	0.01	0.00
1.85	2.00	0.00	0.00	0.01	0.00	1.86	2.00	0.00	0.00	0.01	0.00
1.87	2.00	0.00	0.00	0.01	0.00	1.88	2.00	0.00	0.00	0.01	0.00
1.89	2.00	0.00	0.00	0.01	0.00	1.90	2.00	0.00	0.00	0.01	0.00
1.91	2.00	0.00	0.00	0.01	0.00	1.92	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
1.93	2.00	0.00	0.00	0.01	0.00	1.94	2.00	0.00	0.00	0.01	0.00
1.95	2.00	0.00	0.00	0.01	0.00	1.96	2.00	0.00	0.00	0.01	0.00
1.97	2.00	0.00	0.00	0.01	0.00	1.98	2.00	0.00	0.00	0.01	0.00
1.99	2.00	0.00	0.00	0.01	0.00	2.00	2.00	0.00	0.00	0.01	0.00
2.01	2.00	0.00	0.00	0.01	0.00	2.02	2.00	0.00	0.00	0.01	0.00
2.03	2.00	0.00	0.00	0.01	0.00	2.04	2.00	0.00	0.00	0.01	0.00
2.05	2.00	0.00	0.00	0.01	0.00	2.06	2.00	0.00	0.00	0.01	0.00
2.07	2.00	0.00	0.00	0.01	0.00	2.08	2.00	0.00	0.00	0.01	0.00
2.09	2.00	0.00	0.00	0.01	0.00	2.10	2.00	0.00	0.00	0.01	0.00
2.11	2.00	0.00	0.00	0.01	0.00	2.12	2.00	0.00	0.00	0.01	0.00
2.13	2.00	0.00	0.00	0.01	0.00	2.14	2.00	0.00	0.00	0.01	0.00
2.15	2.00	0.00	0.00	0.01	0.00	2.16	2.00	0.00	0.00	0.01	0.00
2.17	2.00	0.00	0.00	0.01	0.00	2.18	2.00	0.00	0.00	0.01	0.00
2.19	2.00	0.00	0.00	0.01	0.00	2.20	2.00	0.00	0.00	0.01	0.00
2.21	2.00	0.00	0.00	0.01	0.00	2.22	2.00	0.00	0.00	0.01	0.00
2.23	2.00	0.00	0.00	0.01	0.00	2.24	2.00	0.00	0.00	0.01	0.00
2.25	2.00	0.00	0.00	0.01	0.00	2.26	2.00	0.00	0.00	0.01	0.00
2.27	2.00	0.00	0.00	0.01	0.00	2.28	2.00	0.00	0.00	0.01	0.00
2.29	2.00	0.00	0.00	0.01	0.00	2.30	2.00	0.00	0.00	0.01	0.00
2.31	2.00	0.00	0.00	0.01	0.00	2.32	2.00	0.00	0.00	0.01	0.00
2.33	2.00	0.00	0.00	0.01	0.00	2.34	2.00	0.00	0.00	0.01	0.00
2.35	2.00	0.00	0.00	0.01	0.00	2.36	2.00	0.00	0.00	0.01	0.00
2.37	2.00	0.00	0.00	0.01	0.00	2.38	2.00	0.00	0.00	0.01	0.00
2.39	2.00	0.00	0.00	0.01	0.00	2.40	2.00	0.00	0.00	0.01	0.00
2.41	2.00	0.00	0.00	0.01	0.00	2.42	2.00	0.00	0.00	0.01	0.00
2.43	2.00	0.00	0.00	0.01	0.00	2.44	2.00	0.00	0.00	0.01	0.00
2.45	2.00	0.00	0.00	0.01	0.00	2.46	2.00	0.00	0.00	0.01	0.00
2.47	2.00	0.00	0.00	0.01	0.00	2.48	2.00	0.00	0.00	0.01	0.00
2.49	2.00	0.00	0.00	0.01	0.00	2.50	2.00	0.00	0.00	0.01	0.00
2.51	2.00	0.00	0.00	0.01	0.00	2.52	2.00	0.00	0.00	0.01	0.00
2.53	2.00	0.00	0.00	0.01	0.00	2.54	2.00	0.00	0.00	0.01	0.00
2.55	2.00	0.00	0.00	0.01	0.00	2.56	2.00	0.00	0.00	0.01	0.00
2.57	2.00	0.00	0.00	0.01	0.00	2.58	2.00	0.00	0.00	0.01	0.00
2.59	2.00	0.00	0.00	0.01	0.00	2.60	1.82	0.00	0.00	0.01	0.00
2.61	1.78	0.00	0.00	0.01	0.00	2.62	1.73	0.00	0.00	0.01	0.00
2.63	1.68	0.00	0.00	0.01	0.00	2.64	2.00	0.00	0.00	0.01	0.00
2.65	2.00	0.00	0.00	0.01	0.00	2.66	2.00	0.00	0.00	0.01	0.00
2.67	2.00	0.00	0.00	0.01	0.00	2.68	2.00	0.00	0.00	0.01	0.00
2.69	2.00	0.00	0.00	0.01	0.00	2.70	2.00	0.00	0.00	0.01	0.00
2.71	2.00	0.00	0.00	0.01	0.00	2.72	2.00	0.00	0.00	0.01	0.00
2.73	2.00	0.00	0.00	0.01	0.00	2.74	2.00	0.00	0.00	0.01	0.00
2.75	2.00	0.00	0.00	0.01	0.00	2.76	2.00	0.00	0.00	0.01	0.00
2.77	2.00	0.00	0.00	0.01	0.00	2.78	2.00	0.00	0.00	0.01	0.00
2.79	2.00	0.00	0.00	0.01	0.00	2.80	2.00	0.00	0.00	0.01	0.00
2.81	2.00	0.00	0.00	0.01	0.00	2.82	2.00	0.00	0.00	0.01	0.00
2.83	2.00	0.00	0.00	0.01	0.00	2.84	2.00	0.00	0.00	0.01	0.00
2.85	2.00	0.00	0.00	0.01	0.00	2.86	2.00	0.00	0.00	0.01	0.00
2.87	2.00	0.00	0.00	0.01	0.00	2.88	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
2.89	2.00	0.00	0.00	0.01	0.00	2.90	2.00	0.00	0.00	0.01	0.00
2.91	2.00	0.00	0.00	0.01	0.00	2.92	2.00	0.00	0.00	0.01	0.00
2.93	2.00	0.00	0.00	0.01	0.00	2.94	2.00	0.00	0.00	0.01	0.00
2.95	2.00	0.00	0.00	0.01	0.00	2.96	2.00	0.00	0.00	0.01	0.00
2.97	2.00	0.00	0.00	0.01	0.00	2.98	2.00	0.00	0.00	0.01	0.00
2.99	2.00	0.00	0.00	0.01	0.00	3.00	2.00	0.00	0.00	0.01	0.00
3.01	2.00	0.00	0.00	0.01	0.00	3.02	2.00	0.00	0.00	0.01	0.00
3.03	2.00	0.00	0.00	0.01	0.00	3.04	2.00	0.00	0.00	0.01	0.00
3.05	2.00	0.00	0.00	0.01	0.00	3.06	2.00	0.00	0.00	0.01	0.00
3.07	2.00	0.00	0.00	0.01	0.00	3.08	2.00	0.00	0.00	0.01	0.00
3.09	2.00	0.00	0.00	0.01	0.00	3.10	2.00	0.00	0.00	0.01	0.00
3.11	2.00	0.00	0.00	0.01	0.00	3.12	2.00	0.00	0.00	0.01	0.00
3.13	2.00	0.00	0.00	0.01	0.00	3.14	2.00	0.00	0.00	0.01	0.00
3.15	2.00	0.00	0.00	0.01	0.00	3.16	2.00	0.00	0.00	0.01	0.00
3.17	2.00	0.00	0.00	0.01	0.00	3.18	2.00	0.00	0.00	0.01	0.00
3.19	2.00	0.00	0.00	0.01	0.00	3.20	2.00	0.00	0.00	0.01	0.00
3.21	2.00	0.00	0.00	0.01	0.00	3.22	2.00	0.00	0.00	0.01	0.00
3.23	2.00	0.00	0.00	0.01	0.00	3.24	2.00	0.00	0.00	0.01	0.00
3.25	2.00	0.00	0.00	0.01	0.00	3.26	2.00	0.00	0.00	0.01	0.00
3.27	2.00	0.00	0.00	0.01	0.00	3.28	2.00	0.00	0.00	0.01	0.00
3.29	2.00	0.00	0.00	0.01	0.00	3.30	2.00	0.00	0.00	0.01	0.00
3.31	2.00	0.00	0.00	0.01	0.00	3.32	2.00	0.00	0.00	0.01	0.00
3.33	2.00	0.00	0.00	0.01	0.00	3.34	2.00	0.00	0.00	0.01	0.00
3.35	2.00	0.00	0.00	0.01	0.00	3.36	2.00	0.00	0.00	0.01	0.00
3.37	2.00	0.00	0.00	0.01	0.00	3.38	2.00	0.00	0.00	0.01	0.00
3.39	2.00	0.00	0.00	0.01	0.00	3.40	2.00	0.00	0.00	0.01	0.00
3.41	2.00	0.00	0.00	0.01	0.00	3.42	2.00	0.00	0.00	0.01	0.00
3.43	2.00	0.00	0.00	0.01	0.00	3.44	2.00	0.00	0.00	0.01	0.00
3.45	2.00	0.00	0.00	0.01	0.00	3.46	2.00	0.00	0.00	0.01	0.00
3.47	2.00	0.00	0.00	0.01	0.00	3.48	2.00	0.00	0.00	0.01	0.00
3.49	2.00	0.00	0.00	0.01	0.00	3.50	2.00	0.00	0.00	0.01	0.00
3.51	2.00	0.00	0.00	0.01	0.00	3.52	2.00	0.00	0.00	0.01	0.00
3.53	2.00	0.00	0.00	0.01	0.00	3.54	2.00	0.00	0.00	0.01	0.00
3.55	2.00	0.00	0.00	0.01	0.00	3.56	2.00	0.00	0.00	0.01	0.00
3.57	2.00	0.00	0.00	0.01	0.00	3.58	2.00	0.00	0.00	0.01	0.00
3.59	2.00	0.00	0.00	0.01	0.00	3.60	2.00	0.00	0.00	0.01	0.00
3.61	2.00	0.00	0.00	0.01	0.00	3.62	2.00	0.00	0.00	0.01	0.00
3.63	2.00	0.00	0.00	0.01	0.00	3.64	2.00	0.00	0.00	0.01	0.00
3.65	2.00	0.00	0.00	0.01	0.00	3.66	2.00	0.00	0.00	0.01	0.00
3.67	2.00	0.00	0.00	0.01	0.00	3.68	2.00	0.00	0.00	0.01	0.00
3.69	2.00	0.00	0.00	0.01	0.00	3.70	2.00	0.00	0.00	0.01	0.00
3.71	2.00	0.00	0.00	0.01	0.00	3.72	1.63	0.00	0.00	0.01	0.00
3.73	1.67	0.00	0.00	0.01	0.00	3.74	1.68	0.00	0.00	0.01	0.00
3.75	1.70	0.00	0.00	0.01	0.00	3.76	1.79	0.00	0.00	0.01	0.00
3.77	1.85	0.00	0.00	0.01	0.00	3.78	1.92	0.00	0.00	0.01	0.00
3.79	1.97	0.00	0.00	0.01	0.00	3.80	2.00	0.00	0.00	0.01	0.00
3.81	2.00	0.00	0.00	0.01	0.00	3.82	2.00	0.00	0.00	0.01	0.00
3.83	2.00	0.00	0.00	0.01	0.00	3.84	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
3.85	2.00	0.00	0.00	0.01	0.00	3.86	1.96	0.00	0.00	0.01	0.00
3.87	1.89	0.00	0.00	0.01	0.00	3.88	1.82	0.00	0.00	0.01	0.00
3.89	1.78	0.00	0.00	0.01	0.00	3.90	1.77	0.00	0.00	0.01	0.00
3.91	1.79	0.00	0.00	0.01	0.00	3.92	1.79	0.00	0.00	0.01	0.00
3.93	1.83	0.00	0.00	0.01	0.00	3.94	1.85	0.00	0.00	0.01	0.00
3.95	1.87	0.00	0.00	0.01	0.00	3.96	1.85	0.00	0.00	0.01	0.00
3.97	1.82	0.00	0.00	0.01	0.00	3.98	1.73	0.00	0.00	0.01	0.00
3.99	1.65	0.00	0.00	0.01	0.00	4.00	1.63	0.00	0.00	0.01	0.00
4.01	1.67	0.00	0.00	0.01	0.00	4.02	1.69	0.00	0.00	0.01	0.00
4.03	1.70	0.00	0.00	0.01	0.00	4.04	1.71	0.00	0.00	0.01	0.00
4.05	1.70	0.00	0.00	0.01	0.00	4.06	1.68	0.00	0.00	0.01	0.00
4.07	1.67	0.00	0.00	0.01	0.00	4.08	1.64	0.00	0.00	0.01	0.00
4.09	1.63	0.00	0.00	0.01	0.00	4.10	1.66	0.00	0.00	0.01	0.00
4.11	1.72	0.00	0.00	0.01	0.00	4.12	1.78	0.00	0.00	0.01	0.00
4.13	1.77	0.00	0.00	0.01	0.00	4.14	1.75	0.00	0.00	0.01	0.00
4.15	1.71	0.00	0.00	0.01	0.00	4.16	1.63	0.00	0.00	0.01	0.00
4.17	1.60	0.00	0.00	0.01	0.00	4.18	1.54	0.00	0.00	0.01	0.00
4.19	1.51	0.00	0.00	0.01	0.00	4.20	1.50	0.00	0.00	0.01	0.00
4.21	1.53	0.00	0.00	0.01	0.00	4.22	1.54	0.00	0.00	0.01	0.00
4.23	1.63	0.00	0.00	0.01	0.00	4.24	1.68	0.00	0.00	0.01	0.00
4.25	1.72	0.00	0.00	0.01	0.00	4.26	1.73	0.00	0.00	0.01	0.00
4.27	1.72	0.00	0.00	0.01	0.00	4.28	1.64	0.00	0.00	0.01	0.00
4.29	1.60	0.00	0.00	0.01	0.00	4.30	1.55	0.00	0.00	0.01	0.00
4.31	1.50	0.00	0.00	0.01	0.00	4.32	1.39	0.00	0.00	0.01	0.00
4.33	1.34	0.00	0.00	0.01	0.00	4.34	1.29	0.00	0.00	0.01	0.00
4.35	1.25	0.00	0.00	0.01	0.00	4.36	1.22	0.00	0.00	0.01	0.00
4.37	2.00	0.00	0.00	0.01	0.00	4.38	2.00	0.00	0.00	0.01	0.00
4.39	2.00	0.00	0.00	0.01	0.00	4.40	2.00	0.00	0.00	0.01	0.00
4.41	2.00	0.00	0.00	0.01	0.00	4.42	2.00	0.00	0.00	0.01	0.00
4.43	2.00	0.00	0.00	0.01	0.00	4.44	2.00	0.00	0.00	0.01	0.00
4.45	2.00	0.00	0.00	0.01	0.00	4.46	2.00	0.00	0.00	0.01	0.00
4.47	2.00	0.00	0.00	0.01	0.00	4.48	2.00	0.00	0.00	0.01	0.00
4.49	2.00	0.00	0.00	0.01	0.00	4.50	2.00	0.00	0.00	0.01	0.00
4.51	2.00	0.00	0.00	0.01	0.00	4.52	2.00	0.00	0.00	0.01	0.00
4.53	1.22	0.00	0.00	0.01	0.00	4.54	1.23	0.00	0.00	0.01	0.00
4.55	2.00	0.00	0.00	0.01	0.00	4.56	2.00	0.00	0.00	0.01	0.00
4.57	2.00	0.00	0.00	0.01	0.00	4.58	2.00	0.00	0.00	0.01	0.00
4.59	2.00	0.00	0.00	0.01	0.00	4.60	2.00	0.00	0.00	0.01	0.00
4.61	2.00	0.00	0.00	0.01	0.00	4.62	2.00	0.00	0.00	0.01	0.00
4.63	2.00	0.00	0.00	0.01	0.00	4.64	2.00	0.00	0.00	0.01	0.00
4.65	2.00	0.00	0.00	0.01	0.00	4.66	2.00	0.00	0.00	0.01	0.00
4.67	2.00	0.00	0.00	0.01	0.00	4.68	2.00	0.00	0.00	0.01	0.00
4.69	2.00	0.00	0.00	0.01	0.00	4.70	2.00	0.00	0.00	0.01	0.00
4.71	2.00	0.00	0.00	0.01	0.00	4.72	2.00	0.00	0.00	0.01	0.00
4.73	2.00	0.00	0.00	0.01	0.00	4.74	2.00	0.00	0.00	0.01	0.00
4.75	2.00	0.00	0.00	0.01	0.00	4.76	2.00	0.00	0.00	0.01	0.00
4.77	2.00	0.00	0.00	0.01	0.00	4.78	2.00	0.00	0.00	0.01	0.00
4.79	2.00	0.00	0.00	0.01	0.00	4.80	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
4.81	2.00	0.00	0.00	0.01	0.00	4.82	2.00	0.00	0.00	0.01	0.00
4.83	2.00	0.00	0.00	0.01	0.00	4.84	2.00	0.00	0.00	0.01	0.00
4.85	2.00	0.00	0.00	0.01	0.00	4.86	2.00	0.00	0.00	0.01	0.00
4.87	2.00	0.00	0.00	0.01	0.00	4.88	2.00	0.00	0.00	0.01	0.00
4.89	2.00	0.00	0.00	0.01	0.00	4.90	2.00	0.00	0.00	0.01	0.00
4.91	2.00	0.00	0.00	0.01	0.00	4.92	2.00	0.00	0.00	0.01	0.00
4.93	2.00	0.00	0.00	0.01	0.00	4.94	2.00	0.00	0.00	0.01	0.00
4.95	2.00	0.00	0.00	0.01	0.00	4.96	2.00	0.00	0.00	0.01	0.00
4.97	2.00	0.00	0.00	0.01	0.00	4.98	2.00	0.00	0.00	0.01	0.00
4.99	2.00	0.00	0.00	0.01	0.00	5.00	2.00	0.00	0.00	0.01	0.00
5.01	2.00	0.00	0.00	0.01	0.00	5.02	2.00	0.00	0.00	0.01	0.00
5.03	2.00	0.00	0.00	0.01	0.00	5.04	2.00	0.00	0.00	0.01	0.00
5.05	2.00	0.00	0.00	0.01	0.00	5.06	2.00	0.00	0.00	0.01	0.00
5.07	2.00	0.00	0.00	0.01	0.00	5.08	2.00	0.00	0.00	0.01	0.00
5.09	2.00	0.00	0.00	0.01	0.00	5.10	2.00	0.00	0.00	0.01	0.00
5.11	2.00	0.00	0.00	0.01	0.00	5.12	2.00	0.00	0.00	0.01	0.00
5.13	2.00	0.00	0.00	0.01	0.00	5.14	2.00	0.00	0.00	0.01	0.00
5.15	2.00	0.00	0.00	0.01	0.00	5.16	2.00	0.00	0.00	0.01	0.00
5.17	2.00	0.00	0.00	0.01	0.00	5.18	2.00	0.00	0.00	0.01	0.00
5.19	2.00	0.00	0.00	0.01	0.00	5.20	2.00	0.00	0.00	0.01	0.00
5.21	2.00	0.00	0.00	0.01	0.00	5.22	2.00	0.00	0.00	0.01	0.00
5.23	2.00	0.00	0.00	0.01	0.00	5.24	2.00	0.00	0.00	0.01	0.00
5.25	2.00	0.00	0.00	0.01	0.00	5.26	2.00	0.00	0.00	0.01	0.00
5.27	2.00	0.00	0.00	0.01	0.00	5.28	2.00	0.00	0.00	0.01	0.00
5.29	2.00	0.00	0.00	0.01	0.00	5.30	2.00	0.00	0.00	0.01	0.00
5.31	2.00	0.00	0.00	0.01	0.00	5.32	2.00	0.00	0.00	0.01	0.00
5.33	2.00	0.00	0.00	0.01	0.00	5.34	2.00	0.00	0.00	0.01	0.00
5.35	2.00	0.00	0.00	0.01	0.00	5.36	2.00	0.00	0.00	0.01	0.00
5.37	2.00	0.00	0.00	0.01	0.00	5.38	2.00	0.00	0.00	0.01	0.00
5.39	2.00	0.00	0.00	0.01	0.00	5.40	2.00	0.00	0.00	0.01	0.00
5.41	2.00	0.00	0.00	0.01	0.00	5.42	2.00	0.00	0.00	0.01	0.00
5.43	2.00	0.00	0.00	0.01	0.00	5.44	2.00	0.00	0.00	0.01	0.00
5.45	2.00	0.00	0.00	0.01	0.00	5.46	2.00	0.00	0.00	0.01	0.00
5.47	2.00	0.00	0.00	0.01	0.00	5.48	2.00	0.00	0.00	0.01	0.00
5.49	2.00	0.00	0.00	0.01	0.00	5.50	2.00	0.00	0.00	0.01	0.00
5.51	2.00	0.00	0.00	0.01	0.00	5.52	2.00	0.00	0.00	0.01	0.00
5.53	1.08	0.00	0.00	0.01	0.00	5.54	2.00	0.00	0.00	0.01	0.00
5.55	2.00	0.00	0.00	0.01	0.00	5.56	2.00	0.00	0.00	0.01	0.00
5.57	2.00	0.00	0.00	0.01	0.00	5.58	2.00	0.00	0.00	0.01	0.00
5.59	2.00	0.00	0.00	0.01	0.00	5.60	2.00	0.00	0.00	0.01	0.00
5.61	2.00	0.00	0.00	0.01	0.00	5.62	2.00	0.00	0.00	0.01	0.00
5.63	2.00	0.00	0.00	0.01	0.00	5.64	2.00	0.00	0.00	0.01	0.00
5.65	2.00	0.00	0.00	0.01	0.00	5.66	2.00	0.00	0.00	0.01	0.00
5.67	2.00	0.00	0.00	0.01	0.00	5.68	2.00	0.00	0.00	0.01	0.00
5.69	2.00	0.00	0.00	0.01	0.00	5.70	2.00	0.00	0.00	0.01	0.00
5.71	2.00	0.00	0.00	0.01	0.00	5.72	2.00	0.00	0.00	0.01	0.00
5.73	2.00	0.00	0.00	0.01	0.00	5.74	2.00	0.00	0.00	0.01	0.00
5.75	2.00	0.00	0.00	0.01	0.00	5.76	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
5.77	2.00	0.00	0.00	0.01	0.00	5.78	2.00	0.00	0.00	0.01	0.00
5.79	2.00	0.00	0.00	0.01	0.00	5.80	2.00	0.00	0.00	0.01	0.00
5.81	2.00	0.00	0.00	0.01	0.00	5.82	2.00	0.00	0.00	0.01	0.00
5.83	2.00	0.00	0.00	0.01	0.00	5.84	2.00	0.00	0.00	0.01	0.00
5.85	2.00	0.00	0.00	0.01	0.00	5.86	2.00	0.00	0.00	0.01	0.00
5.87	2.00	0.00	0.00	0.01	0.00	5.88	2.00	0.00	0.00	0.01	0.00
5.89	2.00	0.00	0.00	0.01	0.00	5.90	2.00	0.00	0.00	0.01	0.00
5.91	2.00	0.00	0.00	0.01	0.00	5.92	2.00	0.00	0.00	0.01	0.00
5.93	2.00	0.00	0.00	0.01	0.00	5.94	2.00	0.00	0.00	0.01	0.00
5.95	2.00	0.00	0.00	0.01	0.00	5.96	2.00	0.00	0.00	0.01	0.00
5.97	2.00	0.00	0.00	0.01	0.00	5.98	2.00	0.00	0.00	0.01	0.00
5.99	2.00	0.00	0.00	0.01	0.00	6.00	2.00	0.00	0.00	0.01	0.00
6.01	2.00	0.00	0.00	0.01	0.00	6.02	2.00	0.00	0.00	0.01	0.00
6.03	2.00	0.00	0.00	0.01	0.00	6.04	2.00	0.00	0.00	0.01	0.00
6.05	2.00	0.00	0.00	0.01	0.00	6.06	2.00	0.00	0.00	0.01	0.00
6.07	2.00	0.00	0.00	0.01	0.00	6.08	2.00	0.00	0.00	0.01	0.00
6.09	2.00	0.00	0.00	0.01	0.00	6.10	2.00	0.00	0.00	0.01	0.00
6.11	2.00	0.00	0.00	0.01	0.00	6.12	2.00	0.00	0.00	0.01	0.00
6.13	2.00	0.00	0.00	0.01	0.00	6.14	2.00	0.00	0.00	0.01	0.00
6.15	2.00	0.00	0.00	0.01	0.00	6.16	2.00	0.00	0.00	0.01	0.00
6.17	2.00	0.00	0.00	0.01	0.00	6.18	2.00	0.00	0.00	0.01	0.00
6.19	2.00	0.00	0.00	0.01	0.00	6.20	2.00	0.00	0.00	0.01	0.00
6.21	2.00	0.00	0.00	0.01	0.00	6.22	2.00	0.00	0.00	0.01	0.00
6.23	2.00	0.00	0.00	0.01	0.00	6.24	2.00	0.00	0.00	0.01	0.00
6.25	2.00	0.00	0.00	0.01	0.00	6.26	2.00	0.00	0.00	0.01	0.00
6.27	2.00	0.00	0.00	0.01	0.00	6.28	2.00	0.00	0.00	0.01	0.00
6.29	2.00	0.00	0.00	0.01	0.00	6.30	2.00	0.00	0.00	0.01	0.00
6.31	2.00	0.00	0.00	0.01	0.00	6.32	0.99	0.00	0.00	0.01	0.00
6.33	1.03	0.00	0.00	0.01	0.00	6.34	0.78	0.00	0.00	0.01	0.02
6.35	0.85	0.00	0.00	0.01	0.01	6.36	0.94	0.00	0.00	0.01	0.00
6.37	1.00	0.00	0.00	0.01	0.00	6.38	1.04	0.00	0.00	0.01	0.00
6.39	1.08	0.00	0.00	0.01	0.00	6.40	1.14	0.00	0.00	0.01	0.00
6.41	1.24	0.00	0.00	0.01	0.00	6.42	1.41	0.00	0.00	0.01	0.00
6.43	1.47	0.00	0.00	0.01	0.00	6.44	1.53	0.00	0.00	0.01	0.00
6.45	1.57	0.00	0.00	0.01	0.00	6.46	1.59	0.00	0.00	0.01	0.00
6.47	1.60	0.00	0.00	0.01	0.00	6.48	1.62	0.00	0.00	0.01	0.00
6.49	1.61	0.00	0.00	0.01	0.00	6.50	1.59	0.00	0.00	0.01	0.00
6.51	1.59	0.00	0.00	0.01	0.00	6.52	1.59	0.00	0.00	0.01	0.00
6.53	1.60	0.00	0.00	0.01	0.00	6.54	1.69	0.00	0.00	0.01	0.00
6.55	1.74	0.00	0.00	0.01	0.00	6.56	1.89	0.00	0.00	0.01	0.00
6.57	1.89	0.00	0.00	0.01	0.00	6.58	2.00	0.00	0.00	0.01	0.00
6.59	2.00	0.00	0.00	0.01	0.00	6.60	2.00	0.00	0.00	0.01	0.00
6.61	2.00	0.00	0.00	0.01	0.00	6.62	2.00	0.00	0.00	0.01	0.00
6.63	1.90	0.00	0.00	0.01	0.00	6.64	1.83	0.00	0.00	0.01	0.00
6.65	1.73	0.00	0.00	0.01	0.00	6.66	1.64	0.00	0.00	0.01	0.00
6.67	1.70	0.00	0.00	0.01	0.00	6.68	1.53	0.00	0.00	0.01	0.00
6.69	1.56	0.00	0.00	0.01	0.00	6.70	1.58	0.00	0.00	0.01	0.00
6.71	1.58	0.00	0.00	0.01	0.00	6.72	1.61	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
6.73	2.00	0.00	0.00	0.01	0.00	6.74	2.00	0.00	0.00	0.01	0.00
6.75	2.00	0.00	0.00	0.01	0.00	6.76	2.00	0.00	0.00	0.01	0.00
6.77	2.00	0.00	0.00	0.01	0.00	6.78	2.00	0.00	0.00	0.01	0.00
6.79	2.00	0.00	0.00	0.01	0.00	6.80	2.00	0.00	0.00	0.01	0.00
6.81	2.00	0.00	0.00	0.01	0.00	6.82	2.00	0.00	0.00	0.01	0.00
6.83	1.80	0.00	0.00	0.01	0.00	6.84	1.76	0.00	0.00	0.01	0.00
6.85	1.76	0.00	0.00	0.01	0.00	6.86	1.75	0.00	0.00	0.01	0.00
6.87	1.75	0.00	0.00	0.01	0.00	6.88	1.52	0.00	0.00	0.01	0.00
6.89	1.47	0.00	0.00	0.01	0.00	6.90	1.48	0.00	0.00	0.01	0.00
6.91	1.49	0.00	0.00	0.01	0.00	6.92	1.49	0.00	0.00	0.01	0.00
6.93	1.54	0.00	0.00	0.01	0.00	6.94	2.00	0.00	0.00	0.01	0.00
6.95	2.00	0.00	0.00	0.01	0.00	6.96	2.00	0.00	0.00	0.01	0.00
6.97	2.00	0.00	0.00	0.01	0.00	6.98	2.00	0.00	0.00	0.01	0.00
6.99	2.00	0.00	0.00	0.01	0.00	7.00	2.00	0.00	0.00	0.01	0.00
7.01	2.00	0.00	0.00	0.01	0.00	7.02	2.00	0.00	0.00	0.01	0.00
7.03	2.00	0.00	0.00	0.01	0.00	7.04	2.00	0.00	0.00	0.01	0.00
7.05	2.00	0.00	0.00	0.01	0.00	7.06	2.00	0.00	0.00	0.01	0.00
7.07	2.00	0.00	0.00	0.01	0.00	7.08	1.83	0.00	0.00	0.01	0.00
7.09	1.71	0.00	0.00	0.01	0.00	7.10	1.58	0.00	0.00	0.01	0.00
7.11	1.59	0.00	0.00	0.01	0.00	7.12	1.59	0.00	0.00	0.01	0.00
7.13	1.43	0.00	0.00	0.01	0.00	7.14	1.45	0.00	0.00	0.01	0.00
7.15	1.58	0.00	0.00	0.01	0.00	7.16	1.81	0.00	0.00	0.01	0.00
7.17	2.00	0.00	0.00	0.01	0.00	7.18	2.00	0.00	0.00	0.01	0.00
7.19	2.00	0.00	0.00	0.01	0.00	7.20	2.00	0.00	0.00	0.01	0.00
7.21	2.00	0.00	0.00	0.01	0.00	7.22	2.00	0.00	0.00	0.01	0.00
7.23	2.00	0.00	0.00	0.01	0.00	7.24	2.00	0.00	0.00	0.01	0.00
7.25	2.00	0.00	0.00	0.01	0.00	7.26	2.00	0.00	0.00	0.01	0.00
7.27	2.00	0.00	0.00	0.01	0.00	7.28	2.00	0.00	0.00	0.01	0.00
7.29	2.00	0.00	0.00	0.01	0.00	7.30	2.00	0.00	0.00	0.01	0.00
7.31	2.00	0.00	0.00	0.01	0.00	7.32	2.00	0.00	0.00	0.01	0.00
7.33	2.00	0.00	0.00	0.01	0.00	7.34	2.00	0.00	0.00	0.01	0.00
7.35	2.00	0.00	0.00	0.01	0.00	7.36	2.00	0.00	0.00	0.01	0.00
7.37	2.00	0.00	0.00	0.01	0.00	7.38	2.00	0.00	0.00	0.01	0.00
7.39	2.00	0.00	0.00	0.01	0.00	7.40	2.00	0.00	0.00	0.01	0.00
7.41	2.00	0.00	0.00	0.01	0.00	7.42	2.00	0.00	0.00	0.01	0.00
7.43	2.00	0.00	0.00	0.01	0.00	7.44	2.00	0.00	0.00	0.01	0.00
7.45	2.00	0.00	0.00	0.01	0.00	7.46	2.00	0.00	0.00	0.01	0.00
7.47	2.00	0.00	0.00	0.01	0.00	7.48	2.00	0.00	0.00	0.01	0.00
7.49	2.00	0.00	0.00	0.01	0.00	7.50	2.00	0.00	0.00	0.01	0.00
7.51	2.00	0.00	0.00	0.01	0.00	7.52	2.00	0.00	0.00	0.01	0.00
7.53	2.00	0.00	0.00	0.01	0.00	7.54	2.00	0.00	0.00	0.01	0.00
7.55	2.00	0.00	0.00	0.01	0.00	7.56	2.00	0.00	0.00	0.01	0.00
7.57	2.00	0.00	0.00	0.01	0.00	7.58	2.00	0.00	0.00	0.01	0.00
7.59	2.00	0.00	0.00	0.01	0.00	7.60	2.00	0.00	0.00	0.01	0.00
7.61	2.00	0.00	0.00	0.01	0.00	7.62	2.00	0.00	0.00	0.01	0.00
7.63	2.00	0.00	0.00	0.01	0.00	7.64	2.00	0.00	0.00	0.01	0.00
7.65	2.00	0.00	0.00	0.01	0.00	7.66	2.00	0.00	0.00	0.01	0.00
7.67	2.00	0.00	0.00	0.01	0.00	7.68	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
7.69	2.00	0.00	0.00	0.01	0.00	7.70	2.00	0.00	0.00	0.01	0.00
7.71	2.00	0.00	0.00	0.01	0.00	7.72	2.00	0.00	0.00	0.01	0.00
7.73	2.00	0.00	0.00	0.01	0.00	7.74	2.00	0.00	0.00	0.01	0.00
7.75	2.00	0.00	0.00	0.01	0.00	7.76	2.00	0.00	0.00	0.01	0.00
7.77	2.00	0.00	0.00	0.01	0.00	7.78	2.00	0.00	0.00	0.01	0.00
7.79	2.00	0.00	0.00	0.01	0.00	7.80	2.00	0.00	0.00	0.01	0.00
7.81	2.00	0.00	0.00	0.01	0.00	7.82	2.00	0.00	0.00	0.01	0.00
7.83	2.00	0.00	0.00	0.01	0.00	7.84	2.00	0.00	0.00	0.01	0.00
7.85	2.00	0.00	0.00	0.01	0.00	7.86	2.00	0.00	0.00	0.01	0.00
7.87	2.00	0.00	0.00	0.01	0.00	7.88	2.00	0.00	0.00	0.01	0.00
7.89	2.00	0.00	0.00	0.01	0.00	7.90	2.00	0.00	0.00	0.01	0.00
7.91	1.89	0.00	0.00	0.01	0.00	7.92	1.80	0.00	0.00	0.01	0.00
7.93	1.72	0.00	0.00	0.01	0.00	7.94	1.65	0.00	0.00	0.01	0.00
7.95	1.58	0.00	0.00	0.01	0.00	7.96	1.52	0.00	0.00	0.01	0.00
7.97	1.47	0.00	0.00	0.01	0.00	7.98	1.39	0.00	0.00	0.01	0.00
7.99	1.35	0.00	0.00	0.01	0.00	8.00	1.36	0.00	0.00	0.01	0.00
8.01	1.26	0.00	0.00	0.01	0.00	8.02	2.00	0.00	0.00	0.01	0.00
8.03	2.00	0.00	0.00	0.01	0.00	8.04	2.00	0.00	0.00	0.01	0.00
8.05	2.00	0.00	0.00	0.01	0.00	8.06	2.00	0.00	0.00	0.01	0.00
8.07	2.00	0.00	0.00	0.01	0.00	8.08	2.00	0.00	0.00	0.01	0.00
8.09	2.00	0.00	0.00	0.01	0.00	8.10	2.00	0.00	0.00	0.01	0.00
8.11	2.00	0.00	0.00	0.01	0.00	8.12	2.00	0.00	0.00	0.01	0.00
8.13	2.00	0.00	0.00	0.01	0.00	8.14	2.00	0.00	0.00	0.01	0.00
8.15	1.05	0.00	0.00	0.01	0.00	8.16	1.05	0.00	0.00	0.01	0.00
8.17	1.04	0.00	0.00	0.01	0.00	8.18	2.00	0.00	0.00	0.01	0.00
8.19	2.00	0.00	0.00	0.01	0.00	8.20	2.00	0.00	0.00	0.01	0.00
8.21	2.00	0.00	0.00	0.01	0.00	8.22	2.00	0.00	0.00	0.01	0.00
8.23	2.00	0.00	0.00	0.01	0.00	8.24	2.00	0.00	0.00	0.01	0.00
8.25	2.00	0.00	0.00	0.01	0.00	8.26	2.00	0.00	0.00	0.01	0.00
8.27	2.00	0.00	0.00	0.01	0.00	8.28	2.00	0.00	0.00	0.01	0.00
8.29	2.00	0.00	0.00	0.01	0.00	8.30	2.00	0.00	0.00	0.01	0.00
8.31	2.00	0.00	0.00	0.01	0.00	8.32	2.00	0.00	0.00	0.01	0.00
8.33	2.00	0.00	0.00	0.01	0.00	8.34	2.00	0.00	0.00	0.01	0.00
8.35	2.00	0.00	0.00	0.01	0.00	8.36	2.00	0.00	0.00	0.01	0.00
8.37	2.00	0.00	0.00	0.01	0.00	8.38	2.00	0.00	0.00	0.01	0.00
8.39	2.00	0.00	0.00	0.01	0.00	8.40	2.00	0.00	0.00	0.01	0.00
8.41	2.00	0.00	0.00	0.01	0.00	8.42	2.00	0.00	0.00	0.01	0.00
8.43	2.00	0.00	0.00	0.01	0.00	8.44	2.00	0.00	0.00	0.01	0.00
8.45	2.00	0.00	0.00	0.01	0.00	8.46	2.00	0.00	0.00	0.01	0.00
8.47	2.00	0.00	0.00	0.01	0.00	8.48	2.00	0.00	0.00	0.01	0.00
8.49	2.00	0.00	0.00	0.01	0.00	8.50	2.00	0.00	0.00	0.01	0.00
8.51	2.00	0.00	0.00	0.01	0.00	8.52	2.00	0.00	0.00	0.01	0.00
8.53	2.00	0.00	0.00	0.01	0.00	8.54	2.00	0.00	0.00	0.01	0.00
8.55	2.00	0.00	0.00	0.01	0.00	8.56	2.00	0.00	0.00	0.01	0.00
8.57	2.00	0.00	0.00	0.01	0.00	8.58	2.00	0.00	0.00	0.01	0.00
8.59	2.00	0.00	0.00	0.01	0.00	8.60	2.00	0.00	0.00	0.01	0.00
8.61	2.00	0.00	0.00	0.01	0.00	8.62	2.00	0.00	0.00	0.01	0.00
8.63	2.00	0.00	0.00	0.01	0.00	8.64	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
8.65	2.00	0.00	0.00	0.01	0.00	8.66	2.00	0.00	0.00	0.01	0.00
8.67	2.00	0.00	0.00	0.01	0.00	8.68	2.00	0.00	0.00	0.01	0.00
8.69	2.00	0.00	0.00	0.01	0.00	8.70	2.00	0.00	0.00	0.01	0.00
8.71	2.00	0.00	0.00	0.01	0.00	8.72	2.00	0.00	0.00	0.01	0.00
8.73	2.00	0.00	0.00	0.01	0.00	8.74	2.00	0.00	0.00	0.01	0.00
8.75	2.00	0.00	0.00	0.01	0.00	8.76	2.00	0.00	0.00	0.01	0.00
8.77	2.00	0.00	0.00	0.01	0.00	8.78	2.00	0.00	0.00	0.01	0.00
8.79	2.00	0.00	0.00	0.01	0.00	8.80	2.00	0.00	0.00	0.01	0.00
8.81	2.00	0.00	0.00	0.01	0.00	8.82	2.00	0.00	0.00	0.01	0.00
8.83	2.00	0.00	0.00	0.01	0.00	8.84	2.00	0.00	0.00	0.01	0.00
8.85	2.00	0.00	0.00	0.01	0.00	8.86	2.00	0.00	0.00	0.01	0.00
8.87	2.00	0.00	0.00	0.01	0.00	8.88	2.00	0.00	0.00	0.01	0.00
8.89	2.00	0.00	0.00	0.01	0.00	8.90	2.00	0.00	0.00	0.01	0.00
8.91	2.00	0.00	0.00	0.01	0.00	8.92	2.00	0.00	0.00	0.01	0.00
8.93	2.00	0.00	0.00	0.01	0.00	8.94	2.00	0.00	0.00	0.01	0.00
8.95	2.00	0.00	0.00	0.01	0.00	8.96	2.00	0.00	0.00	0.01	0.00
8.97	2.00	0.00	0.00	0.01	0.00	8.98	2.00	0.00	0.00	0.01	0.00
8.99	2.00	0.00	0.00	0.01	0.00	9.00	2.00	0.00	0.00	0.01	0.00
9.01	2.00	0.00	0.00	0.01	0.00	9.02	2.00	0.00	0.00	0.01	0.00
9.03	2.00	0.00	0.00	0.01	0.00	9.04	2.00	0.00	0.00	0.01	0.00
9.05	2.00	0.00	0.00	0.01	0.00	9.06	2.00	0.00	0.00	0.01	0.00
9.07	2.00	0.00	0.00	0.01	0.00	9.08	2.00	0.00	0.00	0.01	0.00
9.09	2.00	0.00	0.00	0.01	0.00	9.10	2.00	0.00	0.00	0.01	0.00
9.11	2.00	0.00	0.00	0.01	0.00	9.12	2.00	0.00	0.00	0.01	0.00
9.13	2.00	0.00	0.00	0.01	0.00	9.14	2.00	0.00	0.00	0.01	0.00
9.15	2.00	0.00	0.00	0.01	0.00	9.16	2.00	0.00	0.00	0.01	0.00
9.17	2.00	0.00	0.00	0.01	0.00	9.18	2.00	0.00	0.00	0.01	0.00
9.19	2.00	0.00	0.00	0.01	0.00	9.20	2.00	0.00	0.00	0.01	0.00
9.21	2.00	0.00	0.00	0.01	0.00	9.22	2.00	0.00	0.00	0.01	0.00
9.23	2.00	0.00	0.00	0.01	0.00	9.24	2.00	0.00	0.00	0.01	0.00
9.25	2.00	0.00	0.00	0.01	0.00	9.26	2.00	0.00	0.00	0.01	0.00
9.27	2.00	0.00	0.00	0.01	0.00	9.28	2.00	0.00	0.00	0.01	0.00
9.29	2.00	0.00	0.00	0.01	0.00	9.30	2.00	0.00	0.00	0.01	0.00
9.31	2.00	0.00	0.00	0.01	0.00	9.32	2.00	0.00	0.00	0.01	0.00
9.33	2.00	0.00	0.00	0.01	0.00	9.34	2.00	0.00	0.00	0.01	0.00
9.35	2.00	0.00	0.00	0.01	0.00	9.36	2.00	0.00	0.00	0.01	0.00
9.37	2.00	0.00	0.00	0.01	0.00	9.38	2.00	0.00	0.00	0.01	0.00
9.39	2.00	0.00	0.00	0.01	0.00	9.40	2.00	0.00	0.00	0.01	0.00
9.41	2.00	0.00	0.00	0.01	0.00	9.42	2.00	0.00	0.00	0.01	0.00
9.43	2.00	0.00	0.00	0.01	0.00	9.44	2.00	0.00	0.00	0.01	0.00
9.45	2.00	0.00	0.00	0.01	0.00	9.46	2.00	0.00	0.00	0.01	0.00
9.47	2.00	0.00	0.00	0.01	0.00	9.48	2.00	0.00	0.00	0.01	0.00
9.49	2.00	0.00	0.00	0.01	0.00	9.50	2.00	0.00	0.00	0.01	0.00
9.51	2.00	0.00	0.00	0.01	0.00	9.52	2.00	0.00	0.00	0.01	0.00
9.53	2.00	0.00	0.00	0.01	0.00	9.54	2.00	0.00	0.00	0.01	0.00
9.55	2.00	0.00	0.00	0.01	0.00	9.56	2.00	0.00	0.00	0.01	0.00
9.57	2.00	0.00	0.00	0.01	0.00	9.58	2.00	0.00	0.00	0.01	0.00
9.59	2.00	0.00	0.00	0.01	0.00	9.60	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
9.61	2.00	0.00	0.00	0.01	0.00	9.62	2.00	0.00	0.00	0.01	0.00
9.63	2.00	0.00	0.00	0.01	0.00	9.64	2.00	0.00	0.00	0.01	0.00
9.65	2.00	0.00	0.00	0.01	0.00	9.66	2.00	0.00	0.00	0.01	0.00
9.67	1.09	0.00	0.00	0.01	0.00	9.68	1.11	0.00	0.00	0.01	0.00
9.69	1.13	0.00	0.00	0.01	0.00	9.70	1.12	0.00	0.00	0.01	0.00
9.71	2.00	0.00	0.00	0.01	0.00	9.72	2.00	0.00	0.00	0.01	0.00
9.73	2.00	0.00	0.00	0.01	0.00	9.74	2.00	0.00	0.00	0.01	0.00
9.75	2.00	0.00	0.00	0.01	0.00	9.76	2.00	0.00	0.00	0.01	0.00
9.77	2.00	0.00	0.00	0.01	0.00	9.78	1.23	0.00	0.00	0.01	0.00
9.79	1.36	0.00	0.00	0.01	0.00	9.80	1.35	0.00	0.00	0.01	0.00
9.81	1.33	0.00	0.00	0.01	0.00	9.82	1.30	0.00	0.00	0.01	0.00
9.83	1.27	0.00	0.00	0.01	0.00	9.84	1.25	0.00	0.00	0.01	0.00
9.85	1.25	0.00	0.00	0.01	0.00	9.86	1.22	0.00	0.00	0.01	0.00
9.87	1.19	0.00	0.00	0.01	0.00	9.88	1.15	0.00	0.00	0.01	0.00
9.89	2.00	0.00	0.00	0.01	0.00	9.90	2.00	0.00	0.00	0.01	0.00
9.91	2.00	0.00	0.00	0.01	0.00	9.92	2.00	0.00	0.00	0.01	0.00
9.93	2.00	0.00	0.00	0.01	0.00	9.94	2.00	0.00	0.00	0.01	0.00
9.95	2.00	0.00	0.00	0.01	0.00	9.96	2.00	0.00	0.00	0.01	0.00
9.97	2.00	0.00	0.00	0.01	0.00	9.98	2.00	0.00	0.00	0.01	0.00
9.99	2.00	0.00	0.00	0.01	0.00	10.00	2.00	0.00	0.00	0.01	0.00
10.01	2.00	0.00	0.00	0.01	0.00	10.02	2.00	0.00	0.00	0.01	0.00
10.03	2.00	0.00	0.00	0.01	0.00	10.04	2.00	0.00	0.00	0.01	0.00
10.05	2.00	0.00	0.00	0.01	0.00	10.06	2.00	0.00	0.00	0.01	0.00
10.07	2.00	0.00	0.00	0.01	0.00	10.08	2.00	0.00	0.00	0.01	0.00
10.09	2.00	0.00	0.00	0.01	0.00	10.10	2.00	0.00	0.00	0.01	0.00
10.11	2.00	0.00	0.00	0.01	0.00	10.12	2.00	0.00	0.00	0.01	0.00
10.13	2.00	0.00	0.00	0.01	0.00	10.14	2.00	0.00	0.00	0.01	0.00
10.15	2.00	0.00	0.00	0.01	0.00	10.16	2.00	0.00	0.00	0.01	0.00
10.17	2.00	0.00	0.00	0.01	0.00	10.18	1.06	0.00	0.00	0.01	0.00
10.19	1.08	0.00	0.00	0.01	0.00	10.20	1.10	0.00	0.00	0.01	0.00
10.21	1.12	0.00	0.00	0.01	0.00	10.22	2.00	0.00	0.00	0.01	0.00
10.23	2.00	0.00	0.00	0.01	0.00	10.24	2.00	0.00	0.00	0.01	0.00
10.25	2.00	0.00	0.00	0.01	0.00	10.26	2.00	0.00	0.00	0.01	0.00
10.27	2.00	0.00	0.00	0.01	0.00	10.28	2.00	0.00	0.00	0.01	0.00
10.29	2.00	0.00	0.00	0.01	0.00	10.30	2.00	0.00	0.00	0.01	0.00
10.31	2.00	0.00	0.00	0.01	0.00	10.32	2.00	0.00	0.00	0.01	0.00
10.33	2.00	0.00	0.00	0.01	0.00	10.34	2.00	0.00	0.00	0.01	0.00
10.35	2.00	0.00	0.00	0.01	0.00	10.36	2.00	0.00	0.00	0.01	0.00
10.37	2.00	0.00	0.00	0.01	0.00	10.38	2.00	0.00	0.00	0.01	0.00
10.39	2.00	0.00	0.00	0.01	0.00	10.40	2.00	0.00	0.00	0.01	0.00
10.41	2.00	0.00	0.00	0.01	0.00	10.42	2.00	0.00	0.00	0.01	0.00
10.43	2.00	0.00	0.00	0.01	0.00	10.44	2.00	0.00	0.00	0.01	0.00
10.45	1.26	0.00	0.00	0.01	0.00	10.46	1.28	0.00	0.00	0.01	0.00
10.47	1.29	0.00	0.00	0.01	0.00	10.48	1.30	0.00	0.00	0.01	0.00
10.49	1.30	0.00	0.00	0.01	0.00	10.50	1.30	0.00	0.00	0.01	0.00
10.51	1.31	0.00	0.00	0.01	0.00	10.52	1.31	0.00	0.00	0.01	0.00
10.53	1.33	0.00	0.00	0.01	0.00	10.54	1.32	0.00	0.00	0.01	0.00
10.55	1.29	0.00	0.00	0.01	0.00	10.56	1.26	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
10.57	1.23	0.00	0.00	0.01	0.00	10.58	1.20	0.00	0.00	0.01	0.00
10.59	2.00	0.00	0.00	0.01	0.00	10.60	2.00	0.00	0.00	0.01	0.00
10.61	2.00	0.00	0.00	0.01	0.00	10.62	2.00	0.00	0.00	0.01	0.00
10.63	2.00	0.00	0.00	0.01	0.00	10.64	2.00	0.00	0.00	0.01	0.00
10.65	2.00	0.00	0.00	0.01	0.00	10.66	1.25	0.00	0.00	0.01	0.00
10.67	1.28	0.00	0.00	0.01	0.00	10.68	1.30	0.00	0.00	0.01	0.00
10.69	1.32	0.00	0.00	0.01	0.00	10.70	1.32	0.00	0.00	0.01	0.00
10.71	1.34	0.00	0.00	0.01	0.00	10.72	1.33	0.00	0.00	0.01	0.00
10.73	1.33	0.00	0.00	0.01	0.00	10.74	1.35	0.00	0.00	0.01	0.00
10.75	1.32	0.00	0.00	0.01	0.00	10.76	1.40	0.00	0.00	0.01	0.00
10.77	1.41	0.00	0.00	0.01	0.00	10.78	1.44	0.00	0.00	0.01	0.00
10.79	1.47	0.00	0.00	0.01	0.00	10.80	1.50	0.00	0.00	0.01	0.00
10.81	1.52	0.00	0.00	0.01	0.00	10.82	1.53	0.00	0.00	0.01	0.00
10.83	1.53	0.00	0.00	0.01	0.00	10.84	1.52	0.00	0.00	0.01	0.00
10.85	1.50	0.00	0.00	0.01	0.00	10.86	1.49	0.00	0.00	0.01	0.00
10.87	1.50	0.00	0.00	0.01	0.00	10.88	1.51	0.00	0.00	0.01	0.00
10.89	1.53	0.00	0.00	0.01	0.00	10.90	1.53	0.00	0.00	0.01	0.00
10.91	1.55	0.00	0.00	0.01	0.00	10.92	1.56	0.00	0.00	0.01	0.00
10.93	1.57	0.00	0.00	0.01	0.00	10.94	1.57	0.00	0.00	0.01	0.00
10.95	1.59	0.00	0.00	0.01	0.00	10.96	1.59	0.00	0.00	0.01	0.00
10.97	1.60	0.00	0.00	0.01	0.00	10.98	1.61	0.00	0.00	0.01	0.00
10.99	1.61	0.00	0.00	0.01	0.00	11.00	1.62	0.00	0.00	0.01	0.00
11.01	1.62	0.00	0.00	0.01	0.00	11.02	1.62	0.00	0.00	0.01	0.00
11.03	1.61	0.00	0.00	0.01	0.00	11.04	1.58	0.00	0.00	0.01	0.00
11.05	1.62	0.00	0.00	0.01	0.00	11.06	1.52	0.00	0.00	0.01	0.00
11.07	1.48	0.00	0.00	0.01	0.00	11.08	1.43	0.00	0.00	0.01	0.00
11.09	1.40	0.00	0.00	0.01	0.00	11.10	1.40	0.00	0.00	0.01	0.00
11.11	1.39	0.00	0.00	0.01	0.00	11.12	1.51	0.00	0.00	0.01	0.00
11.13	1.55	0.00	0.00	0.01	0.00	11.14	1.61	0.00	0.00	0.01	0.00
11.15	1.56	0.00	0.00	0.01	0.00	11.16	1.52	0.00	0.00	0.01	0.00
11.17	1.46	0.00	0.00	0.01	0.00	11.18	1.41	0.00	0.00	0.01	0.00
11.19	1.35	0.00	0.00	0.01	0.00	11.20	1.29	0.00	0.00	0.01	0.00
11.21	1.26	0.00	0.00	0.01	0.00	11.22	1.24	0.00	0.00	0.01	0.00
11.23	2.00	0.00	0.00	0.01	0.00	11.24	2.00	0.00	0.00	0.01	0.00
11.25	1.32	0.00	0.00	0.01	0.00	11.26	1.42	0.00	0.00	0.01	0.00
11.27	1.53	0.00	0.00	0.01	0.00	11.28	1.60	0.00	0.00	0.01	0.00
11.29	1.61	0.00	0.00	0.01	0.00	11.30	1.59	0.00	0.00	0.01	0.00
11.31	1.53	0.00	0.00	0.01	0.00	11.32	1.49	0.00	0.00	0.01	0.00
11.33	1.47	0.00	0.00	0.01	0.00	11.34	1.46	0.00	0.00	0.01	0.00
11.35	1.47	0.00	0.00	0.01	0.00	11.36	1.44	0.00	0.00	0.01	0.00
11.37	1.46	0.00	0.00	0.01	0.00	11.38	1.44	0.00	0.00	0.01	0.00
11.39	1.47	0.00	0.00	0.01	0.00	11.40	1.47	0.00	0.00	0.01	0.00
11.41	1.48	0.00	0.00	0.01	0.00	11.42	1.48	0.00	0.00	0.01	0.00
11.43	1.47	0.00	0.00	0.01	0.00	11.44	1.46	0.00	0.00	0.01	0.00
11.45	1.49	0.00	0.00	0.01	0.00	11.46	1.53	0.00	0.00	0.01	0.00
11.47	1.58	0.00	0.00	0.01	0.00	11.48	1.64	0.00	0.00	0.01	0.00
11.49	1.68	0.00	0.00	0.01	0.00	11.50	1.71	0.00	0.00	0.01	0.00
11.51	1.67	0.00	0.00	0.01	0.00	11.52	1.61	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
11.53	1.57	0.00	0.00	0.01	0.00	11.54	1.27	0.00	0.00	0.01	0.00
11.55	1.26	0.00	0.00	0.01	0.00	11.56	1.25	0.00	0.00	0.01	0.00
11.57	1.53	0.00	0.00	0.01	0.00	11.58	1.56	0.00	0.00	0.01	0.00
11.59	1.57	0.00	0.00	0.01	0.00	11.60	1.61	0.00	0.00	0.01	0.00
11.61	1.64	0.00	0.00	0.01	0.00	11.62	1.66	0.00	0.00	0.01	0.00
11.63	1.67	0.00	0.00	0.01	0.00	11.64	1.67	0.00	0.00	0.01	0.00
11.65	1.67	0.00	0.00	0.01	0.00	11.66	1.65	0.00	0.00	0.01	0.00
11.67	1.65	0.00	0.00	0.01	0.00	11.68	1.66	0.00	0.00	0.01	0.00
11.69	1.73	0.00	0.00	0.01	0.00	11.70	1.77	0.00	0.00	0.01	0.00
11.71	1.79	0.00	0.00	0.01	0.00	11.72	1.78	0.00	0.00	0.01	0.00
11.73	1.86	0.00	0.00	0.01	0.00	11.74	1.82	0.00	0.00	0.01	0.00
11.75	1.84	0.00	0.00	0.01	0.00	11.76	1.83	0.00	0.00	0.01	0.00
11.77	1.84	0.00	0.00	0.01	0.00	11.78	1.83	0.00	0.00	0.01	0.00
11.79	1.71	0.00	0.00	0.01	0.00	11.80	1.70	0.00	0.00	0.01	0.00
11.81	1.68	0.00	0.00	0.01	0.00	11.82	1.79	0.00	0.00	0.01	0.00
11.83	1.78	0.00	0.00	0.01	0.00	11.84	1.80	0.00	0.00	0.01	0.00
11.85	1.83	0.00	0.00	0.01	0.00	11.86	1.85	0.00	0.00	0.01	0.00
11.87	1.89	0.00	0.00	0.01	0.00	11.88	1.90	0.00	0.00	0.01	0.00
11.89	1.93	0.00	0.00	0.01	0.00	11.90	1.93	0.00	0.00	0.01	0.00
11.91	1.92	0.00	0.00	0.01	0.00	11.92	1.93	0.00	0.00	0.01	0.00
11.93	1.88	0.00	0.00	0.01	0.00	11.94	1.90	0.00	0.00	0.01	0.00
11.95	1.91	0.00	0.00	0.01	0.00	11.96	1.92	0.00	0.00	0.01	0.00
11.97	1.90	0.00	0.00	0.01	0.00	11.98	1.95	0.00	0.00	0.01	0.00
11.99	1.99	0.00	0.00	0.01	0.00	12.00	2.00	0.00	0.00	0.01	0.00
12.01	2.00	0.00	0.00	0.01	0.00	12.02	2.00	0.00	0.00	0.01	0.00
12.03	1.98	0.00	0.00	0.01	0.00	12.04	1.95	0.00	0.00	0.01	0.00
12.05	1.91	0.00	0.00	0.01	0.00	12.06	1.85	0.00	0.00	0.01	0.00
12.07	1.84	0.00	0.00	0.01	0.00	12.08	1.85	0.00	0.00	0.01	0.00
12.09	1.69	0.00	0.00	0.01	0.00	12.10	1.69	0.00	0.00	0.01	0.00
12.11	1.72	0.00	0.00	0.01	0.00	12.12	1.71	0.00	0.00	0.01	0.00
12.13	1.75	0.00	0.00	0.01	0.00	12.14	1.77	0.00	0.00	0.01	0.00
12.15	1.81	0.00	0.00	0.01	0.00	12.16	1.76	0.00	0.00	0.01	0.00
12.17	1.91	0.00	0.00	0.01	0.00	12.18	2.00	0.00	0.00	0.01	0.00
12.19	1.97	0.00	0.00	0.01	0.00	12.20	1.96	0.00	0.00	0.01	0.00
12.21	1.94	0.00	0.00	0.01	0.00	12.22	1.92	0.00	0.00	0.01	0.00
12.23	1.87	0.00	0.00	0.01	0.00	12.24	1.79	0.00	0.00	0.01	0.00
12.25	1.78	0.00	0.00	0.01	0.00	12.26	1.74	0.00	0.00	0.01	0.00
12.27	1.64	0.00	0.00	0.01	0.00	12.28	1.70	0.00	0.00	0.01	0.00
12.29	1.77	0.00	0.00	0.01	0.00	12.30	1.86	0.00	0.00	0.01	0.00
12.31	1.99	0.00	0.00	0.01	0.00	12.32	2.00	0.00	0.00	0.01	0.00
12.33	2.00	0.00	0.00	0.01	0.00	12.34	2.00	0.00	0.00	0.01	0.00
12.35	2.00	0.00	0.00	0.01	0.00	12.36	2.00	0.00	0.00	0.01	0.00
12.37	2.00	0.00	0.00	0.01	0.00	12.38	2.00	0.00	0.00	0.01	0.00
12.39	2.00	0.00	0.00	0.01	0.00	12.40	2.00	0.00	0.00	0.01	0.00
12.41	2.00	0.00	0.00	0.01	0.00	12.42	2.00	0.00	0.00	0.01	0.00
12.43	2.00	0.00	0.00	0.01	0.00	12.44	2.00	0.00	0.00	0.01	0.00
12.45	2.00	0.00	0.00	0.01	0.00	12.46	2.00	0.00	0.00	0.01	0.00
12.47	2.00	0.00	0.00	0.01	0.00	12.48	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
12.49	2.00	0.00	0.00	0.01	0.00	12.50	2.00	0.00	0.00	0.01	0.00
12.51	2.00	0.00	0.00	0.01	0.00	12.52	2.00	0.00	0.00	0.01	0.00
12.53	2.00	0.00	0.00	0.01	0.00	12.54	2.00	0.00	0.00	0.01	0.00
12.55	2.00	0.00	0.00	0.01	0.00	12.56	2.00	0.00	0.00	0.01	0.00
12.57	2.00	0.00	0.00	0.01	0.00	12.58	2.00	0.00	0.00	0.01	0.00
12.59	2.00	0.00	0.00	0.01	0.00	12.60	2.00	0.00	0.00	0.01	0.00
12.61	2.00	0.00	0.00	0.01	0.00	12.62	2.00	0.00	0.00	0.01	0.00
12.63	2.00	0.00	0.00	0.01	0.00	12.64	2.00	0.00	0.00	0.01	0.00
12.65	2.00	0.00	0.00	0.01	0.00	12.66	2.00	0.00	0.00	0.01	0.00
12.67	2.00	0.00	0.00	0.01	0.00	12.68	2.00	0.00	0.00	0.01	0.00
12.69	2.00	0.00	0.00	0.01	0.00	12.70	2.00	0.00	0.00	0.01	0.00
12.71	2.00	0.00	0.00	0.01	0.00	12.72	2.00	0.00	0.00	0.01	0.00
12.73	2.00	0.00	0.00	0.01	0.00	12.74	2.00	0.00	0.00	0.01	0.00
12.75	2.00	0.00	0.00	0.01	0.00	12.76	2.00	0.00	0.00	0.01	0.00
12.77	2.00	0.00	0.00	0.01	0.00	12.78	2.00	0.00	0.00	0.01	0.00
12.79	2.00	0.00	0.00	0.01	0.00	12.80	2.00	0.00	0.00	0.01	0.00
12.81	2.00	0.00	0.00	0.01	0.00	12.82	2.00	0.00	0.00	0.01	0.00
12.83	2.00	0.00	0.00	0.01	0.00	12.84	2.00	0.00	0.00	0.01	0.00
12.85	2.00	0.00	0.00	0.01	0.00	12.86	2.00	0.00	0.00	0.01	0.00
12.87	2.00	0.00	0.00	0.01	0.00	12.88	2.00	0.00	0.00	0.01	0.00
12.89	1.77	0.00	0.00	0.01	0.00	12.90	1.70	0.00	0.00	0.01	0.00
12.91	1.60	0.00	0.00	0.01	0.00	12.92	1.52	0.00	0.00	0.01	0.00
12.93	1.46	0.00	0.00	0.01	0.00	12.94	1.41	0.00	0.00	0.01	0.00
12.95	2.00	0.00	0.00	0.01	0.00	12.96	2.00	0.00	0.00	0.01	0.00
12.97	2.00	0.00	0.00	0.01	0.00	12.98	2.00	0.00	0.00	0.01	0.00
12.99	2.00	0.00	0.00	0.01	0.00	13.00	2.00	0.00	0.00	0.01	0.00
13.01	2.00	0.00	0.00	0.01	0.00	13.02	2.00	0.00	0.00	0.01	0.00
13.03	2.00	0.00	0.00	0.01	0.00	13.04	2.00	0.00	0.00	0.01	0.00
13.05	2.00	0.00	0.00	0.01	0.00	13.06	2.00	0.00	0.00	0.01	0.00
13.07	2.00	0.00	0.00	0.01	0.00	13.08	2.00	0.00	0.00	0.01	0.00
13.09	1.27	0.00	0.00	0.01	0.00	13.10	1.71	0.00	0.00	0.01	0.00
13.11	1.69	0.00	0.00	0.01	0.00	13.12	1.71	0.00	0.00	0.01	0.00
13.13	1.69	0.00	0.00	0.01	0.00	13.14	1.71	0.00	0.00	0.01	0.00
13.15	1.66	0.00	0.00	0.01	0.00	13.16	1.66	0.00	0.00	0.01	0.00
13.17	1.65	0.00	0.00	0.01	0.00	13.18	1.66	0.00	0.00	0.01	0.00
13.19	1.63	0.00	0.00	0.01	0.00	13.20	1.62	0.00	0.00	0.01	0.00
13.21	1.27	0.00	0.00	0.01	0.00	13.22	1.27	0.00	0.00	0.01	0.00
13.23	1.28	0.00	0.00	0.01	0.00	13.24	1.30	0.00	0.00	0.01	0.00
13.25	1.32	0.00	0.00	0.01	0.00	13.26	1.66	0.00	0.00	0.01	0.00
13.27	1.69	0.00	0.00	0.01	0.00	13.28	1.72	0.00	0.00	0.01	0.00
13.29	1.73	0.00	0.00	0.01	0.00	13.30	1.73	0.00	0.00	0.01	0.00
13.31	1.74	0.00	0.00	0.01	0.00	13.32	1.76	0.00	0.00	0.01	0.00
13.33	1.78	0.00	0.00	0.01	0.00	13.34	1.78	0.00	0.00	0.01	0.00
13.35	1.78	0.00	0.00	0.01	0.00	13.36	1.80	0.00	0.00	0.01	0.00
13.37	1.81	0.00	0.00	0.01	0.00	13.38	1.82	0.00	0.00	0.01	0.00
13.39	1.83	0.00	0.00	0.01	0.00	13.40	1.84	0.00	0.00	0.01	0.00
13.41	1.83	0.00	0.00	0.01	0.00	13.42	1.82	0.00	0.00	0.01	0.00
13.43	1.80	0.00	0.00	0.01	0.00	13.44	1.79	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
13.45	1.77	0.00	0.00	0.01	0.00	13.46	1.77	0.00	0.00	0.01	0.00
13.47	1.77	0.00	0.00	0.01	0.00	13.48	1.77	0.00	0.00	0.01	0.00
13.49	1.79	0.00	0.00	0.01	0.00	13.50	1.81	0.00	0.00	0.01	0.00
13.51	1.84	0.00	0.00	0.01	0.00	13.52	1.83	0.00	0.00	0.01	0.00
13.53	1.85	0.00	0.00	0.01	0.00	13.54	1.85	0.00	0.00	0.01	0.00
13.55	1.86	0.00	0.00	0.01	0.00	13.56	1.86	0.00	0.00	0.01	0.00
13.57	1.84	0.00	0.00	0.01	0.00	13.58	1.84	0.00	0.00	0.01	0.00
13.59	1.79	0.00	0.00	0.01	0.00	13.60	1.77	0.00	0.00	0.01	0.00
13.61	1.55	0.00	0.00	0.01	0.00	13.62	1.63	0.00	0.00	0.01	0.00
13.63	1.66	0.00	0.00	0.01	0.00	13.64	1.68	0.00	0.00	0.01	0.00
13.65	1.69	0.00	0.00	0.01	0.00	13.66	1.69	0.00	0.00	0.01	0.00
13.67	1.68	0.00	0.00	0.01	0.00	13.68	1.68	0.00	0.00	0.01	0.00
13.69	1.68	0.00	0.00	0.01	0.00	13.70	1.68	0.00	0.00	0.01	0.00
13.71	1.69	0.00	0.00	0.01	0.00	13.72	1.70	0.00	0.00	0.01	0.00
13.73	1.71	0.00	0.00	0.01	0.00	13.74	1.73	0.00	0.00	0.01	0.00
13.75	1.76	0.00	0.00	0.01	0.00	13.76	1.84	0.00	0.00	0.01	0.00
13.77	1.87	0.00	0.00	0.01	0.00	13.78	1.87	0.00	0.00	0.01	0.00
13.79	1.86	0.00	0.00	0.01	0.00	13.80	1.85	0.00	0.00	0.01	0.00
13.81	1.85	0.00	0.00	0.01	0.00	13.82	1.87	0.00	0.00	0.01	0.00
13.83	1.90	0.00	0.00	0.01	0.00	13.84	1.92	0.00	0.00	0.01	0.00
13.85	2.00	0.00	0.00	0.01	0.00	13.86	2.00	0.00	0.00	0.01	0.00
13.87	2.00	0.00	0.00	0.01	0.00	13.88	2.00	0.00	0.00	0.01	0.00
13.89	2.00	0.00	0.00	0.01	0.00	13.90	2.00	0.00	0.00	0.01	0.00
13.91	1.96	0.00	0.00	0.01	0.00	13.92	1.81	0.00	0.00	0.01	0.00
13.93	1.77	0.00	0.00	0.01	0.00	13.94	1.74	0.00	0.00	0.01	0.00
13.95	1.71	0.00	0.00	0.01	0.00	13.96	1.68	0.00	0.00	0.01	0.00
13.97	1.64	0.00	0.00	0.01	0.00	13.98	1.54	0.00	0.00	0.01	0.00
13.99	1.73	0.00	0.00	0.01	0.00	14.00	1.84	0.00	0.00	0.01	0.00
14.01	1.81	0.00	0.00	0.01	0.00	14.02	1.87	0.00	0.00	0.01	0.00
14.03	1.91	0.00	0.00	0.01	0.00	14.04	1.95	0.00	0.00	0.01	0.00
14.05	1.97	0.00	0.00	0.01	0.00	14.06	2.00	0.00	0.00	0.01	0.00
14.07	2.00	0.00	0.00	0.01	0.00	14.08	1.96	0.00	0.00	0.01	0.00
14.09	1.95	0.00	0.00	0.01	0.00	14.10	1.85	0.00	0.00	0.01	0.00
14.11	1.90	0.00	0.00	0.01	0.00	14.12	1.74	0.00	0.00	0.01	0.00
14.13	1.76	0.00	0.00	0.01	0.00	14.14	1.78	0.00	0.00	0.01	0.00
14.15	1.80	0.00	0.00	0.01	0.00	14.16	1.81	0.00	0.00	0.01	0.00
14.17	1.82	0.00	0.00	0.01	0.00	14.18	1.83	0.00	0.00	0.01	0.00
14.19	1.83	0.00	0.00	0.01	0.00	14.20	1.85	0.00	0.00	0.01	0.00
14.21	1.88	0.00	0.00	0.01	0.00	14.22	1.93	0.00	0.00	0.01	0.00
14.23	1.95	0.00	0.00	0.01	0.00	14.24	1.95	0.00	0.00	0.01	0.00
14.25	1.96	0.00	0.00	0.01	0.00	14.26	1.97	0.00	0.00	0.01	0.00
14.27	1.97	0.00	0.00	0.01	0.00	14.28	1.99	0.00	0.00	0.01	0.00
14.29	2.00	0.00	0.00	0.01	0.00	14.30	2.00	0.00	0.00	0.01	0.00
14.31	2.00	0.00	0.00	0.01	0.00	14.32	2.00	0.00	0.00	0.01	0.00
14.33	2.00	0.00	0.00	0.01	0.00	14.34	2.00	0.00	0.00	0.01	0.00
14.35	2.00	0.00	0.00	0.01	0.00	14.36	2.00	0.00	0.00	0.01	0.00
14.37	2.00	0.00	0.00	0.01	0.00	14.38	2.00	0.00	0.00	0.01	0.00
14.39	2.00	0.00	0.00	0.01	0.00	14.40	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
14.41	2.00	0.00	0.00	0.01	0.00	14.42	1.97	0.00	0.00	0.01	0.00
14.43	1.93	0.00	0.00	0.01	0.00	14.44	1.86	0.00	0.00	0.01	0.00
14.45	1.83	0.00	0.00	0.01	0.00	14.46	1.80	0.00	0.00	0.01	0.00
14.47	1.77	0.00	0.00	0.01	0.00	14.48	1.77	0.00	0.00	0.01	0.00
14.49	1.88	0.00	0.00	0.01	0.00	14.50	1.94	0.00	0.00	0.01	0.00
14.51	1.93	0.00	0.00	0.01	0.00	14.52	1.97	0.00	0.00	0.01	0.00
14.53	2.00	0.00	0.00	0.01	0.00	14.54	2.00	0.00	0.00	0.01	0.00
14.55	2.00	0.00	0.00	0.01	0.00	14.56	2.00	0.00	0.00	0.01	0.00
14.57	2.00	0.00	0.00	0.01	0.00	14.58	2.00	0.00	0.00	0.01	0.00
14.59	2.00	0.00	0.00	0.01	0.00	14.60	2.00	0.00	0.00	0.01	0.00
14.61	2.00	0.00	0.00	0.01	0.00	14.62	2.00	0.00	0.00	0.01	0.00
14.63	2.00	0.00	0.00	0.01	0.00	14.64	2.00	0.00	0.00	0.01	0.00
14.65	1.96	0.00	0.00	0.01	0.00	14.66	1.99	0.00	0.00	0.01	0.00
14.67	2.00	0.00	0.00	0.01	0.00	14.68	2.00	0.00	0.00	0.01	0.00
14.69	2.00	0.00	0.00	0.01	0.00	14.70	2.00	0.00	0.00	0.01	0.00
14.71	2.00	0.00	0.00	0.01	0.00	14.72	2.00	0.00	0.00	0.01	0.00
14.73	2.00	0.00	0.00	0.01	0.00	14.74	2.00	0.00	0.00	0.01	0.00
14.75	2.00	0.00	0.00	0.01	0.00	14.76	2.00	0.00	0.00	0.01	0.00
14.77	2.00	0.00	0.00	0.01	0.00	14.78	2.00	0.00	0.00	0.01	0.00
14.79	2.00	0.00	0.00	0.01	0.00	14.80	2.00	0.00	0.00	0.01	0.00
14.81	2.00	0.00	0.00	0.01	0.00	14.82	2.00	0.00	0.00	0.01	0.00
14.83	2.00	0.00	0.00	0.01	0.00	14.84	2.00	0.00	0.00	0.01	0.00
14.85	2.00	0.00	0.00	0.01	0.00	14.86	2.00	0.00	0.00	0.01	0.00
14.87	2.00	0.00	0.00	0.01	0.00	14.88	2.00	0.00	0.00	0.01	0.00
14.89	2.00	0.00	0.00	0.01	0.00	14.90	2.00	0.00	0.00	0.01	0.00
14.91	2.00	0.00	0.00	0.01	0.00	14.92	2.00	0.00	0.00	0.01	0.00
14.93	2.00	0.00	0.00	0.01	0.00	14.94	2.00	0.00	0.00	0.01	0.00
14.95	2.00	0.00	0.00	0.01	0.00	14.96	2.00	0.00	0.00	0.01	0.00
14.97	2.00	0.00	0.00	0.01	0.00	14.98	2.00	0.00	0.00	0.01	0.00
14.99	2.00	0.00	0.00	0.01	0.00	15.00	2.00	0.00	0.00	0.01	0.00
15.01	2.00	0.00	0.00	0.01	0.00	15.02	2.00	0.00	0.00	0.01	0.00
15.03	2.00	0.00	0.00	0.01	0.00	15.04	2.00	0.00	0.00	0.01	0.00
15.05	2.00	0.00	0.00	0.01	0.00	15.06	2.00	0.00	0.00	0.01	0.00
15.07	2.00	0.00	0.00	0.01	0.00	15.08	1.66	0.00	0.00	0.01	0.00
15.09	1.66	0.00	0.00	0.01	0.00	15.10	1.60	0.00	0.00	0.01	0.00
15.11	1.64	0.00	0.00	0.01	0.00	15.12	2.00	0.00	0.00	0.01	0.00
15.13	2.00	0.00	0.00	0.01	0.00	15.14	2.00	0.00	0.00	0.01	0.00
15.15	2.00	0.00	0.00	0.01	0.00	15.16	2.00	0.00	0.00	0.01	0.00
15.17	2.00	0.00	0.00	0.01	0.00	15.18	2.00	0.00	0.00	0.01	0.00
15.19	2.00	0.00	0.00	0.01	0.00	15.20	2.00	0.00	0.00	0.01	0.00
15.21	2.00	0.00	0.00	0.01	0.00	15.22	2.00	0.00	0.00	0.01	0.00
15.23	2.00	0.00	0.00	0.01	0.00	15.24	2.00	0.00	0.00	0.01	0.00
15.25	2.00	0.00	0.00	0.01	0.00	15.26	2.00	0.00	0.00	0.01	0.00
15.27	2.00	0.00	0.00	0.01	0.00	15.28	2.00	0.00	0.00	0.01	0.00
15.29	2.00	0.00	0.00	0.01	0.00	15.30	2.00	0.00	0.00	0.01	0.00
15.31	2.00	0.00	0.00	0.01	0.00	15.32	2.00	0.00	0.00	0.01	0.00
15.33	2.00	0.00	0.00	0.01	0.00	15.34	2.00	0.00	0.00	0.01	0.00
15.35	2.00	0.00	0.00	0.01	0.00	15.36	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
15.37	2.00	0.00	0.00	0.01	0.00	15.38	2.00	0.00	0.00	0.01	0.00
15.39	2.00	0.00	0.00	0.01	0.00	15.40	2.00	0.00	0.00	0.01	0.00
15.41	2.00	0.00	0.00	0.01	0.00	15.42	2.00	0.00	0.00	0.01	0.00
15.43	2.00	0.00	0.00	0.01	0.00	15.44	2.00	0.00	0.00	0.01	0.00
15.45	2.00	0.00	0.00	0.01	0.00	15.46	2.00	0.00	0.00	0.01	0.00
15.47	2.00	0.00	0.00	0.01	0.00	15.48	2.00	0.00	0.00	0.01	0.00
15.49	1.33	0.00	0.00	0.01	0.00	15.50	1.32	0.00	0.00	0.01	0.00
15.51	1.29	0.00	0.00	0.01	0.00	15.52	1.55	0.00	0.00	0.01	0.00
15.53	1.80	0.00	0.00	0.01	0.00	15.54	1.81	0.00	0.00	0.01	0.00
15.55	1.81	0.00	0.00	0.01	0.00	15.56	1.78	0.00	0.00	0.01	0.00
15.57	1.74	0.00	0.00	0.01	0.00	15.58	1.73	0.00	0.00	0.01	0.00
15.59	1.75	0.00	0.00	0.01	0.00	15.60	1.70	0.00	0.00	0.01	0.00
15.61	1.64	0.00	0.00	0.01	0.00	15.62	1.56	0.00	0.00	0.01	0.00
15.63	1.58	0.00	0.00	0.01	0.00	15.64	2.00	0.00	0.00	0.01	0.00
15.65	2.00	0.00	0.00	0.01	0.00	15.66	2.00	0.00	0.00	0.01	0.00
15.67	2.00	0.00	0.00	0.01	0.00	15.68	2.00	0.00	0.00	0.01	0.00
15.69	2.00	0.00	0.00	0.01	0.00	15.70	2.00	0.00	0.00	0.01	0.00
15.71	2.00	0.00	0.00	0.01	0.00	15.72	2.00	0.00	0.00	0.01	0.00
15.73	2.00	0.00	0.00	0.01	0.00	15.74	2.00	0.00	0.00	0.01	0.00
15.75	2.00	0.00	0.00	0.01	0.00	15.76	2.00	0.00	0.00	0.01	0.00
15.77	2.00	0.00	0.00	0.01	0.00	15.78	2.00	0.00	0.00	0.01	0.00
15.79	2.00	0.00	0.00	0.01	0.00	15.80	2.00	0.00	0.00	0.01	0.00
15.81	2.00	0.00	0.00	0.01	0.00	15.82	2.00	0.00	0.00	0.01	0.00
15.83	2.00	0.00	0.00	0.01	0.00	15.84	2.00	0.00	0.00	0.01	0.00
15.85	2.00	0.00	0.00	0.01	0.00	15.86	2.00	0.00	0.00	0.01	0.00
15.87	2.00	0.00	0.00	0.01	0.00	15.88	2.00	0.00	0.00	0.01	0.00
15.89	2.00	0.00	0.00	0.01	0.00	15.90	2.00	0.00	0.00	0.01	0.00
15.91	2.00	0.00	0.00	0.01	0.00	15.92	2.00	0.00	0.00	0.01	0.00
15.93	2.00	0.00	0.00	0.01	0.00	15.94	2.00	0.00	0.00	0.01	0.00
15.95	2.00	0.00	0.00	0.01	0.00	15.96	2.00	0.00	0.00	0.01	0.00
15.97	2.00	0.00	0.00	0.01	0.00	15.98	2.00	0.00	0.00	0.01	0.00
15.99	2.00	0.00	0.00	0.01	0.00	16.00	2.00	0.00	0.00	0.01	0.00
16.01	2.00	0.00	0.00	0.01	0.00	16.02	2.00	0.00	0.00	0.01	0.00
16.03	2.00	0.00	0.00	0.01	0.00	16.04	2.00	0.00	0.00	0.01	0.00
16.05	2.00	0.00	0.00	0.01	0.00	16.06	2.00	0.00	0.00	0.01	0.00
16.07	2.00	0.00	0.00	0.01	0.00	16.08	2.00	0.00	0.00	0.01	0.00
16.09	2.00	0.00	0.00	0.01	0.00	16.10	2.00	0.00	0.00	0.01	0.00
16.11	2.00	0.00	0.00	0.01	0.00	16.12	2.00	0.00	0.00	0.01	0.00
16.13	2.00	0.00	0.00	0.01	0.00	16.14	2.00	0.00	0.00	0.01	0.00
16.15	2.00	0.00	0.00	0.01	0.00	16.16	2.00	0.00	0.00	0.01	0.00
16.17	2.00	0.00	0.00	0.01	0.00	16.18	2.00	0.00	0.00	0.01	0.00
16.19	2.00	0.00	0.00	0.01	0.00	16.20	2.00	0.00	0.00	0.01	0.00
16.21	2.00	0.00	0.00	0.01	0.00	16.22	2.00	0.00	0.00	0.01	0.00
16.23	2.00	0.00	0.00	0.01	0.00	16.24	2.00	0.00	0.00	0.01	0.00
16.25	2.00	0.00	0.00	0.01	0.00	16.26	2.00	0.00	0.00	0.01	0.00
16.27	2.00	0.00	0.00	0.01	0.00	16.28	2.00	0.00	0.00	0.01	0.00
16.29	2.00	0.00	0.00	0.01	0.00	16.30	2.00	0.00	0.00	0.01	0.00
16.31	2.00	0.00	0.00	0.01	0.00	16.32	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
16.33	2.00	0.00	0.00	0.01	0.00	16.34	2.00	0.00	0.00	0.01	0.00
16.35	2.00	0.00	0.00	0.01	0.00	16.36	2.00	0.00	0.00	0.01	0.00
16.37	2.00	0.00	0.00	0.01	0.00	16.38	2.00	0.00	0.00	0.01	0.00
16.39	2.00	0.00	0.00	0.01	0.00	16.40	2.00	0.00	0.00	0.01	0.00
16.41	2.00	0.00	0.00	0.01	0.00	16.42	2.00	0.00	0.00	0.01	0.00
16.43	2.00	0.00	0.00	0.01	0.00	16.44	2.00	0.00	0.00	0.01	0.00
16.45	2.00	0.00	0.00	0.01	0.00	16.46	2.00	0.00	0.00	0.01	0.00
16.47	2.00	0.00	0.00	0.01	0.00	16.48	2.00	0.00	0.00	0.01	0.00
16.49	2.00	0.00	0.00	0.01	0.00	16.50	2.00	0.00	0.00	0.01	0.00
16.51	2.00	0.00	0.00	0.01	0.00	16.52	2.00	0.00	0.00	0.01	0.00
16.53	2.00	0.00	0.00	0.01	0.00	16.54	2.00	0.00	0.00	0.01	0.00
16.55	2.00	0.00	0.00	0.01	0.00	16.56	2.00	0.00	0.00	0.01	0.00
16.57	2.00	0.00	0.00	0.01	0.00	16.58	2.00	0.00	0.00	0.01	0.00
16.59	2.00	0.00	0.00	0.01	0.00	16.60	2.00	0.00	0.00	0.01	0.00
16.61	2.00	0.00	0.00	0.01	0.00	16.62	2.00	0.00	0.00	0.01	0.00
16.63	2.00	0.00	0.00	0.01	0.00	16.64	2.00	0.00	0.00	0.01	0.00
16.65	1.49	0.00	0.00	0.01	0.00	16.66	1.57	0.00	0.00	0.01	0.00
16.67	1.51	0.00	0.00	0.01	0.00	16.68	2.00	0.00	0.00	0.01	0.00
16.69	2.00	0.00	0.00	0.01	0.00	16.70	2.00	0.00	0.00	0.01	0.00
16.71	2.00	0.00	0.00	0.01	0.00	16.72	2.00	0.00	0.00	0.01	0.00
16.73	2.00	0.00	0.00	0.01	0.00	16.74	2.00	0.00	0.00	0.01	0.00
16.75	2.00	0.00	0.00	0.01	0.00	16.76	1.75	0.00	0.00	0.01	0.00
16.77	1.96	0.00	0.00	0.01	0.00	16.78	2.00	0.00	0.00	0.01	0.00
16.79	2.00	0.00	0.00	0.01	0.00	16.80	2.00	0.00	0.00	0.01	0.00
16.81	2.00	0.00	0.00	0.01	0.00	16.82	2.00	0.00	0.00	0.01	0.00
16.83	2.00	0.00	0.00	0.01	0.00	16.84	2.00	0.00	0.00	0.01	0.00
16.85	2.00	0.00	0.00	0.01	0.00	16.86	2.00	0.00	0.00	0.01	0.00
16.87	2.00	0.00	0.00	0.01	0.00	16.88	2.00	0.00	0.00	0.01	0.00
16.89	2.00	0.00	0.00	0.01	0.00	16.90	2.00	0.00	0.00	0.01	0.00
16.91	2.00	0.00	0.00	0.01	0.00	16.92	2.00	0.00	0.00	0.01	0.00
16.93	2.00	0.00	0.00	0.01	0.00	16.94	2.00	0.00	0.00	0.01	0.00
16.95	2.00	0.00	0.00	0.01	0.00	16.96	1.99	0.00	0.00	0.01	0.00
16.97	1.90	0.00	0.00	0.01	0.00	16.98	1.89	0.00	0.00	0.01	0.00
16.99	1.88	0.00	0.00	0.01	0.00	17.00	1.91	0.00	0.00	0.01	0.00
17.01	1.98	0.00	0.00	0.01	0.00	17.02	2.00	0.00	0.00	0.01	0.00
17.03	2.00	0.00	0.00	0.01	0.00	17.04	2.00	0.00	0.00	0.01	0.00
17.05	2.00	0.00	0.00	0.01	0.00	17.06	2.00	0.00	0.00	0.01	0.00
17.07	2.00	0.00	0.00	0.01	0.00	17.08	2.00	0.00	0.00	0.01	0.00
17.09	2.00	0.00	0.00	0.01	0.00	17.10	2.00	0.00	0.00	0.01	0.00
17.11	2.00	0.00	0.00	0.01	0.00	17.12	2.00	0.00	0.00	0.01	0.00
17.13	2.00	0.00	0.00	0.01	0.00	17.14	2.00	0.00	0.00	0.01	0.00
17.15	2.00	0.00	0.00	0.01	0.00	17.16	2.00	0.00	0.00	0.01	0.00
17.17	2.00	0.00	0.00	0.01	0.00	17.18	2.00	0.00	0.00	0.01	0.00
17.19	2.00	0.00	0.00	0.01	0.00	17.20	2.00	0.00	0.00	0.01	0.00
17.21	2.00	0.00	0.00	0.01	0.00	17.22	2.00	0.00	0.00	0.01	0.00
17.23	2.00	0.00	0.00	0.01	0.00	17.24	2.00	0.00	0.00	0.01	0.00
17.25	2.00	0.00	0.00	0.01	0.00	17.26	2.00	0.00	0.00	0.01	0.00
17.27	2.00	0.00	0.00	0.01	0.00	17.28	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
17.29	2.00	0.00	0.00	0.01	0.00	17.30	2.00	0.00	0.00	0.01	0.00
17.31	2.00	0.00	0.00	0.01	0.00	17.32	2.00	0.00	0.00	0.01	0.00
17.33	2.00	0.00	0.00	0.01	0.00	17.34	2.00	0.00	0.00	0.01	0.00
17.35	2.00	0.00	0.00	0.01	0.00	17.36	2.00	0.00	0.00	0.01	0.00
17.37	2.00	0.00	0.00	0.01	0.00	17.38	2.00	0.00	0.00	0.01	0.00
17.39	2.00	0.00	0.00	0.01	0.00	17.40	2.00	0.00	0.00	0.01	0.00
17.41	2.00	0.00	0.00	0.01	0.00	17.42	2.00	0.00	0.00	0.01	0.00
17.43	2.00	0.00	0.00	0.01	0.00	17.44	2.00	0.00	0.00	0.01	0.00
17.45	2.00	0.00	0.00	0.01	0.00	17.46	2.00	0.00	0.00	0.01	0.00
17.47	2.00	0.00	0.00	0.01	0.00	17.48	2.00	0.00	0.00	0.01	0.00
17.49	2.00	0.00	0.00	0.01	0.00	17.50	2.00	0.00	0.00	0.01	0.00
17.51	2.00	0.00	0.00	0.01	0.00	17.52	2.00	0.00	0.00	0.01	0.00
17.53	2.00	0.00	0.00	0.01	0.00	17.54	2.00	0.00	0.00	0.01	0.00
17.55	2.00	0.00	0.00	0.01	0.00	17.56	2.00	0.00	0.00	0.01	0.00
17.57	2.00	0.00	0.00	0.01	0.00	17.58	2.00	0.00	0.00	0.01	0.00
17.59	2.00	0.00	0.00	0.01	0.00	17.60	2.00	0.00	0.00	0.01	0.00
17.61	2.00	0.00	0.00	0.01	0.00	17.62	2.00	0.00	0.00	0.01	0.00
17.63	2.00	0.00	0.00	0.01	0.00	17.64	2.00	0.00	0.00	0.01	0.00
17.65	2.00	0.00	0.00	0.01	0.00	17.66	2.00	0.00	0.00	0.01	0.00
17.67	2.00	0.00	0.00	0.01	0.00	17.68	2.00	0.00	0.00	0.01	0.00
17.69	2.00	0.00	0.00	0.01	0.00	17.70	2.00	0.00	0.00	0.01	0.00
17.71	2.00	0.00	0.00	0.01	0.00	17.72	2.00	0.00	0.00	0.01	0.00
17.73	2.00	0.00	0.00	0.01	0.00	17.74	2.00	0.00	0.00	0.01	0.00
17.75	2.00	0.00	0.00	0.01	0.00	17.76	2.00	0.00	0.00	0.01	0.00
17.77	2.00	0.00	0.00	0.01	0.00	17.78	2.00	0.00	0.00	0.01	0.00
17.79	2.00	0.00	0.00	0.01	0.00	17.80	2.00	0.00	0.00	0.01	0.00
17.81	2.00	0.00	0.00	0.01	0.00	17.82	2.00	0.00	0.00	0.01	0.00
17.83	2.00	0.00	0.00	0.01	0.00	17.84	2.00	0.00	0.00	0.01	0.00
17.85	2.00	0.00	0.00	0.01	0.00	17.86	2.00	0.00	0.00	0.01	0.00
17.87	2.00	0.00	0.00	0.01	0.00	17.88	2.00	0.00	0.00	0.01	0.00
17.89	2.00	0.00	0.00	0.01	0.00	17.90	2.00	0.00	0.00	0.01	0.00
17.91	2.00	0.00	0.00	0.01	0.00	17.92	2.00	0.00	0.00	0.01	0.00
17.93	2.00	0.00	0.00	0.01	0.00	17.94	2.00	0.00	0.00	0.01	0.00
17.95	2.00	0.00	0.00	0.01	0.00	17.96	2.00	0.00	0.00	0.01	0.00
17.97	2.00	0.00	0.00	0.01	0.00	17.98	2.00	0.00	0.00	0.01	0.00
17.99	2.00	0.00	0.00	0.01	0.00	18.00	2.00	0.00	0.00	0.01	0.00
18.01	2.00	0.00	0.00	0.01	0.00	18.02	2.00	0.00	0.00	0.01	0.00
18.03	2.00	0.00	0.00	0.01	0.00	18.04	2.00	0.00	0.00	0.01	0.00
18.05	2.00	0.00	0.00	0.01	0.00	18.06	2.00	0.00	0.00	0.01	0.00
18.07	2.00	0.00	0.00	0.01	0.00	18.08	2.00	0.00	0.00	0.01	0.00
18.09	2.00	0.00	0.00	0.01	0.00	18.10	2.00	0.00	0.00	0.01	0.00
18.11	2.00	0.00	0.00	0.01	0.00	18.12	2.00	0.00	0.00	0.01	0.00
18.13	2.00	0.00	0.00	0.01	0.00	18.14	2.00	0.00	0.00	0.01	0.00
18.15	2.00	0.00	0.00	0.01	0.00	18.16	2.00	0.00	0.00	0.01	0.00
18.17	2.00	0.00	0.00	0.01	0.00	18.18	2.00	0.00	0.00	0.01	0.00
18.19	2.00	0.00	0.00	0.01	0.00	18.20	2.00	0.00	0.00	0.01	0.00
18.21	2.00	0.00	0.00	0.01	0.00	18.22	2.00	0.00	0.00	0.01	0.00
18.23	2.00	0.00	0.00	0.01	0.00	18.24	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
18.25	2.00	0.00	0.00	0.01	0.00	18.26	2.00	0.00	0.00	0.01	0.00
18.27	2.00	0.00	0.00	0.01	0.00	18.28	2.00	0.00	0.00	0.01	0.00
18.29	2.00	0.00	0.00	0.01	0.00	18.30	2.00	0.00	0.00	0.01	0.00
18.31	2.00	0.00	0.00	0.01	0.00	18.32	2.00	0.00	0.00	0.01	0.00
18.33	2.00	0.00	0.00	0.01	0.00	18.34	2.00	0.00	0.00	0.01	0.00
18.35	2.00	0.00	0.00	0.01	0.00	18.36	2.00	0.00	0.00	0.01	0.00
18.37	2.00	0.00	0.00	0.01	0.00	18.38	2.00	0.00	0.00	0.01	0.00
18.39	2.00	0.00	0.00	0.01	0.00	18.40	2.00	0.00	0.00	0.01	0.00
18.41	2.00	0.00	0.00	0.01	0.00	18.42	2.00	0.00	0.00	0.01	0.00
18.43	2.00	0.00	0.00	0.01	0.00	18.44	2.00	0.00	0.00	0.01	0.00
18.45	2.00	0.00	0.00	0.01	0.00	18.46	2.00	0.00	0.00	0.01	0.00
18.47	2.00	0.00	0.00	0.01	0.00	18.48	2.00	0.00	0.00	0.01	0.00
18.49	2.00	0.00	0.00	0.01	0.00	18.50	2.00	0.00	0.00	0.01	0.00
18.51	2.00	0.00	0.00	0.01	0.00	18.52	2.00	0.00	0.00	0.01	0.00
18.53	2.00	0.00	0.00	0.01	0.00	18.54	2.00	0.00	0.00	0.01	0.00
18.55	2.00	0.00	0.00	0.01	0.00	18.56	2.00	0.00	0.00	0.01	0.00
18.57	2.00	0.00	0.00	0.01	0.00	18.58	2.00	0.00	0.00	0.01	0.00
18.59	2.00	0.00	0.00	0.01	0.00	18.60	2.00	0.00	0.00	0.01	0.00
18.61	2.00	0.00	0.00	0.01	0.00	18.62	2.00	0.00	0.00	0.01	0.00
18.63	2.00	0.00	0.00	0.01	0.00	18.64	2.00	0.00	0.00	0.01	0.00
18.65	2.00	0.00	0.00	0.01	0.00	18.66	2.00	0.00	0.00	0.01	0.00
18.67	2.00	0.00	0.00	0.01	0.00	18.68	2.00	0.00	0.00	0.01	0.00
18.69	2.00	0.00	0.00	0.01	0.00	18.70	2.00	0.00	0.00	0.01	0.00
18.71	2.00	0.00	0.00	0.01	0.00	18.72	2.00	0.00	0.00	0.01	0.00
18.73	2.00	0.00	0.00	0.01	0.00	18.74	2.00	0.00	0.00	0.01	0.00
18.75	2.00	0.00	0.00	0.01	0.00	18.76	2.00	0.00	0.00	0.01	0.00
18.77	2.00	0.00	0.00	0.01	0.00	18.78	2.00	0.00	0.00	0.01	0.00
18.79	2.00	0.00	0.00	0.01	0.00	18.80	2.00	0.00	0.00	0.01	0.00
18.81	2.00	0.00	0.00	0.01	0.00	18.82	2.00	0.00	0.00	0.01	0.00
18.83	2.00	0.00	0.00	0.01	0.00	18.84	2.00	0.00	0.00	0.01	0.00
18.85	2.00	0.00	0.00	0.01	0.00	18.86	2.00	0.00	0.00	0.01	0.00
18.87	2.00	0.00	0.00	0.01	0.00	18.88	2.00	0.00	0.00	0.01	0.00
18.89	2.00	0.00	0.00	0.01	0.00	18.90	2.00	0.00	0.00	0.01	0.00
18.91	2.00	0.00	0.00	0.01	0.00	18.92	2.00	0.00	0.00	0.01	0.00
18.93	2.00	0.00	0.00	0.01	0.00	18.94	2.00	0.00	0.00	0.01	0.00
18.95	2.00	0.00	0.00	0.01	0.00	18.96	2.00	0.00	0.00	0.01	0.00
18.97	2.00	0.00	0.00	0.01	0.00	18.98	2.00	0.00	0.00	0.01	0.00
18.99	2.00	0.00	0.00	0.01	0.00	19.00	2.00	0.00	0.00	0.01	0.00
19.01	2.00	0.00	0.00	0.01	0.00	19.02	2.00	0.00	0.00	0.01	0.00
19.03	2.00	0.00	0.00	0.01	0.00	19.04	2.00	0.00	0.00	0.01	0.00
19.05	2.00	0.00	0.00	0.01	0.00	19.06	2.00	0.00	0.00	0.01	0.00
19.07	2.00	0.00	0.00	0.01	0.00	19.08	2.00	0.00	0.00	0.01	0.00
19.09	2.00	0.00	0.00	0.01	0.00	19.10	2.00	0.00	0.00	0.01	0.00
19.11	2.00	0.00	0.00	0.01	0.00	19.12	2.00	0.00	0.00	0.01	0.00
19.13	2.00	0.00	0.00	0.01	0.00	19.14	2.00	0.00	0.00	0.01	0.00
19.15	2.00	0.00	0.00	0.01	0.00	19.16	2.00	0.00	0.00	0.01	0.00
19.17	2.00	0.00	0.00	0.01	0.00	19.18	2.00	0.00	0.00	0.01	0.00
19.19	2.00	0.00	0.00	0.01	0.00	19.20	1.55	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
19.21	1.72	0.00	0.00	0.01	0.00	19.22	1.80	0.00	0.00	0.01	0.00
19.23	1.88	0.00	0.00	0.01	0.00	19.24	2.00	0.00	0.00	0.01	0.00
19.25	2.00	0.00	0.00	0.01	0.00	19.26	2.00	0.00	0.00	0.01	0.00
19.27	2.00	0.00	0.00	0.01	0.00	19.28	1.97	0.00	0.00	0.01	0.00
19.29	2.00	0.00	0.00	0.01	0.00	19.30	2.00	0.00	0.00	0.01	0.00
19.31	2.00	0.00	0.00	0.01	0.00	19.32	2.00	0.00	0.00	0.01	0.00
19.33	2.00	0.00	0.00	0.01	0.00	19.34	2.00	0.00	0.00	0.01	0.00
19.35	2.00	0.00	0.00	0.01	0.00	19.36	2.00	0.00	0.00	0.01	0.00
19.37	2.00	0.00	0.00	0.01	0.00	19.38	2.00	0.00	0.00	0.01	0.00
19.39	2.00	0.00	0.00	0.01	0.00	19.40	2.00	0.00	0.00	0.01	0.00
19.41	2.00	0.00	0.00	0.01	0.00	19.42	2.00	0.00	0.00	0.01	0.00
19.43	2.00	0.00	0.00	0.01	0.00	19.44	2.00	0.00	0.00	0.01	0.00
19.45	2.00	0.00	0.00	0.01	0.00	19.46	2.00	0.00	0.00	0.01	0.00
19.47	2.00	0.00	0.00	0.01	0.00	19.48	2.00	0.00	0.00	0.01	0.00
19.49	2.00	0.00	0.00	0.01	0.00	19.50	2.00	0.00	0.00	0.01	0.00
19.51	2.00	0.00	0.00	0.01	0.00	19.52	2.00	0.00	0.00	0.01	0.00
19.53	2.00	0.00	0.00	0.01	0.00	19.54	2.00	0.00	0.00	0.01	0.00
19.55	2.00	0.00	0.00	0.01	0.00	19.56	2.00	0.00	0.00	0.01	0.00
19.57	2.00	0.00	0.00	0.01	0.00	19.58	2.00	0.00	0.00	0.01	0.00
19.59	2.00	0.00	0.00	0.01	0.00	19.60	2.00	0.00	0.00	0.01	0.00
19.61	2.00	0.00	0.00	0.01	0.00	19.62	2.00	0.00	0.00	0.01	0.00
19.63	2.00	0.00	0.00	0.01	0.00	19.64	2.00	0.00	0.00	0.01	0.00
19.65	2.00	0.00	0.00	0.01	0.00	19.66	2.00	0.00	0.00	0.01	0.00
19.67	1.96	0.00	0.00	0.01	0.00	19.68	2.00	0.00	0.00	0.01	0.00
19.69	2.00	0.00	0.00	0.01	0.00	19.70	2.00	0.00	0.00	0.01	0.00
19.71	2.00	0.00	0.00	0.01	0.00	19.72	2.00	0.00	0.00	0.01	0.00
19.73	2.00	0.00	0.00	0.01	0.00	19.74	2.00	0.00	0.00	0.01	0.00
19.75	2.00	0.00	0.00	0.01	0.00	19.76	2.00	0.00	0.00	0.01	0.00
19.77	2.00	0.00	0.00	0.01	0.00	19.78	2.00	0.00	0.00	0.01	0.00
19.79	2.00	0.00	0.00	0.01	0.00	19.80	2.00	0.00	0.00	0.01	0.00
19.81	2.00	0.00	0.00	0.01	0.00	19.82	2.00	0.00	0.00	0.01	0.00
19.83	2.00	0.00	0.00	0.01	0.00	19.84	2.00	0.00	0.00	0.01	0.00
19.85	2.00	0.00	0.00	0.01	0.00	19.86	2.00	0.00	0.00	0.01	0.00
19.87	2.00	0.00	0.00	0.01	0.00	19.88	2.00	0.00	0.00	0.01	0.00
19.89	2.00	0.00	0.00	0.01	0.00	19.90	2.00	0.00	0.00	0.01	0.00
19.91	2.00	0.00	0.00	0.01	0.00	19.92	2.00	0.00	0.00	0.01	0.00
19.93	2.00	0.00	0.00	0.01	0.00	19.94	2.00	0.00	0.00	0.01	0.00
19.95	2.00	0.00	0.00	0.01	0.00	19.96	2.00	0.00	0.00	0.01	0.00
19.97	2.00	0.00	0.00	0.01	0.00	19.98	2.00	0.00	0.00	0.01	0.00
19.99	2.00	0.00	0.00	0.01	0.00	20.00	2.00	0.00	0.00	0.01	0.00
20.01	2.00	0.00	0.00	0.01	0.00	20.02	2.00	0.00	0.00	0.01	0.00
20.03	2.00	0.00	0.00	0.01	0.00	20.04	2.00	0.00	0.00	0.01	0.00
20.05	2.00	0.00	0.00	0.01	0.00	20.06	2.00	0.00	0.00	0.01	0.00
20.07	2.00	0.00	0.00	0.01	0.00	20.08	2.00	0.00	0.00	0.01	0.00
20.09	2.00	0.00	0.00	0.01	0.00	20.10	2.00	0.00	0.00	0.01	0.00
20.11	2.00	0.00	0.00	0.01	0.00	20.12	1.91	0.00	0.00	0.01	0.00
20.13	1.87	0.00	0.00	0.01	0.00	20.14	2.00	0.00	0.00	0.01	0.00
20.15	2.00	0.00	0.00	0.01	0.00	20.16	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
20.17	2.00	0.00	0.00	0.01	0.00	20.18	2.00	0.00	0.00	0.01	0.00
20.19	2.00	0.00	0.00	0.01	0.00	20.20	1.96	0.00	0.00	0.01	0.00
20.21	2.00	0.00	0.00	0.01	0.00	20.22	2.00	0.00	0.00	0.01	0.00
20.23	2.00	0.00	0.00	0.01	0.00	20.24	2.00	0.00	0.00	0.01	0.00
20.25	2.00	0.00	0.00	0.01	0.00	20.26	2.00	0.00	0.00	0.01	0.00
20.27	2.00	0.00	0.00	0.01	0.00	20.28	2.00	0.00	0.00	0.01	0.00
20.29	2.00	0.00	0.00	0.01	0.00	20.30	2.00	0.00	0.00	0.01	0.00
20.31	2.00	0.00	0.00	0.01	0.00	20.32	2.00	0.00	0.00	0.01	0.00
20.33	2.00	0.00	0.00	0.01	0.00	20.34	2.00	0.00	0.00	0.01	0.00
20.35	2.00	0.00	0.00	0.01	0.00	20.36	2.00	0.00	0.00	0.01	0.00
20.37	2.00	0.00	0.00	0.01	0.00	20.38	2.00	0.00	0.00	0.01	0.00
20.39	2.00	0.00	0.00	0.01	0.00	20.40	2.00	0.00	0.00	0.01	0.00
20.41	2.00	0.00	0.00	0.01	0.00	20.42	2.00	0.00	0.00	0.01	0.00
20.43	2.00	0.00	0.00	0.01	0.00	20.44	2.00	0.00	0.00	0.01	0.00
20.45	2.00	0.00	0.00	0.01	0.00	20.46	2.00	0.00	0.00	0.01	0.00
20.47	2.00	0.00	0.00	0.01	0.00	20.48	2.00	0.00	0.00	0.01	0.00
20.49	2.00	0.00	0.00	0.01	0.00	20.50	2.00	0.00	0.00	0.01	0.00
20.51	2.00	0.00	0.00	0.01	0.00	20.52	2.00	0.00	0.00	0.01	0.00
20.53	2.00	0.00	0.00	0.01	0.00	20.54	2.00	0.00	0.00	0.01	0.00
20.55	2.00	0.00	0.00	0.01	0.00	20.56	2.00	0.00	0.00	0.01	0.00
20.57	2.00	0.00	0.00	0.01	0.00	20.58	2.00	0.00	0.00	0.01	0.00
20.59	2.00	0.00	0.00	0.01	0.00	20.60	2.00	0.00	0.00	0.01	0.00
20.61	2.00	0.00	0.00	0.01	0.00	20.62	2.00	0.00	0.00	0.01	0.00
20.63	2.00	0.00	0.00	0.01	0.00	20.64	2.00	0.00	0.00	0.01	0.00
20.65	2.00	0.00	0.00	0.01	0.00	20.66	2.00	0.00	0.00	0.01	0.00
20.67	2.00	0.00	0.00	0.01	0.00	20.68	2.00	0.00	0.00	0.01	0.00
20.69	2.00	0.00	0.00	0.01	0.00	20.70	2.00	0.00	0.00	0.01	0.00
20.71	2.00	0.00	0.00	0.01	0.00	20.72	2.00	0.00	0.00	0.01	0.00
20.73	2.00	0.00	0.00	0.01	0.00	20.74	2.00	0.00	0.00	0.01	0.00
20.75	2.00	0.00	0.00	0.01	0.00	20.76	2.00	0.00	0.00	0.01	0.00
20.77	2.00	0.00	0.00	0.01	0.00	20.78	2.00	0.00	0.00	0.01	0.00
20.79	2.00	0.00	0.00	0.01	0.00	20.80	2.00	0.00	0.00	0.01	0.00
20.81	2.00	0.00	0.00	0.01	0.00	20.82	2.00	0.00	0.00	0.01	0.00
20.83	2.00	0.00	0.00	0.01	0.00	20.84	2.00	0.00	0.00	0.01	0.00
20.85	2.00	0.00	0.00	0.01	0.00	20.86	2.00	0.00	0.00	0.01	0.00
20.87	2.00	0.00	0.00	0.01	0.00	20.88	2.00	0.00	0.00	0.01	0.00
20.89	2.00	0.00	0.00	0.01	0.00	20.90	2.00	0.00	0.00	0.01	0.00
20.91	2.00	0.00	0.00	0.01	0.00	20.92	2.00	0.00	0.00	0.01	0.00
20.93	2.00	0.00	0.00	0.01	0.00	20.94	2.00	0.00	0.00	0.01	0.00
20.95	2.00	0.00	0.00	0.01	0.00	20.96	2.00	0.00	0.00	0.01	0.00
20.97	2.00	0.00	0.00	0.01	0.00	20.98	2.00	0.00	0.00	0.01	0.00
20.99	2.00	0.00	0.00	0.01	0.00	21.00	2.00	0.00	0.00	0.01	0.00
21.01	2.00	0.00	0.00	0.01	0.00	21.02	2.00	0.00	0.00	0.01	0.00
21.03	2.00	0.00	0.00	0.01	0.00	21.04	2.00	0.00	0.00	0.01	0.00
21.05	2.00	0.00	0.00	0.01	0.00	21.06	2.00	0.00	0.00	0.01	0.00
21.07	2.00	0.00	0.00	0.01	0.00	21.08	2.00	0.00	0.00	0.01	0.00
21.09	2.00	0.00	0.00	0.01	0.00	21.10	2.00	0.00	0.00	0.01	0.00
21.11	2.00	0.00	0.00	0.01	0.00	21.12	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
21.13	2.00	0.00	0.00	0.01	0.00	21.14	2.00	0.00	0.00	0.01	0.00
21.15	2.00	0.00	0.00	0.01	0.00	21.16	2.00	0.00	0.00	0.01	0.00
21.17	2.00	0.00	0.00	0.01	0.00	21.18	2.00	0.00	0.00	0.01	0.00
21.19	2.00	0.00	0.00	0.01	0.00	21.20	2.00	0.00	0.00	0.01	0.00
21.21	2.00	0.00	0.00	0.01	0.00	21.22	2.00	0.00	0.00	0.01	0.00
21.23	2.00	0.00	0.00	0.01	0.00	21.24	2.00	0.00	0.00	0.01	0.00
21.25	2.00	0.00	0.00	0.01	0.00	21.26	2.00	0.00	0.00	0.01	0.00
21.27	2.00	0.00	0.00	0.01	0.00	21.28	2.00	0.00	0.00	0.01	0.00
21.29	2.00	0.00	0.00	0.01	0.00	21.30	2.00	0.00	0.00	0.01	0.00
21.31	2.00	0.00	0.00	0.01	0.00	21.32	2.00	0.00	0.00	0.01	0.00
21.33	2.00	0.00	0.00	0.01	0.00	21.34	2.00	0.00	0.00	0.01	0.00
21.35	2.00	0.00	0.00	0.01	0.00	21.36	2.00	0.00	0.00	0.01	0.00
21.37	2.00	0.00	0.00	0.01	0.00	21.38	2.00	0.00	0.00	0.01	0.00
21.39	2.00	0.00	0.00	0.01	0.00	21.40	2.00	0.00	0.00	0.01	0.00
21.41	2.00	0.00	0.00	0.01	0.00	21.42	2.00	0.00	0.00	0.01	0.00
21.43	2.00	0.00	0.00	0.01	0.00	21.44	2.00	0.00	0.00	0.01	0.00
21.45	2.00	0.00	0.00	0.01	0.00	21.46	2.00	0.00	0.00	0.01	0.00
21.47	2.00	0.00	0.00	0.01	0.00	21.48	2.00	0.00	0.00	0.01	0.00
21.49	2.00	0.00	0.00	0.01	0.00	21.50	2.00	0.00	0.00	0.01	0.00
21.51	2.00	0.00	0.00	0.01	0.00	21.52	2.00	0.00	0.00	0.01	0.00
21.53	2.00	0.00	0.00	0.01	0.00	21.54	2.00	0.00	0.00	0.01	0.00
21.55	2.00	0.00	0.00	0.01	0.00	21.56	2.00	0.00	0.00	0.01	0.00
21.57	2.00	0.00	0.00	0.01	0.00	21.58	2.00	0.00	0.00	0.01	0.00
21.59	2.00	0.00	0.00	0.01	0.00	21.60	2.00	0.00	0.00	0.01	0.00
21.61	2.00	0.00	0.00	0.01	0.00	21.62	2.00	0.00	0.00	0.01	0.00
21.63	2.00	0.00	0.00	0.01	0.00	21.64	2.00	0.00	0.00	0.01	0.00
21.65	2.00	0.00	0.00	0.01	0.00	21.66	2.00	0.00	0.00	0.01	0.00
21.67	2.00	0.00	0.00	0.01	0.00	21.68	2.00	0.00	0.00	0.01	0.00
21.69	2.00	0.00	0.00	0.01	0.00	21.70	2.00	0.00	0.00	0.01	0.00
21.71	2.00	0.00	0.00	0.01	0.00	21.72	2.00	0.00	0.00	0.01	0.00
21.73	2.00	0.00	0.00	0.01	0.00	21.74	2.00	0.00	0.00	0.01	0.00
21.75	2.00	0.00	0.00	0.01	0.00	21.76	2.00	0.00	0.00	0.01	0.00
21.77	2.00	0.00	0.00	0.01	0.00	21.78	2.00	0.00	0.00	0.01	0.00
21.79	2.00	0.00	0.00	0.01	0.00	21.80	2.00	0.00	0.00	0.01	0.00
21.81	2.00	0.00	0.00	0.01	0.00	21.82	2.00	0.00	0.00	0.01	0.00
21.83	2.00	0.00	0.00	0.01	0.00	21.84	2.00	0.00	0.00	0.01	0.00
21.85	2.00	0.00	0.00	0.01	0.00	21.86	2.00	0.00	0.00	0.01	0.00
21.87	2.00	0.00	0.00	0.01	0.00	21.88	2.00	0.00	0.00	0.01	0.00
21.89	2.00	0.00	0.00	0.01	0.00	21.90	2.00	0.00	0.00	0.01	0.00
21.91	2.00	0.00	0.00	0.01	0.00	21.92	2.00	0.00	0.00	0.01	0.00
21.93	2.00	0.00	0.00	0.01	0.00	21.94	2.00	0.00	0.00	0.01	0.00
21.95	2.00	0.00	0.00	0.01	0.00	21.96	2.00	0.00	0.00	0.01	0.00
21.97	2.00	0.00	0.00	0.01	0.00	21.98	2.00	0.00	0.00	0.01	0.00
21.99	2.00	0.00	0.00	0.01	0.00	22.00	2.00	0.00	0.00	0.01	0.00
22.01	2.00	0.00	0.00	0.01	0.00	22.02	2.00	0.00	0.00	0.01	0.00
22.03	2.00	0.00	0.00	0.01	0.00	22.04	2.00	0.00	0.00	0.01	0.00
22.05	2.00	0.00	0.00	0.01	0.00	22.06	2.00	0.00	0.00	0.01	0.00
22.07	2.00	0.00	0.00	0.01	0.00	22.08	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
22.09	2.00	0.00	0.00	0.01	0.00	22.10	2.00	0.00	0.00	0.01	0.00
22.11	2.00	0.00	0.00	0.01	0.00	22.12	2.00	0.00	0.00	0.01	0.00
22.13	2.00	0.00	0.00	0.01	0.00	22.14	2.00	0.00	0.00	0.01	0.00
22.15	2.00	0.00	0.00	0.01	0.00	22.16	2.00	0.00	0.00	0.01	0.00
22.17	2.00	0.00	0.00	0.01	0.00	22.18	2.00	0.00	0.00	0.01	0.00
22.19	2.00	0.00	0.00	0.01	0.00	22.20	2.00	0.00	0.00	0.01	0.00
22.21	2.00	0.00	0.00	0.01	0.00	22.22	2.00	0.00	0.00	0.01	0.00
22.23	2.00	0.00	0.00	0.01	0.00	22.24	2.00	0.00	0.00	0.01	0.00
22.25	2.00	0.00	0.00	0.01	0.00	22.26	2.00	0.00	0.00	0.01	0.00
22.27	2.00	0.00	0.00	0.01	0.00	22.28	2.00	0.00	0.00	0.01	0.00
22.29	2.00	0.00	0.00	0.01	0.00	22.30	2.00	0.00	0.00	0.01	0.00
22.31	2.00	0.00	0.00	0.01	0.00	22.32	2.00	0.00	0.00	0.01	0.00
22.33	2.00	0.00	0.00	0.01	0.00	22.34	2.00	0.00	0.00	0.01	0.00
22.35	2.00	0.00	0.00	0.01	0.00	22.36	2.00	0.00	0.00	0.01	0.00
22.37	2.00	0.00	0.00	0.01	0.00	22.38	2.00	0.00	0.00	0.01	0.00
22.39	2.00	0.00	0.00	0.01	0.00	22.40	2.00	0.00	0.00	0.01	0.00
22.41	2.00	0.00	0.00	0.01	0.00	22.42	2.00	0.00	0.00	0.01	0.00
22.43	2.00	0.00	0.00	0.01	0.00	22.44	2.00	0.00	0.00	0.01	0.00
22.45	2.00	0.00	0.00	0.01	0.00	22.46	2.00	0.00	0.00	0.01	0.00
22.47	2.00	0.00	0.00	0.01	0.00	22.48	2.00	0.00	0.00	0.01	0.00
22.49	2.00	0.00	0.00	0.01	0.00	22.50	2.00	0.00	0.00	0.01	0.00
22.51	2.00	0.00	0.00	0.01	0.00	22.52	2.00	0.00	0.00	0.01	0.00
22.53	2.00	0.00	0.00	0.01	0.00	22.54	2.00	0.00	0.00	0.01	0.00
22.55	2.00	0.00	0.00	0.01	0.00	22.56	2.00	0.00	0.00	0.01	0.00
22.57	2.00	0.00	0.00	0.01	0.00	22.58	2.00	0.00	0.00	0.01	0.00
22.59	2.00	0.00	0.00	0.01	0.00	22.60	2.00	0.00	0.00	0.01	0.00
22.61	2.00	0.00	0.00	0.01	0.00	22.62	2.00	0.00	0.00	0.01	0.00
22.63	2.00	0.00	0.00	0.01	0.00	22.64	2.00	0.00	0.00	0.01	0.00
22.65	2.00	0.00	0.00	0.01	0.00	22.66	2.00	0.00	0.00	0.01	0.00
22.67	2.00	0.00	0.00	0.01	0.00	22.68	2.00	0.00	0.00	0.01	0.00
22.69	2.00	0.00	0.00	0.01	0.00	22.70	2.00	0.00	0.00	0.01	0.00
22.71	2.00	0.00	0.00	0.01	0.00	22.72	2.00	0.00	0.00	0.01	0.00
22.73	2.00	0.00	0.00	0.01	0.00	22.74	2.00	0.00	0.00	0.01	0.00
22.75	2.00	0.00	0.00	0.01	0.00	22.76	2.00	0.00	0.00	0.01	0.00
22.77	1.91	0.00	0.00	0.01	0.00	22.78	1.94	0.00	0.00	0.01	0.00
22.79	1.88	0.00	0.00	0.01	0.00	22.80	2.00	0.00	0.00	0.01	0.00
22.81	1.98	0.00	0.00	0.01	0.00	22.82	2.00	0.00	0.00	0.01	0.00
22.83	2.00	0.00	0.00	0.01	0.00	22.84	2.00	0.00	0.00	0.01	0.00
22.85	2.00	0.00	0.00	0.01	0.00	22.86	2.00	0.00	0.00	0.01	0.00
22.87	2.00	0.00	0.00	0.01	0.00	22.88	2.00	0.00	0.00	0.01	0.00
22.89	2.00	0.00	0.00	0.01	0.00	22.90	2.00	0.00	0.00	0.01	0.00
22.91	2.00	0.00	0.00	0.01	0.00	22.92	2.00	0.00	0.00	0.01	0.00
22.93	2.00	0.00	0.00	0.01	0.00	22.94	2.00	0.00	0.00	0.01	0.00
22.95	2.00	0.00	0.00	0.01	0.00	22.96	2.00	0.00	0.00	0.01	0.00
22.97	2.00	0.00	0.00	0.01	0.00	22.98	2.00	0.00	0.00	0.01	0.00
22.99	2.00	0.00	0.00	0.01	0.00	23.00	2.00	0.00	0.00	0.01	0.00
23.01	2.00	0.00	0.00	0.01	0.00	23.02	2.00	0.00	0.00	0.01	0.00
23.03	2.00	0.00	0.00	0.01	0.00	23.04	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
23.05	2.00	0.00	0.00	0.01	0.00	23.06	2.00	0.00	0.00	0.01	0.00
23.07	2.00	0.00	0.00	0.01	0.00	23.08	2.00	0.00	0.00	0.01	0.00
23.09	2.00	0.00	0.00	0.01	0.00	23.10	2.00	0.00	0.00	0.01	0.00
23.11	2.00	0.00	0.00	0.01	0.00	23.12	2.00	0.00	0.00	0.01	0.00
23.13	2.00	0.00	0.00	0.01	0.00	23.14	2.00	0.00	0.00	0.01	0.00
23.15	2.00	0.00	0.00	0.01	0.00	23.16	2.00	0.00	0.00	0.01	0.00
23.17	2.00	0.00	0.00	0.01	0.00	23.18	2.00	0.00	0.00	0.01	0.00
23.19	2.00	0.00	0.00	0.01	0.00	23.20	2.00	0.00	0.00	0.01	0.00
23.21	2.00	0.00	0.00	0.01	0.00	23.22	2.00	0.00	0.00	0.01	0.00
23.23	2.00	0.00	0.00	0.01	0.00	23.24	2.00	0.00	0.00	0.01	0.00
23.25	2.00	0.00	0.00	0.01	0.00	23.26	2.00	0.00	0.00	0.01	0.00
23.27	2.00	0.00	0.00	0.01	0.00	23.28	2.00	0.00	0.00	0.01	0.00
23.29	2.00	0.00	0.00	0.01	0.00	23.30	2.00	0.00	0.00	0.01	0.00
23.31	2.00	0.00	0.00	0.01	0.00	23.32	2.00	0.00	0.00	0.01	0.00
23.33	2.00	0.00	0.00	0.01	0.00	23.34	2.00	0.00	0.00	0.01	0.00
23.35	2.00	0.00	0.00	0.01	0.00	23.36	2.00	0.00	0.00	0.01	0.00
23.37	2.00	0.00	0.00	0.01	0.00	23.38	2.00	0.00	0.00	0.01	0.00
23.39	2.00	0.00	0.00	0.01	0.00	23.40	2.00	0.00	0.00	0.01	0.00
23.41	2.00	0.00	0.00	0.01	0.00	23.42	2.00	0.00	0.00	0.01	0.00
23.43	2.00	0.00	0.00	0.01	0.00	23.44	2.00	0.00	0.00	0.01	0.00
23.45	2.00	0.00	0.00	0.01	0.00	23.46	2.00	0.00	0.00	0.01	0.00
23.47	2.00	0.00	0.00	0.01	0.00	23.48	2.00	0.00	0.00	0.01	0.00
23.49	2.00	0.00	0.00	0.01	0.00	23.50	2.00	0.00	0.00	0.01	0.00
23.51	2.00	0.00	0.00	0.01	0.00	23.52	2.00	0.00	0.00	0.01	0.00
23.53	2.00	0.00	0.00	0.01	0.00	23.54	2.00	0.00	0.00	0.01	0.00
23.55	2.00	0.00	0.00	0.01	0.00	23.56	2.00	0.00	0.00	0.01	0.00
23.57	2.00	0.00	0.00	0.01	0.00	23.58	2.00	0.00	0.00	0.01	0.00
23.59	2.00	0.00	0.00	0.01	0.00	23.60	2.00	0.00	0.00	0.01	0.00
23.61	2.00	0.00	0.00	0.01	0.00	23.62	2.00	0.00	0.00	0.01	0.00
23.63	2.00	0.00	0.00	0.01	0.00	23.64	2.00	0.00	0.00	0.01	0.00
23.65	2.00	0.00	0.00	0.01	0.00	23.66	2.00	0.00	0.00	0.01	0.00
23.67	2.00	0.00	0.00	0.01	0.00	23.68	2.00	0.00	0.00	0.01	0.00
23.69	2.00	0.00	0.00	0.01	0.00	23.70	2.00	0.00	0.00	0.01	0.00
23.71	2.00	0.00	0.00	0.01	0.00	23.72	2.00	0.00	0.00	0.01	0.00
23.73	2.00	0.00	0.00	0.01	0.00	23.74	2.00	0.00	0.00	0.01	0.00
23.75	2.00	0.00	0.00	0.01	0.00	23.76	2.00	0.00	0.00	0.01	0.00
23.77	2.00	0.00	0.00	0.01	0.00	23.78	2.00	0.00	0.00	0.01	0.00
23.79	2.00	0.00	0.00	0.01	0.00	23.80	2.00	0.00	0.00	0.01	0.00
23.81	2.00	0.00	0.00	0.01	0.00	23.82	2.00	0.00	0.00	0.01	0.00
23.83	2.00	0.00	0.00	0.01	0.00	23.84	2.00	0.00	0.00	0.01	0.00
23.85	2.00	0.00	0.00	0.01	0.00	23.86	2.00	0.00	0.00	0.01	0.00
23.87	2.00	0.00	0.00	0.01	0.00	23.88	2.00	0.00	0.00	0.01	0.00
23.89	2.00	0.00	0.00	0.01	0.00	23.90	2.00	0.00	0.00	0.01	0.00
23.91	2.00	0.00	0.00	0.01	0.00	23.92	2.00	0.00	0.00	0.01	0.00
23.93	2.00	0.00	0.00	0.01	0.00	23.94	2.00	0.00	0.00	0.01	0.00
23.95	2.00	0.00	0.00	0.01	0.00	23.96	2.00	0.00	0.00	0.01	0.00
23.97	2.00	0.00	0.00	0.01	0.00	23.98	2.00	0.00	0.00	0.01	0.00
23.99	2.00	0.00	0.00	0.01	0.00	24.00	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
24.01	2.00	0.00	0.00	0.01	0.00	24.02	2.00	0.00	0.00	0.01	0.00
24.03	2.00	0.00	0.00	0.01	0.00	24.04	2.00	0.00	0.00	0.01	0.00
24.05	2.00	0.00	0.00	0.01	0.00	24.06	2.00	0.00	0.00	0.01	0.00
24.07	2.00	0.00	0.00	0.01	0.00	24.08	2.00	0.00	0.00	0.01	0.00
24.09	2.00	0.00	0.00	0.01	0.00	24.10	2.00	0.00	0.00	0.01	0.00
24.11	2.00	0.00	0.00	0.01	0.00	24.12	2.00	0.00	0.00	0.01	0.00
24.13	2.00	0.00	0.00	0.01	0.00	24.14	2.00	0.00	0.00	0.01	0.00
24.15	2.00	0.00	0.00	0.01	0.00	24.16	2.00	0.00	0.00	0.01	0.00
24.17	2.00	0.00	0.00	0.01	0.00	24.18	2.00	0.00	0.00	0.01	0.00
24.19	2.00	0.00	0.00	0.01	0.00	24.20	2.00	0.00	0.00	0.01	0.00
24.21	2.00	0.00	0.00	0.01	0.00	24.22	2.00	0.00	0.00	0.01	0.00
24.23	2.00	0.00	0.00	0.01	0.00	24.24	2.00	0.00	0.00	0.01	0.00
24.25	2.00	0.00	0.00	0.01	0.00	24.26	2.00	0.00	0.00	0.01	0.00
24.27	2.00	0.00	0.00	0.01	0.00	24.28	2.00	0.00	0.00	0.01	0.00
24.29	2.00	0.00	0.00	0.01	0.00	24.30	2.00	0.00	0.00	0.01	0.00
24.31	2.00	0.00	0.00	0.01	0.00	24.32	2.00	0.00	0.00	0.01	0.00
24.33	2.00	0.00	0.00	0.01	0.00	24.34	2.00	0.00	0.00	0.01	0.00
24.35	2.00	0.00	0.00	0.01	0.00	24.36	2.00	0.00	0.00	0.01	0.00
24.37	2.00	0.00	0.00	0.01	0.00	24.38	2.00	0.00	0.00	0.01	0.00
24.39	2.00	0.00	0.00	0.01	0.00	24.40	2.00	0.00	0.00	0.01	0.00
24.41	2.00	0.00	0.00	0.01	0.00	24.42	2.00	0.00	0.00	0.01	0.00
24.43	2.00	0.00	0.00	0.01	0.00	24.44	2.00	0.00	0.00	0.01	0.00
24.45	2.00	0.00	0.00	0.01	0.00	24.46	2.00	0.00	0.00	0.01	0.00
24.47	2.00	0.00	0.00	0.01	0.00	24.48	2.00	0.00	0.00	0.01	0.00
24.49	2.00	0.00	0.00	0.01	0.00	24.50	2.00	0.00	0.00	0.01	0.00
24.51	2.00	0.00	0.00	0.01	0.00	24.52	2.00	0.00	0.00	0.01	0.00
24.53	2.00	0.00	0.00	0.01	0.00	24.54	2.00	0.00	0.00	0.01	0.00
24.55	2.00	0.00	0.00	0.01	0.00	24.56	2.00	0.00	0.00	0.01	0.00
24.57	2.00	0.00	0.00	0.01	0.00	24.58	2.00	0.00	0.00	0.01	0.00
24.59	2.00	0.00	0.00	0.01	0.00	24.60	2.00	0.00	0.00	0.01	0.00
24.61	2.00	0.00	0.00	0.01	0.00	24.62	2.00	0.00	0.00	0.01	0.00
24.63	2.00	0.00	0.00	0.01	0.00	24.64	2.00	0.00	0.00	0.01	0.00
24.65	2.00	0.00	0.00	0.01	0.00	24.66	2.00	0.00	0.00	0.01	0.00
24.67	2.00	0.00	0.00	0.01	0.00	24.68	2.00	0.00	0.00	0.01	0.00
24.69	2.00	0.00	0.00	0.01	0.00	24.70	2.00	0.00	0.00	0.01	0.00
24.71	2.00	0.00	0.00	0.01	0.00	24.72	2.00	0.00	0.00	0.01	0.00
24.73	2.00	0.00	0.00	0.01	0.00	24.74	2.00	0.00	0.00	0.01	0.00
24.75	2.00	0.00	0.00	0.01	0.00	24.76	2.00	0.00	0.00	0.01	0.00
24.77	2.00	0.00	0.00	0.01	0.00	24.78	2.00	0.00	0.00	0.01	0.00
24.79	2.00	0.00	0.00	0.01	0.00	24.80	2.00	0.00	0.00	0.01	0.00
24.81	2.00	0.00	0.00	0.01	0.00	24.82	2.00	0.00	0.00	0.01	0.00
24.83	2.00	0.00	0.00	0.01	0.00	24.84	2.00	0.00	0.00	0.01	0.00
24.85	2.00	0.00	0.00	0.01	0.00	24.86	2.00	0.00	0.00	0.01	0.00
24.87	2.00	0.00	0.00	0.01	0.00	24.88	2.00	0.00	0.00	0.01	0.00
24.89	2.00	0.00	0.00	0.01	0.00	24.90	2.00	0.00	0.00	0.01	0.00
24.91	2.00	0.00	0.00	0.01	0.00	24.92	2.00	0.00	0.00	0.01	0.00
24.93	2.00	0.00	0.00	0.01	0.00	24.94	2.00	0.00	0.00	0.01	0.00
24.95	2.00	0.00	0.00	0.01	0.00	24.96	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
24.97	2.00	0.00	0.00	0.01	0.00	24.98	2.00	0.00	0.00	0.01	0.00
24.99	2.00	0.00	0.00	0.01	0.00	25.00	2.00	0.00	0.00	0.01	0.00
25.01	2.00	0.00	0.00	0.01	0.00	25.02	2.00	0.00	0.00	0.01	0.00
25.03	2.00	0.00	0.00	0.01	0.00	25.04	2.00	0.00	0.00	0.01	0.00
25.05	2.00	0.00	0.00	0.01	0.00	25.06	2.00	0.00	0.00	0.01	0.00
25.07	2.00	0.00	0.00	0.01	0.00	25.08	2.00	0.00	0.00	0.01	0.00
25.09	2.00	0.00	0.00	0.01	0.00	25.10	2.00	0.00	0.00	0.01	0.00
25.11	2.00	0.00	0.00	0.01	0.00	25.12	2.00	0.00	0.00	0.01	0.00
25.13	2.00	0.00	0.00	0.01	0.00	25.14	2.00	0.00	0.00	0.01	0.00
25.15	2.00	0.00	0.00	0.01	0.00	25.16	2.00	0.00	0.00	0.01	0.00
25.17	2.00	0.00	0.00	0.01	0.00	25.18	2.00	0.00	0.00	0.01	0.00
25.19	2.00	0.00	0.00	0.01	0.00	25.20	2.00	0.00	0.00	0.01	0.00
25.21	2.00	0.00	0.00	0.01	0.00	25.22	2.00	0.00	0.00	0.01	0.00
25.23	2.00	0.00	0.00	0.01	0.00	25.24	2.00	0.00	0.00	0.01	0.00
25.25	2.00	0.00	0.00	0.01	0.00	25.26	2.00	0.00	0.00	0.01	0.00
25.27	2.00	0.00	0.00	0.01	0.00	25.28	2.00	0.00	0.00	0.01	0.00
25.29	2.00	0.00	0.00	0.01	0.00	25.30	2.00	0.00	0.00	0.01	0.00
25.31	2.00	0.00	0.00	0.01	0.00	25.32	2.00	0.00	0.00	0.01	0.00
25.33	2.00	0.00	0.00	0.01	0.00	25.34	2.00	0.00	0.00	0.01	0.00
25.35	2.00	0.00	0.00	0.01	0.00	25.36	2.00	0.00	0.00	0.01	0.00
25.37	2.00	0.00	0.00	0.01	0.00	25.38	2.00	0.00	0.00	0.01	0.00
25.39	2.00	0.00	0.00	0.01	0.00	25.40	2.00	0.00	0.00	0.01	0.00
25.41	2.00	0.00	0.00	0.01	0.00	25.42	2.00	0.00	0.00	0.01	0.00
25.43	2.00	0.00	0.00	0.01	0.00	25.44	2.00	0.00	0.00	0.01	0.00
25.45	2.00	0.00	0.00	0.01	0.00	25.46	2.00	0.00	0.00	0.01	0.00
25.47	2.00	0.00	0.00	0.01	0.00	25.48	2.00	0.00	0.00	0.01	0.00
25.49	2.00	0.00	0.00	0.01	0.00	25.50	2.00	0.00	0.00	0.01	0.00
25.51	2.00	0.00	0.00	0.01	0.00	25.52	2.00	0.00	0.00	0.01	0.00
25.53	2.00	0.00	0.00	0.01	0.00	25.54	2.00	0.00	0.00	0.01	0.00
25.55	2.00	0.00	0.00	0.01	0.00	25.56	2.00	0.00	0.00	0.01	0.00
25.57	2.00	0.00	0.00	0.01	0.00	25.58	2.00	0.00	0.00	0.01	0.00
25.59	2.00	0.00	0.00	0.01	0.00	25.60	2.00	0.00	0.00	0.01	0.00
25.61	2.00	0.00	0.00	0.01	0.00	25.62	2.00	0.00	0.00	0.01	0.00
25.63	2.00	0.00	0.00	0.01	0.00	25.64	2.00	0.00	0.00	0.01	0.00
25.65	2.00	0.00	0.00	0.01	0.00	25.66	2.00	0.00	0.00	0.01	0.00
25.67	2.00	0.00	0.00	0.01	0.00	25.68	2.00	0.00	0.00	0.01	0.00
25.69	2.00	0.00	0.00	0.01	0.00	25.70	2.00	0.00	0.00	0.01	0.00
25.71	2.00	0.00	0.00	0.01	0.00	25.72	2.00	0.00	0.00	0.01	0.00
25.73	2.00	0.00	0.00	0.01	0.00	25.74	2.00	0.00	0.00	0.01	0.00
25.75	2.00	0.00	0.00	0.01	0.00	25.76	2.00	0.00	0.00	0.01	0.00
25.77	2.00	0.00	0.00	0.01	0.00	25.78	2.00	0.00	0.00	0.01	0.00
25.79	2.00	0.00	0.00	0.01	0.00	25.80	2.00	0.00	0.00	0.01	0.00
25.81	2.00	0.00	0.00	0.01	0.00	25.82	2.00	0.00	0.00	0.01	0.00
25.83	2.00	0.00	0.00	0.01	0.00	25.84	2.00	0.00	0.00	0.01	0.00
25.85	2.00	0.00	0.00	0.01	0.00	25.86	2.00	0.00	0.00	0.01	0.00
25.87	2.00	0.00	0.00	0.01	0.00	25.88	2.00	0.00	0.00	0.01	0.00
25.89	2.00	0.00	0.00	0.01	0.00	25.90	2.00	0.00	0.00	0.01	0.00
25.91	2.00	0.00	0.00	0.01	0.00	25.92	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
25.93	2.00	0.00	0.00	0.01	0.00	25.94	2.00	0.00	0.00	0.01	0.00
25.95	2.00	0.00	0.00	0.01	0.00	25.96	2.00	0.00	0.00	0.01	0.00
25.97	2.00	0.00	0.00	0.01	0.00	25.98	2.00	0.00	0.00	0.01	0.00
25.99	2.00	0.00	0.00	0.01	0.00	26.00	2.00	0.00	0.00	0.01	0.00
26.01	2.00	0.00	0.00	0.01	0.00	26.02	2.00	0.00	0.00	0.01	0.00
26.03	2.00	0.00	0.00	0.01	0.00	26.04	2.00	0.00	0.00	0.01	0.00
26.05	2.00	0.00	0.00	0.01	0.00	26.06	2.00	0.00	0.00	0.01	0.00
26.07	2.00	0.00	0.00	0.01	0.00	26.08	2.00	0.00	0.00	0.01	0.00
26.09	2.00	0.00	0.00	0.01	0.00	26.10	2.00	0.00	0.00	0.01	0.00
26.11	2.00	0.00	0.00	0.01	0.00	26.12	2.00	0.00	0.00	0.01	0.00
26.13	2.00	0.00	0.00	0.01	0.00	26.14	2.00	0.00	0.00	0.01	0.00
26.15	2.00	0.00	0.00	0.01	0.00	26.16	2.00	0.00	0.00	0.01	0.00
26.17	2.00	0.00	0.00	0.01	0.00	26.18	2.00	0.00	0.00	0.01	0.00
26.19	2.00	0.00	0.00	0.01	0.00	26.20	2.00	0.00	0.00	0.01	0.00
26.21	2.00	0.00	0.00	0.01	0.00	26.22	2.00	0.00	0.00	0.01	0.00
26.23	2.00	0.00	0.00	0.01	0.00	26.24	2.00	0.00	0.00	0.01	0.00
26.25	2.00	0.00	0.00	0.01	0.00	26.26	2.00	0.00	0.00	0.01	0.00
26.27	2.00	0.00	0.00	0.01	0.00	26.28	2.00	0.00	0.00	0.01	0.00
26.29	2.00	0.00	0.00	0.01	0.00	26.30	2.00	0.00	0.00	0.01	0.00
26.31	2.00	0.00	0.00	0.01	0.00	26.32	2.00	0.00	0.00	0.01	0.00
26.33	2.00	0.00	0.00	0.01	0.00	26.34	2.00	0.00	0.00	0.01	0.00
26.35	2.00	0.00	0.00	0.01	0.00	26.36	2.00	0.00	0.00	0.01	0.00
26.37	2.00	0.00	0.00	0.01	0.00	26.38	2.00	0.00	0.00	0.01	0.00
26.39	2.00	0.00	0.00	0.01	0.00	26.40	2.00	0.00	0.00	0.01	0.00
26.41	2.00	0.00	0.00	0.01	0.00	26.42	2.00	0.00	0.00	0.01	0.00
26.43	2.00	0.00	0.00	0.01	0.00	26.44	2.00	0.00	0.00	0.01	0.00
26.45	2.00	0.00	0.00	0.01	0.00	26.46	2.00	0.00	0.00	0.01	0.00
26.47	2.00	0.00	0.00	0.01	0.00	26.48	2.00	0.00	0.00	0.01	0.00
26.49	2.00	0.00	0.00	0.01	0.00	26.50	2.00	0.00	0.00	0.01	0.00
26.51	2.00	0.00	0.00	0.01	0.00	26.52	2.00	0.00	0.00	0.01	0.00
26.53	2.00	0.00	0.00	0.01	0.00	26.54	2.00	0.00	0.00	0.01	0.00
26.55	2.00	0.00	0.00	0.01	0.00	26.56	2.00	0.00	0.00	0.01	0.00
26.57	2.00	0.00	0.00	0.01	0.00	26.58	2.00	0.00	0.00	0.01	0.00
26.59	2.00	0.00	0.00	0.01	0.00	26.60	2.00	0.00	0.00	0.01	0.00
26.61	2.00	0.00	0.00	0.01	0.00	26.62	2.00	0.00	0.00	0.01	0.00
26.63	2.00	0.00	0.00	0.01	0.00	26.64	2.00	0.00	0.00	0.01	0.00
26.65	2.00	0.00	0.00	0.01	0.00	26.66	2.00	0.00	0.00	0.01	0.00
26.67	2.00	0.00	0.00	0.01	0.00	26.68	2.00	0.00	0.00	0.01	0.00
26.69	2.00	0.00	0.00	0.01	0.00	26.70	2.00	0.00	0.00	0.01	0.00
26.71	2.00	0.00	0.00	0.01	0.00	26.72	2.00	0.00	0.00	0.01	0.00
26.73	2.00	0.00	0.00	0.01	0.00	26.74	2.00	0.00	0.00	0.01	0.00
26.75	2.00	0.00	0.00	0.01	0.00	26.76	2.00	0.00	0.00	0.01	0.00
26.77	2.00	0.00	0.00	0.01	0.00	26.78	2.00	0.00	0.00	0.01	0.00
26.79	2.00	0.00	0.00	0.01	0.00	26.80	2.00	0.00	0.00	0.01	0.00
26.81	2.00	0.00	0.00	0.01	0.00	26.82	2.00	0.00	0.00	0.01	0.00
26.83	2.00	0.00	0.00	0.01	0.00	26.84	2.00	0.00	0.00	0.01	0.00
26.85	2.00	0.00	0.00	0.01	0.00	26.86	2.00	0.00	0.00	0.01	0.00
26.87	2.00	0.00	0.00	0.01	0.00	26.88	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
26.89	2.00	0.00	0.00	0.01	0.00	26.90	2.00	0.00	0.00	0.01	0.00
26.91	2.00	0.00	0.00	0.01	0.00	26.92	2.00	0.00	0.00	0.01	0.00
26.93	2.00	0.00	0.00	0.01	0.00	26.94	2.00	0.00	0.00	0.01	0.00
26.95	2.00	0.00	0.00	0.01	0.00	26.96	2.00	0.00	0.00	0.01	0.00
26.97	2.00	0.00	0.00	0.01	0.00	26.98	2.00	0.00	0.00	0.01	0.00
26.99	2.00	0.00	0.00	0.01	0.00	27.00	2.00	0.00	0.00	0.01	0.00
27.01	2.00	0.00	0.00	0.01	0.00	27.02	2.00	0.00	0.00	0.01	0.00
27.03	2.00	0.00	0.00	0.01	0.00	27.04	2.00	0.00	0.00	0.01	0.00
27.05	2.00	0.00	0.00	0.01	0.00	27.06	2.00	0.00	0.00	0.01	0.00
27.07	2.00	0.00	0.00	0.01	0.00	27.08	2.00	0.00	0.00	0.01	0.00
27.09	2.00	0.00	0.00	0.01	0.00	27.10	2.00	0.00	0.00	0.01	0.00
27.11	2.00	0.00	0.00	0.01	0.00	27.12	2.00	0.00	0.00	0.01	0.00
27.13	2.00	0.00	0.00	0.01	0.00	27.14	2.00	0.00	0.00	0.01	0.00
27.15	2.00	0.00	0.00	0.01	0.00	27.16	2.00	0.00	0.00	0.01	0.00
27.17	2.00	0.00	0.00	0.01	0.00	27.18	2.00	0.00	0.00	0.01	0.00
27.19	2.00	0.00	0.00	0.01	0.00	27.20	2.00	0.00	0.00	0.01	0.00
27.21	2.00	0.00	0.00	0.01	0.00	27.22	2.00	0.00	0.00	0.01	0.00
27.23	2.00	0.00	0.00	0.01	0.00	27.24	2.00	0.00	0.00	0.01	0.00
27.25	2.00	0.00	0.00	0.01	0.00	27.26	2.00	0.00	0.00	0.01	0.00
27.27	2.00	0.00	0.00	0.01	0.00	27.28	2.00	0.00	0.00	0.01	0.00
27.29	2.00	0.00	0.00	0.01	0.00	27.30	2.00	0.00	0.00	0.01	0.00
27.31	2.00	0.00	0.00	0.01	0.00	27.32	2.00	0.00	0.00	0.01	0.00
27.33	2.00	0.00	0.00	0.01	0.00	27.34	2.00	0.00	0.00	0.01	0.00
27.35	2.00	0.00	0.00	0.01	0.00	27.36	2.00	0.00	0.00	0.01	0.00
27.37	2.00	0.00	0.00	0.01	0.00	27.38	2.00	0.00	0.00	0.01	0.00
27.39	2.00	0.00	0.00	0.01	0.00	27.40	2.00	0.00	0.00	0.01	0.00
27.41	2.00	0.00	0.00	0.01	0.00	27.42	2.00	0.00	0.00	0.01	0.00
27.43	2.00	0.00	0.00	0.01	0.00	27.44	2.00	0.00	0.00	0.01	0.00
27.45	2.00	0.00	0.00	0.01	0.00	27.46	2.00	0.00	0.00	0.01	0.00
27.47	2.00	0.00	0.00	0.01	0.00	27.48	2.00	0.00	0.00	0.01	0.00
27.49	2.00	0.00	0.00	0.01	0.00	27.50	2.00	0.00	0.00	0.01	0.00
27.51	2.00	0.00	0.00	0.01	0.00	27.52	2.00	0.00	0.00	0.01	0.00
27.53	2.00	0.00	0.00	0.01	0.00	27.54	2.00	0.00	0.00	0.01	0.00
27.55	2.00	0.00	0.00	0.01	0.00	27.56	2.00	0.00	0.00	0.01	0.00
27.57	2.00	0.00	0.00	0.01	0.00	27.58	2.00	0.00	0.00	0.01	0.00
27.59	2.00	0.00	0.00	0.01	0.00	27.60	2.00	0.00	0.00	0.01	0.00
27.61	2.00	0.00	0.00	0.01	0.00	27.62	2.00	0.00	0.00	0.01	0.00
27.63	2.00	0.00	0.00	0.01	0.00	27.64	2.00	0.00	0.00	0.01	0.00
27.65	2.00	0.00	0.00	0.01	0.00	27.66	2.00	0.00	0.00	0.01	0.00
27.67	2.00	0.00	0.00	0.01	0.00	27.68	2.00	0.00	0.00	0.01	0.00
27.69	2.00	0.00	0.00	0.01	0.00	27.70	2.00	0.00	0.00	0.01	0.00
27.71	2.00	0.00	0.00	0.01	0.00	27.72	2.00	0.00	0.00	0.01	0.00
27.73	2.00	0.00	0.00	0.01	0.00	27.74	2.00	0.00	0.00	0.01	0.00
27.75	2.00	0.00	0.00	0.01	0.00	27.76	2.00	0.00	0.00	0.01	0.00
27.77	2.00	0.00	0.00	0.01	0.00	27.78	2.00	0.00	0.00	0.01	0.00
27.79	2.00	0.00	0.00	0.01	0.00	27.80	2.00	0.00	0.00	0.01	0.00
27.81	2.00	0.00	0.00	0.01	0.00	27.82	2.00	0.00	0.00	0.01	0.00
27.83	2.00	0.00	0.00	0.01	0.00	27.84	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
27.85	2.00	0.00	0.00	0.01	0.00	27.86	2.00	0.00	0.00	0.01	0.00
27.87	2.00	0.00	0.00	0.01	0.00	27.88	2.00	0.00	0.00	0.01	0.00
27.89	2.00	0.00	0.00	0.01	0.00	27.90	2.00	0.00	0.00	0.01	0.00
27.91	2.00	0.00	0.00	0.01	0.00	27.92	2.00	0.00	0.00	0.01	0.00
27.93	2.00	0.00	0.00	0.01	0.00	27.94	2.00	0.00	0.00	0.01	0.00
27.95	2.00	0.00	0.00	0.01	0.00	27.96	2.00	0.00	0.00	0.01	0.00
27.97	2.00	0.00	0.00	0.01	0.00	27.98	2.00	0.00	0.00	0.01	0.00
27.99	2.00	0.00	0.00	0.01	0.00	28.00	2.00	0.00	0.00	0.01	0.00
28.01	2.00	0.00	0.00	0.01	0.00	28.02	2.00	0.00	0.00	0.01	0.00
28.03	2.00	0.00	0.00	0.01	0.00	28.04	2.00	0.00	0.00	0.01	0.00
28.05	2.00	0.00	0.00	0.01	0.00	28.06	2.00	0.00	0.00	0.01	0.00
28.07	2.00	0.00	0.00	0.01	0.00	28.08	2.00	0.00	0.00	0.01	0.00
28.09	2.00	0.00	0.00	0.01	0.00	28.10	2.00	0.00	0.00	0.01	0.00
28.11	2.00	0.00	0.00	0.01	0.00	28.12	2.00	0.00	0.00	0.01	0.00
28.13	2.00	0.00	0.00	0.01	0.00	28.14	2.00	0.00	0.00	0.01	0.00
28.15	2.00	0.00	0.00	0.01	0.00	28.16	2.00	0.00	0.00	0.01	0.00
28.17	2.00	0.00	0.00	0.01	0.00	28.18	2.00	0.00	0.00	0.01	0.00
28.19	2.00	0.00	0.00	0.01	0.00	28.20	2.00	0.00	0.00	0.01	0.00
28.21	2.00	0.00	0.00	0.01	0.00	28.22	2.00	0.00	0.00	0.01	0.00
28.23	2.00	0.00	0.00	0.01	0.00	28.24	2.00	0.00	0.00	0.01	0.00
28.25	2.00	0.00	0.00	0.01	0.00	28.26	2.00	0.00	0.00	0.01	0.00
28.27	2.00	0.00	0.00	0.01	0.00	28.28	2.00	0.00	0.00	0.01	0.00
28.29	2.00	0.00	0.00	0.01	0.00	28.30	2.00	0.00	0.00	0.01	0.00
28.31	2.00	0.00	0.00	0.01	0.00	28.32	2.00	0.00	0.00	0.01	0.00
28.33	2.00	0.00	0.00	0.01	0.00	28.34	2.00	0.00	0.00	0.01	0.00
28.35	2.00	0.00	0.00	0.01	0.00	28.36	2.00	0.00	0.00	0.01	0.00
28.37	2.00	0.00	0.00	0.01	0.00	28.38	2.00	0.00	0.00	0.01	0.00
28.39	2.00	0.00	0.00	0.01	0.00	28.40	2.00	0.00	0.00	0.01	0.00
28.41	2.00	0.00	0.00	0.01	0.00	28.42	2.00	0.00	0.00	0.01	0.00
28.43	2.00	0.00	0.00	0.01	0.00	28.44	2.00	0.00	0.00	0.01	0.00
28.45	2.00	0.00	0.00	0.01	0.00	28.46	2.00	0.00	0.00	0.01	0.00
28.47	2.00	0.00	0.00	0.01	0.00	28.48	2.00	0.00	0.00	0.01	0.00
28.49	2.00	0.00	0.00	0.01	0.00	28.50	2.00	0.00	0.00	0.01	0.00
28.51	2.00	0.00	0.00	0.01	0.00	28.52	2.00	0.00	0.00	0.01	0.00
28.53	2.00	0.00	0.00	0.01	0.00	28.54	2.00	0.00	0.00	0.01	0.00
28.55	2.00	0.00	0.00	0.01	0.00	28.56	2.00	0.00	0.00	0.01	0.00
28.57	2.00	0.00	0.00	0.01	0.00	28.58	2.00	0.00	0.00	0.01	0.00
28.59	2.00	0.00	0.00	0.01	0.00	28.60	2.00	0.00	0.00	0.01	0.00
28.61	2.00	0.00	0.00	0.01	0.00	28.62	2.00	0.00	0.00	0.01	0.00
28.63	2.00	0.00	0.00	0.01	0.00	28.64	2.00	0.00	0.00	0.01	0.00
28.65	2.00	0.00	0.00	0.01	0.00	28.66	2.00	0.00	0.00	0.01	0.00
28.67	2.00	0.00	0.00	0.01	0.00	28.68	2.00	0.00	0.00	0.01	0.00
28.69	2.00	0.00	0.00	0.01	0.00	28.70	2.00	0.00	0.00	0.01	0.00
28.71	2.00	0.00	0.00	0.01	0.00	28.72	2.00	0.00	0.00	0.01	0.00
28.73	2.00	0.00	0.00	0.01	0.00	28.74	2.00	0.00	0.00	0.01	0.00
28.75	2.00	0.00	0.00	0.01	0.00	28.76	2.00	0.00	0.00	0.01	0.00
28.77	2.00	0.00	0.00	0.01	0.00	28.78	2.00	0.00	0.00	0.01	0.00
28.79	2.00	0.00	0.00	0.01	0.00	28.80	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
28.81	2.00	0.00	0.00	0.01	0.00	28.82	2.00	0.00	0.00	0.01	0.00
28.83	2.00	0.00	0.00	0.01	0.00	28.84	2.00	0.00	0.00	0.01	0.00
28.85	2.00	0.00	0.00	0.01	0.00	28.86	2.00	0.00	0.00	0.01	0.00
28.87	2.00	0.00	0.00	0.01	0.00	28.88	2.00	0.00	0.00	0.01	0.00
28.89	2.00	0.00	0.00	0.01	0.00	28.90	2.00	0.00	0.00	0.01	0.00
28.91	2.00	0.00	0.00	0.01	0.00	28.92	2.00	0.00	0.00	0.01	0.00
28.93	2.00	0.00	0.00	0.01	0.00	28.94	2.00	0.00	0.00	0.01	0.00
28.95	2.00	0.00	0.00	0.01	0.00	28.96	2.00	0.00	0.00	0.01	0.00
28.97	2.00	0.00	0.00	0.01	0.00	28.98	2.00	0.00	0.00	0.01	0.00
28.99	2.00	0.00	0.00	0.01	0.00	29.00	2.00	0.00	0.00	0.01	0.00
29.01	2.00	0.00	0.00	0.01	0.00	29.02	2.00	0.00	0.00	0.01	0.00
29.03	2.00	0.00	0.00	0.01	0.00	29.04	2.00	0.00	0.00	0.01	0.00
29.05	2.00	0.00	0.00	0.01	0.00	29.06	2.00	0.00	0.00	0.01	0.00
29.07	2.00	0.00	0.00	0.01	0.00	29.08	2.00	0.00	0.00	0.01	0.00
29.09	2.00	0.00	0.00	0.01	0.00	29.10	2.00	0.00	0.00	0.01	0.00
29.11	2.00	0.00	0.00	0.01	0.00	29.12	2.00	0.00	0.00	0.01	0.00
29.13	2.00	0.00	0.00	0.01	0.00	29.14	2.00	0.00	0.00	0.01	0.00
29.15	2.00	0.00	0.00	0.01	0.00	29.16	2.00	0.00	0.00	0.01	0.00
29.17	2.00	0.00	0.00	0.01	0.00	29.18	2.00	0.00	0.00	0.01	0.00
29.19	2.00	0.00	0.00	0.01	0.00	29.20	2.00	0.00	0.00	0.01	0.00
29.21	2.00	0.00	0.00	0.01	0.00	29.22	2.00	0.00	0.00	0.01	0.00
29.23	2.00	0.00	0.00	0.01	0.00	29.24	2.00	0.00	0.00	0.01	0.00
29.25	2.00	0.00	0.00	0.01	0.00	29.26	2.00	0.00	0.00	0.01	0.00
29.27	2.00	0.00	0.00	0.01	0.00	29.28	2.00	0.00	0.00	0.01	0.00
29.29	2.00	0.00	0.00	0.01	0.00	29.30	2.00	0.00	0.00	0.01	0.00
29.31	2.00	0.00	0.00	0.01	0.00	29.32	2.00	0.00	0.00	0.01	0.00
29.33	2.00	0.00	0.00	0.01	0.00	29.34	2.00	0.00	0.00	0.01	0.00
29.35	2.00	0.00	0.00	0.01	0.00	29.36	2.00	0.00	0.00	0.01	0.00
29.37	2.00	0.00	0.00	0.01	0.00	29.38	2.00	0.00	0.00	0.01	0.00
29.39	2.00	0.00	0.00	0.01	0.00	29.40	2.00	0.00	0.00	0.01	0.00
29.41	2.00	0.00	0.00	0.01	0.00	29.42	2.00	0.00	0.00	0.01	0.00
29.43	2.00	0.00	0.00	0.01	0.00	29.44	2.00	0.00	0.00	0.01	0.00
29.45	2.00	0.00	0.00	0.01	0.00	29.46	2.00	0.00	0.00	0.01	0.00
29.47	2.00	0.00	0.00	0.01	0.00	29.48	2.00	0.00	0.00	0.01	0.00
29.49	2.00	0.00	0.00	0.01	0.00	29.50	2.00	0.00	0.00	0.01	0.00
29.51	2.00	0.00	0.00	0.01	0.00	29.52	2.00	0.00	0.00	0.01	0.00
29.53	2.00	0.00	0.00	0.01	0.00	29.54	2.00	0.00	0.00	0.01	0.00
29.55	2.00	0.00	0.00	0.01	0.00	29.56	2.00	0.00	0.00	0.01	0.00
29.57	2.00	0.00	0.00	0.01	0.00	29.58	2.00	0.00	0.00	0.01	0.00
29.59	2.00	0.00	0.00	0.01	0.00	29.60	2.00	0.00	0.00	0.01	0.00
29.61	2.00	0.00	0.00	0.01	0.00	29.62	2.00	0.00	0.00	0.01	0.00
29.63	2.00	0.00	0.00	0.01	0.00	29.64	2.00	0.00	0.00	0.01	0.00
29.65	2.00	0.00	0.00	0.01	0.00	29.66	2.00	0.00	0.00	0.01	0.00
29.67	2.00	0.00	0.00	0.01	0.00	29.68	2.00	0.00	0.00	0.01	0.00
29.69	2.00	0.00	0.00	0.01	0.00	29.70	2.00	0.00	0.00	0.01	0.00
29.71	2.00	0.00	0.00	0.01	0.00	29.72	2.00	0.00	0.00	0.01	0.00
29.73	2.00	0.00	0.00	0.01	0.00	29.74	2.00	0.00	0.00	0.01	0.00
29.75	2.00	0.00	0.00	0.01	0.00	29.76	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
29.77	2.00	0.00	0.00	0.01	0.00	29.78	2.00	0.00	0.00	0.01	0.00
29.79	2.00	0.00	0.00	0.01	0.00	29.80	2.00	0.00	0.00	0.01	0.00
29.81	2.00	0.00	0.00	0.01	0.00	29.82	2.00	0.00	0.00	0.01	0.00
29.83	2.00	0.00	0.00	0.01	0.00	29.84	2.00	0.00	0.00	0.01	0.00
29.85	2.00	0.00	0.00	0.01	0.00	29.86	2.00	0.00	0.00	0.01	0.00
29.87	2.00	0.00	0.00	0.01	0.00	29.88	2.00	0.00	0.00	0.01	0.00
29.89	2.00	0.00	0.00	0.01	0.00	29.90	2.00	0.00	0.00	0.01	0.00
29.91	2.00	0.00	0.00	0.01	0.00	29.92	2.00	0.00	0.00	0.01	0.00
29.93	2.00	0.00	0.00	0.01	0.00	29.94	2.00	0.00	0.00	0.01	0.00
29.95	2.00	0.00	0.00	0.01	0.00	29.96	2.00	0.00	0.00	0.01	0.00
29.97	2.00	0.00	0.00	0.01	0.00	29.98	2.00	0.00	0.00	0.01	0.00
29.99	2.00	0.00	0.00	0.01	0.00	30.00	2.00	0.00	0.00	0.01	0.00

Overall liquefaction potential: 0.03

LPI_{ISH} > 5.0 - Liquefaction manifestation is expected

Abbreviations

FS: Calculated factor of safety for test point
d_z: Layer thickness (m)
LPI: Liquefaction potential index value for test point

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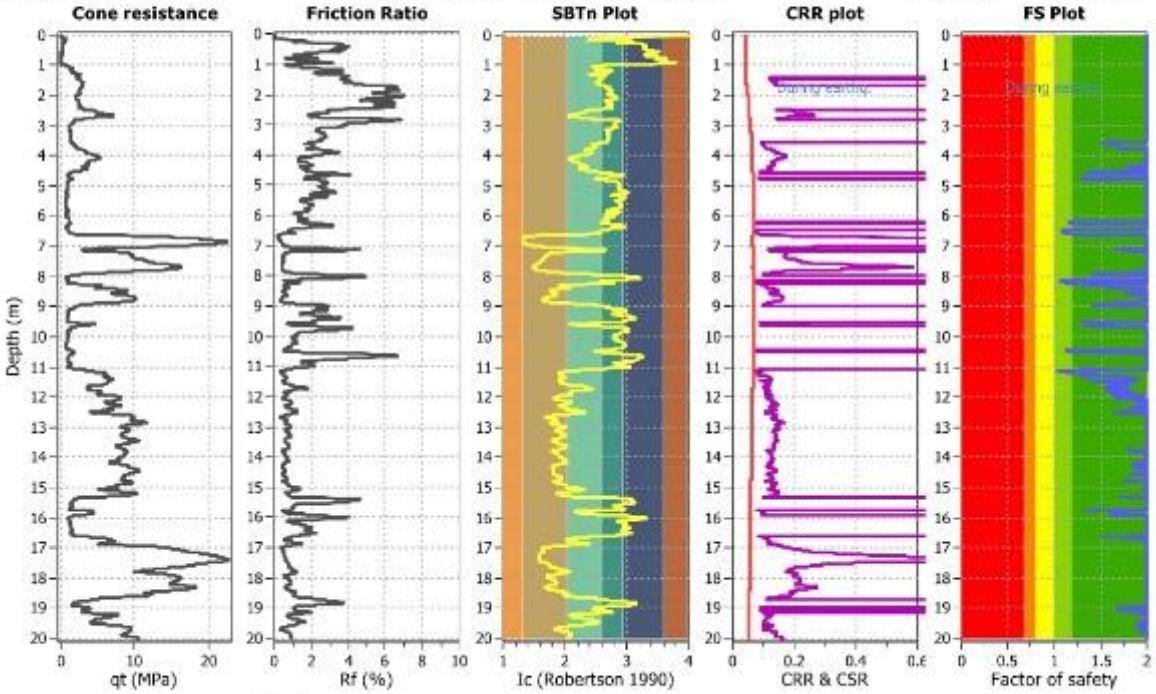
LIQUEFACTION ANALYSIS REPORT

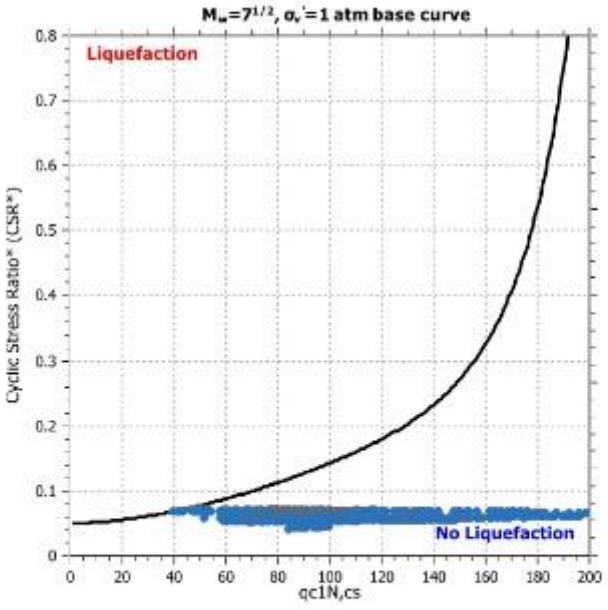
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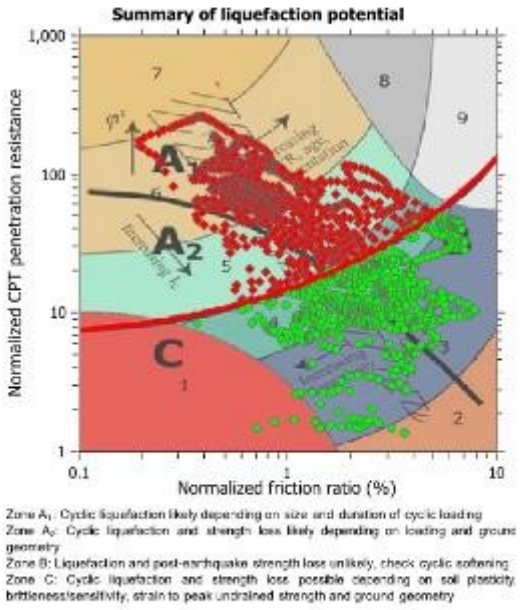
CPT file : CPTU2 - Basic

Input parameters and analysis data

Analysis method:	I&B (2008)	G.W.T. (in-situ):	1.40 m	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	R&W (1998)	G.W.T. (earthq.):	1.40 m	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	5.45	Ic cut-off value:	2.60	Trans. detect. applied:	No	MSF method:	Method based
Peak ground acceleration:	0.12	Unit weight calculation:	Based on SBT	K_o applied:	Yes		

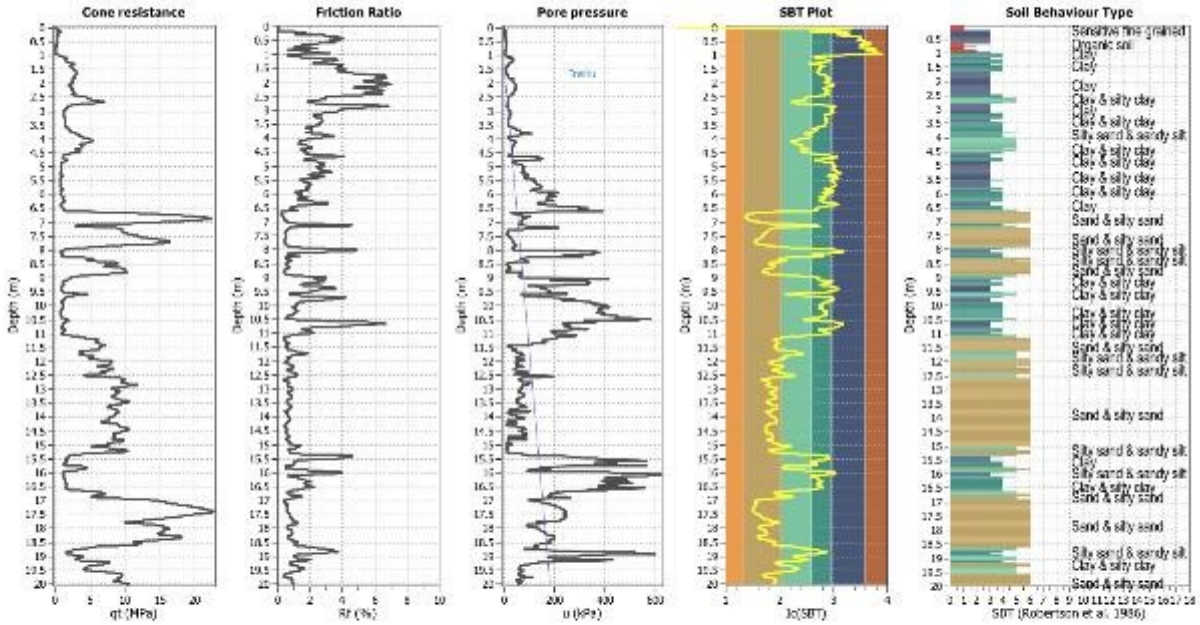






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



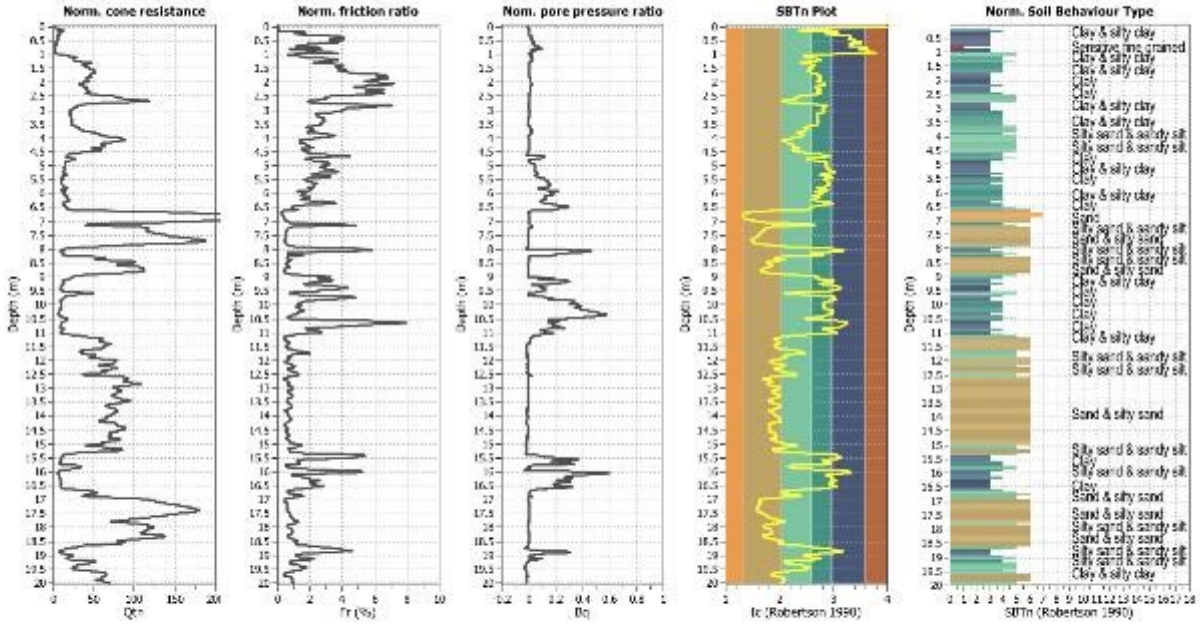
Input parameters and analysis data

Analysis method:	ISBI (2016)	Depth to GWT (erthq.):	1.40 m	Fill weight:	N/A
Fines correction method:	RAW (1998)	Average results interval:	3	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w:	5.45	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.12	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.40 m	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravelly sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



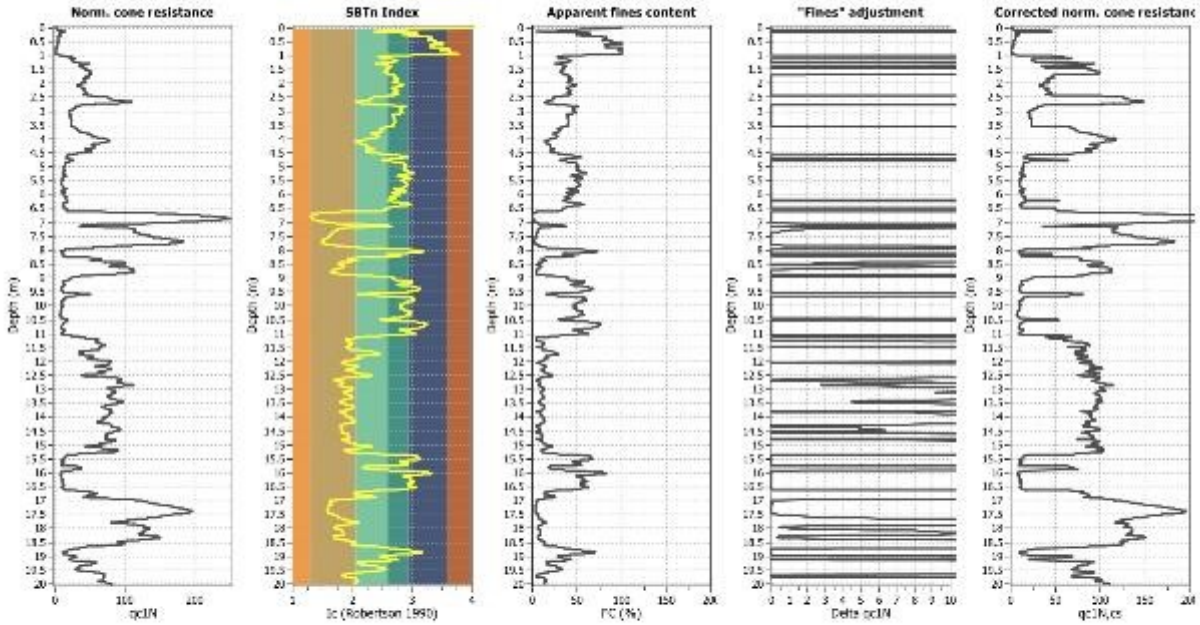
Input parameters and analysis data

Analysis method:	ISBI (2016)	Depth to GWT (erthq.):	1.40 m	Fill weight:	N/A
Fines correction method:	RAW (1998)	Average results interval:	3	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w:	5.45	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.12	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.40 m	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravelly sand to sand
8. Very stiff sand to
9. Very stiff fine grained

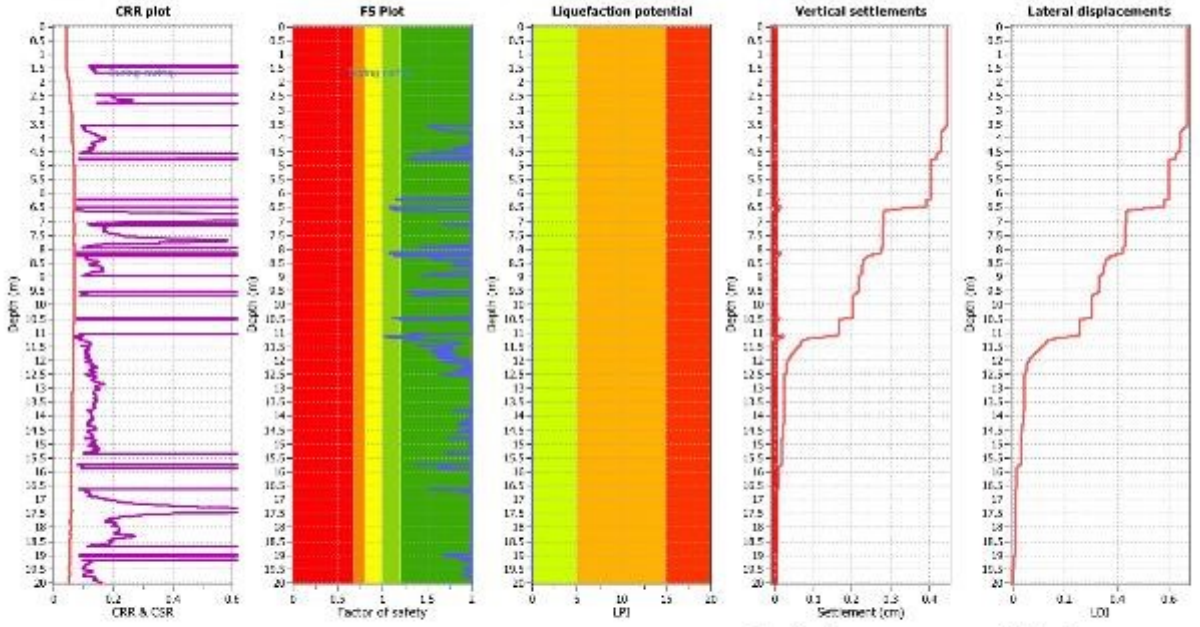
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	IBB (2016)	Depth to GWT (erthq.):	1.40 m	Fill weight:	N/A
Flow correction method:	RAW (1998)	Average results interval:	3	Transition layers applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w:	5.45	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.12	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.40 m	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	IBB (2016)	Depth to GWT (erthq.):	1.40 m	Fill weight:	N/A
Flow correction method:	RAW (1998)	Average results interval:	3	Transition layers applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w:	5.45	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.12	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.40 m	Fill height:	N/A	Limit depth:	N/A

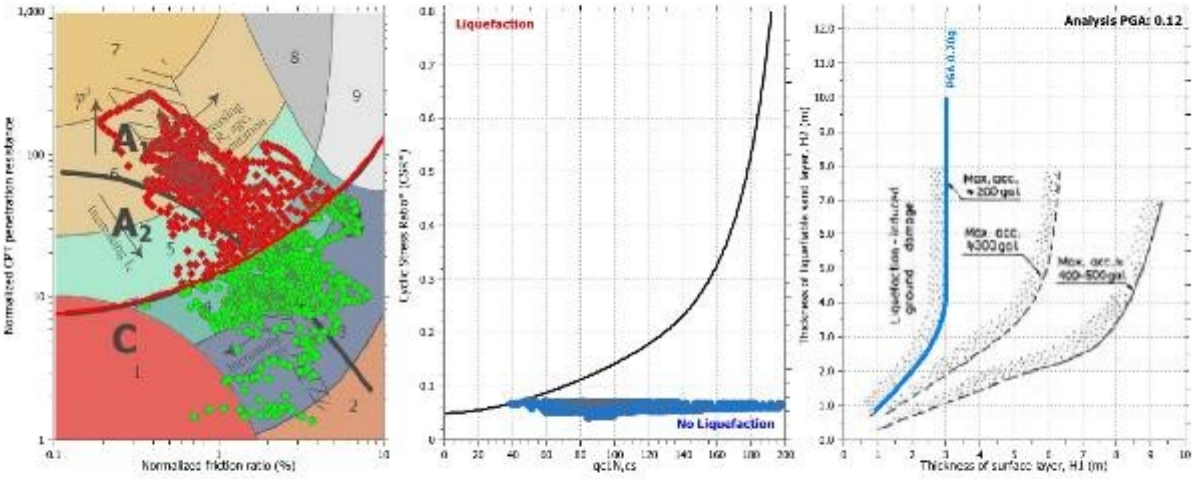
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlikely to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

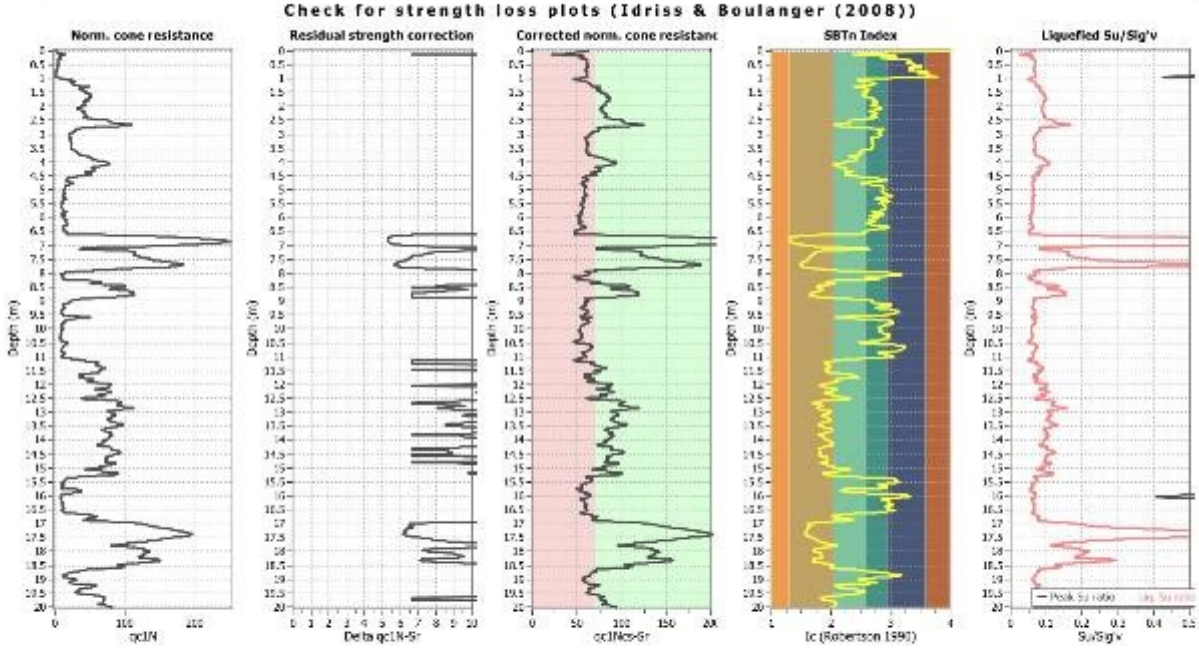
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	IS8 (2018)	Depth to GWT (erthq.):	1.40 m	Fill weight:	N/A
Flow correction method:	RAW (1998)	Average results interval:	3	Transition layers applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w:	5.45	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.12	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.40 m	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

Analysis method:	IS8 (2018)	Depth to GWT (erthq.):	1.40 m	Fill weight:	N/A
Flow correction method:	RAW (1998)	Average results interval:	3	Transition layers applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w:	5.45	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.12	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.40 m	Fill height:	N/A	Limit depth:	N/A

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
0.01	2.00	0.00	0.00	0.01	0.00	0.02	2.00	0.00	0.00	0.01	0.00
0.03	2.00	0.00	0.00	0.01	0.00	0.04	2.00	0.00	0.00	0.01	0.00
0.05	2.00	0.00	0.00	0.01	0.00	0.06	2.00	0.00	0.00	0.01	0.00
0.07	2.00	0.00	0.00	0.01	0.00	0.08	2.00	0.00	0.00	0.01	0.00
0.09	2.00	0.00	0.00	0.01	0.00	0.10	2.00	0.00	0.00	0.01	0.00
0.11	2.00	0.00	0.00	0.01	0.00	0.12	2.00	0.00	0.00	0.01	0.00
0.13	2.00	0.00	0.00	0.01	0.00	0.14	2.00	0.00	0.00	0.01	0.00
0.15	2.00	0.00	0.00	0.01	0.00	0.16	2.00	0.00	0.00	0.01	0.00
0.17	2.00	0.00	0.00	0.01	0.00	0.18	2.00	0.00	0.00	0.01	0.00
0.19	2.00	0.00	0.00	0.01	0.00	0.20	2.00	0.00	0.00	0.01	0.00
0.21	2.00	0.00	0.00	0.01	0.00	0.22	2.00	0.00	0.00	0.01	0.00
0.23	2.00	0.00	0.00	0.01	0.00	0.24	2.00	0.00	0.00	0.01	0.00
0.25	2.00	0.00	0.00	0.01	0.00	0.26	2.00	0.00	0.00	0.01	0.00
0.27	2.00	0.00	0.00	0.01	0.00	0.28	2.00	0.00	0.00	0.01	0.00
0.29	2.00	0.00	0.00	0.01	0.00	0.30	2.00	0.00	0.00	0.01	0.00
0.31	2.00	0.00	0.00	0.01	0.00	0.32	2.00	0.00	0.00	0.01	0.00
0.33	2.00	0.00	0.00	0.01	0.00	0.34	2.00	0.00	0.00	0.01	0.00
0.35	2.00	0.00	0.00	0.01	0.00	0.36	2.00	0.00	0.00	0.01	0.00
0.37	2.00	0.00	0.00	0.01	0.00	0.38	2.00	0.00	0.00	0.01	0.00
0.39	2.00	0.00	0.00	0.01	0.00	0.40	2.00	0.00	0.00	0.01	0.00
0.41	2.00	0.00	0.00	0.01	0.00	0.42	2.00	0.00	0.00	0.01	0.00
0.43	2.00	0.00	0.00	0.01	0.00	0.44	2.00	0.00	0.00	0.01	0.00
0.45	2.00	0.00	0.00	0.01	0.00	0.46	2.00	0.00	0.00	0.01	0.00
0.47	2.00	0.00	0.00	0.01	0.00	0.48	2.00	0.00	0.00	0.01	0.00
0.49	2.00	0.00	0.00	0.01	0.00	0.50	2.00	0.00	0.00	0.01	0.00
0.51	2.00	0.00	0.00	0.01	0.00	0.52	2.00	0.00	0.00	0.01	0.00
0.53	2.00	0.00	0.00	0.01	0.00	0.54	2.00	0.00	0.00	0.01	0.00
0.55	2.00	0.00	0.00	0.01	0.00	0.56	2.00	0.00	0.00	0.01	0.00
0.57	2.00	0.00	0.00	0.01	0.00	0.58	2.00	0.00	0.00	0.01	0.00
0.59	2.00	0.00	0.00	0.01	0.00	0.60	2.00	0.00	0.00	0.01	0.00
0.61	2.00	0.00	0.00	0.01	0.00	0.62	2.00	0.00	0.00	0.01	0.00
0.63	2.00	0.00	0.00	0.01	0.00	0.64	2.00	0.00	0.00	0.01	0.00
0.65	2.00	0.00	0.00	0.01	0.00	0.66	2.00	0.00	0.00	0.01	0.00
0.67	2.00	0.00	0.00	0.01	0.00	0.68	2.00	0.00	0.00	0.01	0.00
0.69	2.00	0.00	0.00	0.01	0.00	0.70	2.00	0.00	0.00	0.01	0.00
0.71	2.00	0.00	0.00	0.01	0.00	0.72	2.00	0.00	0.00	0.01	0.00
0.73	2.00	0.00	0.00	0.01	0.00	0.74	2.00	0.00	0.00	0.01	0.00
0.75	2.00	0.00	0.00	0.01	0.00	0.76	2.00	0.00	0.00	0.01	0.00
0.77	2.00	0.00	0.00	0.01	0.00	0.78	2.00	0.00	0.00	0.01	0.00
0.79	2.00	0.00	0.00	0.01	0.00	0.80	2.00	0.00	0.00	0.01	0.00
0.81	2.00	0.00	0.00	0.01	0.00	0.82	2.00	0.00	0.00	0.01	0.00
0.83	2.00	0.00	0.00	0.01	0.00	0.84	2.00	0.00	0.00	0.01	0.00
0.85	2.00	0.00	0.00	0.01	0.00	0.86	2.00	0.00	0.00	0.01	0.00
0.87	2.00	0.00	0.00	0.01	0.00	0.88	2.00	0.00	0.00	0.01	0.00
0.89	2.00	0.00	0.00	0.01	0.00	0.90	2.00	0.00	0.00	0.01	0.00
0.91	2.00	0.00	0.00	0.01	0.00	0.92	2.00	0.00	0.00	0.01	0.00
0.93	2.00	0.00	0.00	0.01	0.00	0.94	2.00	0.00	0.00	0.01	0.00
0.95	2.00	0.00	0.00	0.01	0.00	0.96	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
0.97	2.00	0.00	0.00	0.01	0.00	0.98	2.00	0.00	0.00	0.01	0.00
0.99	2.00	0.00	0.00	0.01	0.00	1.00	2.00	0.00	0.00	0.01	0.00
1.01	2.00	0.00	0.00	0.01	0.00	1.02	2.00	0.00	0.00	0.01	0.00
1.03	2.00	0.00	0.00	0.01	0.00	1.04	2.00	0.00	0.00	0.01	0.00
1.05	2.00	0.00	0.00	0.01	0.00	1.06	2.00	0.00	0.00	0.01	0.00
1.07	2.00	0.00	0.00	0.01	0.00	1.08	2.00	0.00	0.00	0.01	0.00
1.09	2.00	0.00	0.00	0.01	0.00	1.10	2.00	0.00	0.00	0.01	0.00
1.11	2.00	0.00	0.00	0.01	0.00	1.12	2.00	0.00	0.00	0.01	0.00
1.13	2.00	0.00	0.00	0.01	0.00	1.14	2.00	0.00	0.00	0.01	0.00
1.15	2.00	0.00	0.00	0.01	0.00	1.16	2.00	0.00	0.00	0.01	0.00
1.17	2.00	0.00	0.00	0.01	0.00	1.18	2.00	0.00	0.00	0.01	0.00
1.19	2.00	0.00	0.00	0.01	0.00	1.20	2.00	0.00	0.00	0.01	0.00
1.21	2.00	0.00	0.00	0.01	0.00	1.22	2.00	0.00	0.00	0.01	0.00
1.23	2.00	0.00	0.00	0.01	0.00	1.24	2.00	0.00	0.00	0.01	0.00
1.25	2.00	0.00	0.00	0.01	0.00	1.26	2.00	0.00	0.00	0.01	0.00
1.27	2.00	0.00	0.00	0.01	0.00	1.28	2.00	0.00	0.00	0.01	0.00
1.29	2.00	0.00	0.00	0.01	0.00	1.30	2.00	0.00	0.00	0.01	0.00
1.31	2.00	0.00	0.00	0.01	0.00	1.32	2.00	0.00	0.00	0.01	0.00
1.33	2.00	0.00	0.00	0.01	0.00	1.34	2.00	0.00	0.00	0.01	0.00
1.35	2.00	0.00	0.00	0.01	0.00	1.36	2.00	0.00	0.00	0.01	0.00
1.37	2.00	0.00	0.00	0.01	0.00	1.38	2.00	0.00	0.00	0.01	0.00
1.39	2.00	0.00	0.00	0.01	0.00	1.40	2.00	0.00	0.00	0.01	0.00
1.41	2.00	0.00	0.00	0.01	0.00	1.42	2.00	0.00	0.00	0.01	0.00
1.43	2.00	0.00	0.00	0.01	0.00	1.44	2.00	0.00	0.00	0.01	0.00
1.45	2.00	0.00	0.00	0.01	0.00	1.46	2.00	0.00	0.00	0.01	0.00
1.47	2.00	0.00	0.00	0.01	0.00	1.48	2.00	0.00	0.00	0.01	0.00
1.49	2.00	0.00	0.00	0.01	0.00	1.50	2.00	0.00	0.00	0.01	0.00
1.51	2.00	0.00	0.00	0.01	0.00	1.52	2.00	0.00	0.00	0.01	0.00
1.53	2.00	0.00	0.00	0.01	0.00	1.54	2.00	0.00	0.00	0.01	0.00
1.55	2.00	0.00	0.00	0.01	0.00	1.56	2.00	0.00	0.00	0.01	0.00
1.57	2.00	0.00	0.00	0.01	0.00	1.58	2.00	0.00	0.00	0.01	0.00
1.59	2.00	0.00	0.00	0.01	0.00	1.60	2.00	0.00	0.00	0.01	0.00
1.61	2.00	0.00	0.00	0.01	0.00	1.62	2.00	0.00	0.00	0.01	0.00
1.63	2.00	0.00	0.00	0.01	0.00	1.64	2.00	0.00	0.00	0.01	0.00
1.65	2.00	0.00	0.00	0.01	0.00	1.66	2.00	0.00	0.00	0.01	0.00
1.67	2.00	0.00	0.00	0.01	0.00	1.68	2.00	0.00	0.00	0.01	0.00
1.69	2.00	0.00	0.00	0.01	0.00	1.70	2.00	0.00	0.00	0.01	0.00
1.71	2.00	0.00	0.00	0.01	0.00	1.72	2.00	0.00	0.00	0.01	0.00
1.73	2.00	0.00	0.00	0.01	0.00	1.74	2.00	0.00	0.00	0.01	0.00
1.75	2.00	0.00	0.00	0.01	0.00	1.76	2.00	0.00	0.00	0.01	0.00
1.77	2.00	0.00	0.00	0.01	0.00	1.78	2.00	0.00	0.00	0.01	0.00
1.79	2.00	0.00	0.00	0.01	0.00	1.80	2.00	0.00	0.00	0.01	0.00
1.81	2.00	0.00	0.00	0.01	0.00	1.82	2.00	0.00	0.00	0.01	0.00
1.83	2.00	0.00	0.00	0.01	0.00	1.84	2.00	0.00	0.00	0.01	0.00
1.85	2.00	0.00	0.00	0.01	0.00	1.86	2.00	0.00	0.00	0.01	0.00
1.87	2.00	0.00	0.00	0.01	0.00	1.88	2.00	0.00	0.00	0.01	0.00
1.89	2.00	0.00	0.00	0.01	0.00	1.90	2.00	0.00	0.00	0.01	0.00
1.91	2.00	0.00	0.00	0.01	0.00	1.92	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
1.93	2.00	0.00	0.00	0.01	0.00	1.94	2.00	0.00	0.00	0.01	0.00
1.95	2.00	0.00	0.00	0.01	0.00	1.96	2.00	0.00	0.00	0.01	0.00
1.97	2.00	0.00	0.00	0.01	0.00	1.98	2.00	0.00	0.00	0.01	0.00
1.99	2.00	0.00	0.00	0.01	0.00	2.00	2.00	0.00	0.00	0.01	0.00
2.01	2.00	0.00	0.00	0.01	0.00	2.02	2.00	0.00	0.00	0.01	0.00
2.03	2.00	0.00	0.00	0.01	0.00	2.04	2.00	0.00	0.00	0.01	0.00
2.05	2.00	0.00	0.00	0.01	0.00	2.06	2.00	0.00	0.00	0.01	0.00
2.07	2.00	0.00	0.00	0.01	0.00	2.08	2.00	0.00	0.00	0.01	0.00
2.09	2.00	0.00	0.00	0.01	0.00	2.10	2.00	0.00	0.00	0.01	0.00
2.11	2.00	0.00	0.00	0.01	0.00	2.12	2.00	0.00	0.00	0.01	0.00
2.13	2.00	0.00	0.00	0.01	0.00	2.14	2.00	0.00	0.00	0.01	0.00
2.15	2.00	0.00	0.00	0.01	0.00	2.16	2.00	0.00	0.00	0.01	0.00
2.17	2.00	0.00	0.00	0.01	0.00	2.18	2.00	0.00	0.00	0.01	0.00
2.19	2.00	0.00	0.00	0.01	0.00	2.20	2.00	0.00	0.00	0.01	0.00
2.21	2.00	0.00	0.00	0.01	0.00	2.22	2.00	0.00	0.00	0.01	0.00
2.23	2.00	0.00	0.00	0.01	0.00	2.24	2.00	0.00	0.00	0.01	0.00
2.25	2.00	0.00	0.00	0.01	0.00	2.26	2.00	0.00	0.00	0.01	0.00
2.27	2.00	0.00	0.00	0.01	0.00	2.28	2.00	0.00	0.00	0.01	0.00
2.29	2.00	0.00	0.00	0.01	0.00	2.30	2.00	0.00	0.00	0.01	0.00
2.31	2.00	0.00	0.00	0.01	0.00	2.32	2.00	0.00	0.00	0.01	0.00
2.33	2.00	0.00	0.00	0.01	0.00	2.34	2.00	0.00	0.00	0.01	0.00
2.35	2.00	0.00	0.00	0.01	0.00	2.36	2.00	0.00	0.00	0.01	0.00
2.37	2.00	0.00	0.00	0.01	0.00	2.38	2.00	0.00	0.00	0.01	0.00
2.39	2.00	0.00	0.00	0.01	0.00	2.40	2.00	0.00	0.00	0.01	0.00
2.41	2.00	0.00	0.00	0.01	0.00	2.42	2.00	0.00	0.00	0.01	0.00
2.43	2.00	0.00	0.00	0.01	0.00	2.44	2.00	0.00	0.00	0.01	0.00
2.45	2.00	0.00	0.00	0.01	0.00	2.46	2.00	0.00	0.00	0.01	0.00
2.47	2.00	0.00	0.00	0.01	0.00	2.48	2.00	0.00	0.00	0.01	0.00
2.49	2.00	0.00	0.00	0.01	0.00	2.50	2.00	0.00	0.00	0.01	0.00
2.51	2.00	0.00	0.00	0.01	0.00	2.52	2.00	0.00	0.00	0.01	0.00
2.53	2.00	0.00	0.00	0.01	0.00	2.54	2.00	0.00	0.00	0.01	0.00
2.55	2.00	0.00	0.00	0.01	0.00	2.56	2.00	0.00	0.00	0.01	0.00
2.57	2.00	0.00	0.00	0.01	0.00	2.58	2.00	0.00	0.00	0.01	0.00
2.59	2.00	0.00	0.00	0.01	0.00	2.60	2.00	0.00	0.00	0.01	0.00
2.61	2.00	0.00	0.00	0.01	0.00	2.62	2.00	0.00	0.00	0.01	0.00
2.63	2.00	0.00	0.00	0.01	0.00	2.64	2.00	0.00	0.00	0.01	0.00
2.65	2.00	0.00	0.00	0.01	0.00	2.66	2.00	0.00	0.00	0.01	0.00
2.67	2.00	0.00	0.00	0.01	0.00	2.68	2.00	0.00	0.00	0.01	0.00
2.69	2.00	0.00	0.00	0.01	0.00	2.70	2.00	0.00	0.00	0.01	0.00
2.71	2.00	0.00	0.00	0.01	0.00	2.72	2.00	0.00	0.00	0.01	0.00
2.73	2.00	0.00	0.00	0.01	0.00	2.74	2.00	0.00	0.00	0.01	0.00
2.75	2.00	0.00	0.00	0.01	0.00	2.76	2.00	0.00	0.00	0.01	0.00
2.77	2.00	0.00	0.00	0.01	0.00	2.78	2.00	0.00	0.00	0.01	0.00
2.79	2.00	0.00	0.00	0.01	0.00	2.80	2.00	0.00	0.00	0.01	0.00
2.81	2.00	0.00	0.00	0.01	0.00	2.82	2.00	0.00	0.00	0.01	0.00
2.83	2.00	0.00	0.00	0.01	0.00	2.84	2.00	0.00	0.00	0.01	0.00
2.85	2.00	0.00	0.00	0.01	0.00	2.86	2.00	0.00	0.00	0.01	0.00
2.87	2.00	0.00	0.00	0.01	0.00	2.88	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
2.89	2.00	0.00	0.00	0.01	0.00	2.90	2.00	0.00	0.00	0.01	0.00
2.91	2.00	0.00	0.00	0.01	0.00	2.92	2.00	0.00	0.00	0.01	0.00
2.93	2.00	0.00	0.00	0.01	0.00	2.94	2.00	0.00	0.00	0.01	0.00
2.95	2.00	0.00	0.00	0.01	0.00	2.96	2.00	0.00	0.00	0.01	0.00
2.97	2.00	0.00	0.00	0.01	0.00	2.98	2.00	0.00	0.00	0.01	0.00
2.99	2.00	0.00	0.00	0.01	0.00	3.00	2.00	0.00	0.00	0.01	0.00
3.01	2.00	0.00	0.00	0.01	0.00	3.02	2.00	0.00	0.00	0.01	0.00
3.03	2.00	0.00	0.00	0.01	0.00	3.04	2.00	0.00	0.00	0.01	0.00
3.05	2.00	0.00	0.00	0.01	0.00	3.06	2.00	0.00	0.00	0.01	0.00
3.07	2.00	0.00	0.00	0.01	0.00	3.08	2.00	0.00	0.00	0.01	0.00
3.09	2.00	0.00	0.00	0.01	0.00	3.10	2.00	0.00	0.00	0.01	0.00
3.11	2.00	0.00	0.00	0.01	0.00	3.12	2.00	0.00	0.00	0.01	0.00
3.13	2.00	0.00	0.00	0.01	0.00	3.14	2.00	0.00	0.00	0.01	0.00
3.15	2.00	0.00	0.00	0.01	0.00	3.16	2.00	0.00	0.00	0.01	0.00
3.17	2.00	0.00	0.00	0.01	0.00	3.18	2.00	0.00	0.00	0.01	0.00
3.19	2.00	0.00	0.00	0.01	0.00	3.20	2.00	0.00	0.00	0.01	0.00
3.21	2.00	0.00	0.00	0.01	0.00	3.22	2.00	0.00	0.00	0.01	0.00
3.23	2.00	0.00	0.00	0.01	0.00	3.24	2.00	0.00	0.00	0.01	0.00
3.25	2.00	0.00	0.00	0.01	0.00	3.26	2.00	0.00	0.00	0.01	0.00
3.27	2.00	0.00	0.00	0.01	0.00	3.28	2.00	0.00	0.00	0.01	0.00
3.29	2.00	0.00	0.00	0.01	0.00	3.30	2.00	0.00	0.00	0.01	0.00
3.31	2.00	0.00	0.00	0.01	0.00	3.32	2.00	0.00	0.00	0.01	0.00
3.33	2.00	0.00	0.00	0.01	0.00	3.34	2.00	0.00	0.00	0.01	0.00
3.35	2.00	0.00	0.00	0.01	0.00	3.36	2.00	0.00	0.00	0.01	0.00
3.37	2.00	0.00	0.00	0.01	0.00	3.38	2.00	0.00	0.00	0.01	0.00
3.39	2.00	0.00	0.00	0.01	0.00	3.40	2.00	0.00	0.00	0.01	0.00
3.41	2.00	0.00	0.00	0.01	0.00	3.42	2.00	0.00	0.00	0.01	0.00
3.43	2.00	0.00	0.00	0.01	0.00	3.44	2.00	0.00	0.00	0.01	0.00
3.45	2.00	0.00	0.00	0.01	0.00	3.46	2.00	0.00	0.00	0.01	0.00
3.47	2.00	0.00	0.00	0.01	0.00	3.48	2.00	0.00	0.00	0.01	0.00
3.49	2.00	0.00	0.00	0.01	0.00	3.50	2.00	0.00	0.00	0.01	0.00
3.51	2.00	0.00	0.00	0.01	0.00	3.52	2.00	0.00	0.00	0.01	0.00
3.53	2.00	0.00	0.00	0.01	0.00	3.54	2.00	0.00	0.00	0.01	0.00
3.55	2.00	0.00	0.00	0.01	0.00	3.56	2.00	0.00	0.00	0.01	0.00
3.57	1.50	0.00	0.00	0.01	0.00	3.58	1.53	0.00	0.00	0.01	0.00
3.59	1.54	0.00	0.00	0.01	0.00	3.60	1.56	0.00	0.00	0.01	0.00
3.61	1.58	0.00	0.00	0.01	0.00	3.62	1.59	0.00	0.00	0.01	0.00
3.63	1.63	0.00	0.00	0.01	0.00	3.64	1.63	0.00	0.00	0.01	0.00
3.65	1.63	0.00	0.00	0.01	0.00	3.66	1.62	0.00	0.00	0.01	0.00
3.67	1.63	0.00	0.00	0.01	0.00	3.68	1.64	0.00	0.00	0.01	0.00
3.69	1.65	0.00	0.00	0.01	0.00	3.70	1.67	0.00	0.00	0.01	0.00
3.71	1.68	0.00	0.00	0.01	0.00	3.72	1.68	0.00	0.00	0.01	0.00
3.73	1.68	0.00	0.00	0.01	0.00	3.74	1.70	0.00	0.00	0.01	0.00
3.75	1.72	0.00	0.00	0.01	0.00	3.76	1.75	0.00	0.00	0.01	0.00
3.77	1.75	0.00	0.00	0.01	0.00	3.78	1.72	0.00	0.00	0.01	0.00
3.79	1.99	0.00	0.00	0.01	0.00	3.80	2.00	0.00	0.00	0.01	0.00
3.81	2.00	0.00	0.00	0.01	0.00	3.82	2.00	0.00	0.00	0.01	0.00
3.83	2.00	0.00	0.00	0.01	0.00	3.84	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
3.85	2.00	0.00	0.00	0.01	0.00	3.86	2.00	0.00	0.00	0.01	0.00
3.87	2.00	0.00	0.00	0.01	0.00	3.88	2.00	0.00	0.00	0.01	0.00
3.89	2.00	0.00	0.00	0.01	0.00	3.90	2.00	0.00	0.00	0.01	0.00
3.91	2.00	0.00	0.00	0.01	0.00	3.92	2.00	0.00	0.00	0.01	0.00
3.93	2.00	0.00	0.00	0.01	0.00	3.94	2.00	0.00	0.00	0.01	0.00
3.95	2.00	0.00	0.00	0.01	0.00	3.96	2.00	0.00	0.00	0.01	0.00
3.97	2.00	0.00	0.00	0.01	0.00	3.98	2.00	0.00	0.00	0.01	0.00
3.99	2.00	0.00	0.00	0.01	0.00	4.00	2.00	0.00	0.00	0.01	0.00
4.01	2.00	0.00	0.00	0.01	0.00	4.02	2.00	0.00	0.00	0.01	0.00
4.03	2.00	0.00	0.00	0.01	0.00	4.04	2.00	0.00	0.00	0.01	0.00
4.05	2.00	0.00	0.00	0.01	0.00	4.06	2.00	0.00	0.00	0.01	0.00
4.07	2.00	0.00	0.00	0.01	0.00	4.08	2.00	0.00	0.00	0.01	0.00
4.09	2.00	0.00	0.00	0.01	0.00	4.10	2.00	0.00	0.00	0.01	0.00
4.11	2.00	0.00	0.00	0.01	0.00	4.12	2.00	0.00	0.00	0.01	0.00
4.13	2.00	0.00	0.00	0.01	0.00	4.14	2.00	0.00	0.00	0.01	0.00
4.15	2.00	0.00	0.00	0.01	0.00	4.16	2.00	0.00	0.00	0.01	0.00
4.17	2.00	0.00	0.00	0.01	0.00	4.18	2.00	0.00	0.00	0.01	0.00
4.19	1.99	0.00	0.00	0.01	0.00	4.20	1.97	0.00	0.00	0.01	0.00
4.21	1.96	0.00	0.00	0.01	0.00	4.22	1.98	0.00	0.00	0.01	0.00
4.23	2.00	0.00	0.00	0.01	0.00	4.24	2.00	0.00	0.00	0.01	0.00
4.25	2.00	0.00	0.00	0.01	0.00	4.26	2.00	0.00	0.00	0.01	0.00
4.27	2.00	0.00	0.00	0.01	0.00	4.28	2.00	0.00	0.00	0.01	0.00
4.29	2.00	0.00	0.00	0.01	0.00	4.30	2.00	0.00	0.00	0.01	0.00
4.31	2.00	0.00	0.00	0.01	0.00	4.32	2.00	0.00	0.00	0.01	0.00
4.33	1.99	0.00	0.00	0.01	0.00	4.34	1.95	0.00	0.00	0.01	0.00
4.35	1.85	0.00	0.00	0.01	0.00	4.36	1.82	0.00	0.00	0.01	0.00
4.37	1.80	0.00	0.00	0.01	0.00	4.38	1.80	0.00	0.00	0.01	0.00
4.39	1.81	0.00	0.00	0.01	0.00	4.40	1.92	0.00	0.00	0.01	0.00
4.41	1.95	0.00	0.00	0.01	0.00	4.42	1.97	0.00	0.00	0.01	0.00
4.43	1.97	0.00	0.00	0.01	0.00	4.44	1.99	0.00	0.00	0.01	0.00
4.45	1.99	0.00	0.00	0.01	0.00	4.46	1.98	0.00	0.00	0.01	0.00
4.47	1.89	0.00	0.00	0.01	0.00	4.48	1.83	0.00	0.00	0.01	0.00
4.49	1.79	0.00	0.00	0.01	0.00	4.50	1.68	0.00	0.00	0.01	0.00
4.51	1.64	0.00	0.00	0.01	0.00	4.52	1.55	0.00	0.00	0.01	0.00
4.53	1.51	0.00	0.00	0.01	0.00	4.54	1.44	0.00	0.00	0.01	0.00
4.55	1.38	0.00	0.00	0.01	0.00	4.56	1.35	0.00	0.00	0.01	0.00
4.57	2.00	0.00	0.00	0.01	0.00	4.58	2.00	0.00	0.00	0.01	0.00
4.59	2.00	0.00	0.00	0.01	0.00	4.60	2.00	0.00	0.00	0.01	0.00
4.61	2.00	0.00	0.00	0.01	0.00	4.62	2.00	0.00	0.00	0.01	0.00
4.63	2.00	0.00	0.00	0.01	0.00	4.64	2.00	0.00	0.00	0.01	0.00
4.65	2.00	0.00	0.00	0.01	0.00	4.66	2.00	0.00	0.00	0.01	0.00
4.67	2.00	0.00	0.00	0.01	0.00	4.68	2.00	0.00	0.00	0.01	0.00
4.69	2.00	0.00	0.00	0.01	0.00	4.70	2.00	0.00	0.00	0.01	0.00
4.71	2.00	0.00	0.00	0.01	0.00	4.72	2.00	0.00	0.00	0.01	0.00
4.73	1.29	0.00	0.00	0.01	0.00	4.74	1.31	0.00	0.00	0.01	0.00
4.75	1.39	0.00	0.00	0.01	0.00	4.76	1.38	0.00	0.00	0.01	0.00
4.77	1.38	0.00	0.00	0.01	0.00	4.78	1.38	0.00	0.00	0.01	0.00
4.79	1.34	0.00	0.00	0.01	0.00	4.80	1.32	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
4.81	2.00	0.00	0.00	0.01	0.00	4.82	2.00	0.00	0.00	0.01	0.00
4.83	2.00	0.00	0.00	0.01	0.00	4.84	2.00	0.00	0.00	0.01	0.00
4.85	2.00	0.00	0.00	0.01	0.00	4.86	2.00	0.00	0.00	0.01	0.00
4.87	2.00	0.00	0.00	0.01	0.00	4.88	2.00	0.00	0.00	0.01	0.00
4.89	2.00	0.00	0.00	0.01	0.00	4.90	2.00	0.00	0.00	0.01	0.00
4.91	2.00	0.00	0.00	0.01	0.00	4.92	2.00	0.00	0.00	0.01	0.00
4.93	2.00	0.00	0.00	0.01	0.00	4.94	2.00	0.00	0.00	0.01	0.00
4.95	2.00	0.00	0.00	0.01	0.00	4.96	2.00	0.00	0.00	0.01	0.00
4.97	2.00	0.00	0.00	0.01	0.00	4.98	2.00	0.00	0.00	0.01	0.00
4.99	2.00	0.00	0.00	0.01	0.00	5.00	2.00	0.00	0.00	0.01	0.00
5.01	2.00	0.00	0.00	0.01	0.00	5.02	2.00	0.00	0.00	0.01	0.00
5.03	2.00	0.00	0.00	0.01	0.00	5.04	2.00	0.00	0.00	0.01	0.00
5.05	2.00	0.00	0.00	0.01	0.00	5.06	2.00	0.00	0.00	0.01	0.00
5.07	2.00	0.00	0.00	0.01	0.00	5.08	2.00	0.00	0.00	0.01	0.00
5.09	2.00	0.00	0.00	0.01	0.00	5.10	2.00	0.00	0.00	0.01	0.00
5.11	2.00	0.00	0.00	0.01	0.00	5.12	2.00	0.00	0.00	0.01	0.00
5.13	2.00	0.00	0.00	0.01	0.00	5.14	2.00	0.00	0.00	0.01	0.00
5.15	2.00	0.00	0.00	0.01	0.00	5.16	2.00	0.00	0.00	0.01	0.00
5.17	2.00	0.00	0.00	0.01	0.00	5.18	2.00	0.00	0.00	0.01	0.00
5.19	2.00	0.00	0.00	0.01	0.00	5.20	2.00	0.00	0.00	0.01	0.00
5.21	2.00	0.00	0.00	0.01	0.00	5.22	2.00	0.00	0.00	0.01	0.00
5.23	2.00	0.00	0.00	0.01	0.00	5.24	2.00	0.00	0.00	0.01	0.00
5.25	2.00	0.00	0.00	0.01	0.00	5.26	2.00	0.00	0.00	0.01	0.00
5.27	2.00	0.00	0.00	0.01	0.00	5.28	2.00	0.00	0.00	0.01	0.00
5.29	2.00	0.00	0.00	0.01	0.00	5.30	2.00	0.00	0.00	0.01	0.00
5.31	2.00	0.00	0.00	0.01	0.00	5.32	2.00	0.00	0.00	0.01	0.00
5.33	2.00	0.00	0.00	0.01	0.00	5.34	2.00	0.00	0.00	0.01	0.00
5.35	2.00	0.00	0.00	0.01	0.00	5.36	2.00	0.00	0.00	0.01	0.00
5.37	2.00	0.00	0.00	0.01	0.00	5.38	2.00	0.00	0.00	0.01	0.00
5.39	2.00	0.00	0.00	0.01	0.00	5.40	2.00	0.00	0.00	0.01	0.00
5.41	2.00	0.00	0.00	0.01	0.00	5.42	2.00	0.00	0.00	0.01	0.00
5.43	2.00	0.00	0.00	0.01	0.00	5.44	2.00	0.00	0.00	0.01	0.00
5.45	2.00	0.00	0.00	0.01	0.00	5.46	2.00	0.00	0.00	0.01	0.00
5.47	2.00	0.00	0.00	0.01	0.00	5.48	2.00	0.00	0.00	0.01	0.00
5.49	2.00	0.00	0.00	0.01	0.00	5.50	2.00	0.00	0.00	0.01	0.00
5.51	2.00	0.00	0.00	0.01	0.00	5.52	2.00	0.00	0.00	0.01	0.00
5.53	2.00	0.00	0.00	0.01	0.00	5.54	2.00	0.00	0.00	0.01	0.00
5.55	2.00	0.00	0.00	0.01	0.00	5.56	2.00	0.00	0.00	0.01	0.00
5.57	2.00	0.00	0.00	0.01	0.00	5.58	2.00	0.00	0.00	0.01	0.00
5.59	2.00	0.00	0.00	0.01	0.00	5.60	2.00	0.00	0.00	0.01	0.00
5.61	2.00	0.00	0.00	0.01	0.00	5.62	2.00	0.00	0.00	0.01	0.00
5.63	2.00	0.00	0.00	0.01	0.00	5.64	2.00	0.00	0.00	0.01	0.00
5.65	2.00	0.00	0.00	0.01	0.00	5.66	2.00	0.00	0.00	0.01	0.00
5.67	2.00	0.00	0.00	0.01	0.00	5.68	2.00	0.00	0.00	0.01	0.00
5.69	2.00	0.00	0.00	0.01	0.00	5.70	2.00	0.00	0.00	0.01	0.00
5.71	2.00	0.00	0.00	0.01	0.00	5.72	2.00	0.00	0.00	0.01	0.00
5.73	2.00	0.00	0.00	0.01	0.00	5.74	2.00	0.00	0.00	0.01	0.00
5.75	2.00	0.00	0.00	0.01	0.00	5.76	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
5.77	2.00	0.00	0.00	0.01	0.00	5.78	2.00	0.00	0.00	0.01	0.00
5.79	2.00	0.00	0.00	0.01	0.00	5.80	2.00	0.00	0.00	0.01	0.00
5.81	2.00	0.00	0.00	0.01	0.00	5.82	2.00	0.00	0.00	0.01	0.00
5.83	2.00	0.00	0.00	0.01	0.00	5.84	2.00	0.00	0.00	0.01	0.00
5.85	2.00	0.00	0.00	0.01	0.00	5.86	2.00	0.00	0.00	0.01	0.00
5.87	2.00	0.00	0.00	0.01	0.00	5.88	2.00	0.00	0.00	0.01	0.00
5.89	2.00	0.00	0.00	0.01	0.00	5.90	2.00	0.00	0.00	0.01	0.00
5.91	2.00	0.00	0.00	0.01	0.00	5.92	2.00	0.00	0.00	0.01	0.00
5.93	2.00	0.00	0.00	0.01	0.00	5.94	2.00	0.00	0.00	0.01	0.00
5.95	2.00	0.00	0.00	0.01	0.00	5.96	2.00	0.00	0.00	0.01	0.00
5.97	2.00	0.00	0.00	0.01	0.00	5.98	2.00	0.00	0.00	0.01	0.00
5.99	2.00	0.00	0.00	0.01	0.00	6.00	2.00	0.00	0.00	0.01	0.00
6.01	2.00	0.00	0.00	0.01	0.00	6.02	2.00	0.00	0.00	0.01	0.00
6.03	2.00	0.00	0.00	0.01	0.00	6.04	2.00	0.00	0.00	0.01	0.00
6.05	2.00	0.00	0.00	0.01	0.00	6.06	2.00	0.00	0.00	0.01	0.00
6.07	2.00	0.00	0.00	0.01	0.00	6.08	2.00	0.00	0.00	0.01	0.00
6.09	2.00	0.00	0.00	0.01	0.00	6.10	2.00	0.00	0.00	0.01	0.00
6.11	2.00	0.00	0.00	0.01	0.00	6.12	2.00	0.00	0.00	0.01	0.00
6.13	2.00	0.00	0.00	0.01	0.00	6.14	2.00	0.00	0.00	0.01	0.00
6.15	2.00	0.00	0.00	0.01	0.00	6.16	2.00	0.00	0.00	0.01	0.00
6.17	2.00	0.00	0.00	0.01	0.00	6.18	2.00	0.00	0.00	0.01	0.00
6.19	2.00	0.00	0.00	0.01	0.00	6.20	2.00	0.00	0.00	0.01	0.00
6.21	1.16	0.00	0.00	0.01	0.00	6.22	1.17	0.00	0.00	0.01	0.00
6.23	2.00	0.00	0.00	0.01	0.00	6.24	2.00	0.00	0.00	0.01	0.00
6.25	2.00	0.00	0.00	0.01	0.00	6.26	2.00	0.00	0.00	0.01	0.00
6.27	2.00	0.00	0.00	0.01	0.00	6.28	2.00	0.00	0.00	0.01	0.00
6.29	2.00	0.00	0.00	0.01	0.00	6.30	2.00	0.00	0.00	0.01	0.00
6.31	2.00	0.00	0.00	0.01	0.00	6.32	2.00	0.00	0.00	0.01	0.00
6.33	2.00	0.00	0.00	0.01	0.00	6.34	2.00	0.00	0.00	0.01	0.00
6.35	2.00	0.00	0.00	0.01	0.00	6.36	2.00	0.00	0.00	0.01	0.00
6.37	2.00	0.00	0.00	0.01	0.00	6.38	2.00	0.00	0.00	0.01	0.00
6.39	2.00	0.00	0.00	0.01	0.00	6.40	2.00	0.00	0.00	0.01	0.00
6.41	2.00	0.00	0.00	0.01	0.00	6.42	2.00	0.00	0.00	0.01	0.00
6.43	2.00	0.00	0.00	0.01	0.00	6.44	2.00	0.00	0.00	0.01	0.00
6.45	2.00	0.00	0.00	0.01	0.00	6.46	2.00	0.00	0.00	0.01	0.00
6.47	2.00	0.00	0.00	0.01	0.00	6.48	1.08	0.00	0.00	0.01	0.00
6.49	1.09	0.00	0.00	0.01	0.00	6.50	1.08	0.00	0.00	0.01	0.00
6.51	1.09	0.00	0.00	0.01	0.00	6.52	1.09	0.00	0.00	0.01	0.00
6.53	1.11	0.00	0.00	0.01	0.00	6.54	1.11	0.00	0.00	0.01	0.00
6.55	1.12	0.00	0.00	0.01	0.00	6.56	1.13	0.00	0.00	0.01	0.00
6.57	1.14	0.00	0.00	0.01	0.00	6.58	1.15	0.00	0.00	0.01	0.00
6.59	1.14	0.00	0.00	0.01	0.00	6.60	1.26	0.00	0.00	0.01	0.00
6.61	1.25	0.00	0.00	0.01	0.00	6.62	1.34	0.00	0.00	0.01	0.00
6.63	1.64	0.00	0.00	0.01	0.00	6.64	2.00	0.00	0.00	0.01	0.00
6.65	2.00	0.00	0.00	0.01	0.00	6.66	2.00	0.00	0.00	0.01	0.00
6.67	2.00	0.00	0.00	0.01	0.00	6.68	2.00	0.00	0.00	0.01	0.00
6.69	2.00	0.00	0.00	0.01	0.00	6.70	2.00	0.00	0.00	0.01	0.00
6.71	2.00	0.00	0.00	0.01	0.00	6.72	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
6.73	2.00	0.00	0.00	0.01	0.00	6.74	2.00	0.00	0.00	0.01	0.00
6.75	2.00	0.00	0.00	0.01	0.00	6.76	2.00	0.00	0.00	0.01	0.00
6.77	2.00	0.00	0.00	0.01	0.00	6.78	2.00	0.00	0.00	0.01	0.00
6.79	2.00	0.00	0.00	0.01	0.00	6.80	2.00	0.00	0.00	0.01	0.00
6.81	2.00	0.00	0.00	0.01	0.00	6.82	2.00	0.00	0.00	0.01	0.00
6.83	2.00	0.00	0.00	0.01	0.00	6.84	2.00	0.00	0.00	0.01	0.00
6.85	2.00	0.00	0.00	0.01	0.00	6.86	2.00	0.00	0.00	0.01	0.00
6.87	2.00	0.00	0.00	0.01	0.00	6.88	2.00	0.00	0.00	0.01	0.00
6.89	2.00	0.00	0.00	0.01	0.00	6.90	2.00	0.00	0.00	0.01	0.00
6.91	2.00	0.00	0.00	0.01	0.00	6.92	2.00	0.00	0.00	0.01	0.00
6.93	2.00	0.00	0.00	0.01	0.00	6.94	2.00	0.00	0.00	0.01	0.00
6.95	2.00	0.00	0.00	0.01	0.00	6.96	2.00	0.00	0.00	0.01	0.00
6.97	2.00	0.00	0.00	0.01	0.00	6.98	2.00	0.00	0.00	0.01	0.00
6.99	2.00	0.00	0.00	0.01	0.00	7.00	2.00	0.00	0.00	0.01	0.00
7.01	2.00	0.00	0.00	0.01	0.00	7.02	2.00	0.00	0.00	0.01	0.00
7.03	2.00	0.00	0.00	0.01	0.00	7.04	2.00	0.00	0.00	0.01	0.00
7.05	2.00	0.00	0.00	0.01	0.00	7.06	2.00	0.00	0.00	0.01	0.00
7.07	2.00	0.00	0.00	0.01	0.00	7.08	2.00	0.00	0.00	0.01	0.00
7.09	1.75	0.00	0.00	0.01	0.00	7.10	1.71	0.00	0.00	0.01	0.00
7.11	1.66	0.00	0.00	0.01	0.00	7.12	2.00	0.00	0.00	0.01	0.00
7.13	2.00	0.00	0.00	0.01	0.00	7.14	2.00	0.00	0.00	0.01	0.00
7.15	1.77	0.00	0.00	0.01	0.00	7.16	1.98	0.00	0.00	0.01	0.00
7.17	2.00	0.00	0.00	0.01	0.00	7.18	2.00	0.00	0.00	0.01	0.00
7.19	2.00	0.00	0.00	0.01	0.00	7.20	2.00	0.00	0.00	0.01	0.00
7.21	2.00	0.00	0.00	0.01	0.00	7.22	2.00	0.00	0.00	0.01	0.00
7.23	2.00	0.00	0.00	0.01	0.00	7.24	2.00	0.00	0.00	0.01	0.00
7.25	2.00	0.00	0.00	0.01	0.00	7.26	2.00	0.00	0.00	0.01	0.00
7.27	2.00	0.00	0.00	0.01	0.00	7.28	2.00	0.00	0.00	0.01	0.00
7.29	2.00	0.00	0.00	0.01	0.00	7.30	2.00	0.00	0.00	0.01	0.00
7.31	2.00	0.00	0.00	0.01	0.00	7.32	2.00	0.00	0.00	0.01	0.00
7.33	2.00	0.00	0.00	0.01	0.00	7.34	2.00	0.00	0.00	0.01	0.00
7.35	2.00	0.00	0.00	0.01	0.00	7.36	2.00	0.00	0.00	0.01	0.00
7.37	2.00	0.00	0.00	0.01	0.00	7.38	2.00	0.00	0.00	0.01	0.00
7.39	2.00	0.00	0.00	0.01	0.00	7.40	2.00	0.00	0.00	0.01	0.00
7.41	2.00	0.00	0.00	0.01	0.00	7.42	2.00	0.00	0.00	0.01	0.00
7.43	2.00	0.00	0.00	0.01	0.00	7.44	2.00	0.00	0.00	0.01	0.00
7.45	2.00	0.00	0.00	0.01	0.00	7.46	2.00	0.00	0.00	0.01	0.00
7.47	2.00	0.00	0.00	0.01	0.00	7.48	2.00	0.00	0.00	0.01	0.00
7.49	2.00	0.00	0.00	0.01	0.00	7.50	2.00	0.00	0.00	0.01	0.00
7.51	2.00	0.00	0.00	0.01	0.00	7.52	2.00	0.00	0.00	0.01	0.00
7.53	2.00	0.00	0.00	0.01	0.00	7.54	2.00	0.00	0.00	0.01	0.00
7.55	2.00	0.00	0.00	0.01	0.00	7.56	2.00	0.00	0.00	0.01	0.00
7.57	2.00	0.00	0.00	0.01	0.00	7.58	2.00	0.00	0.00	0.01	0.00
7.59	2.00	0.00	0.00	0.01	0.00	7.60	2.00	0.00	0.00	0.01	0.00
7.61	2.00	0.00	0.00	0.01	0.00	7.62	2.00	0.00	0.00	0.01	0.00
7.63	2.00	0.00	0.00	0.01	0.00	7.64	2.00	0.00	0.00	0.01	0.00
7.65	2.00	0.00	0.00	0.01	0.00	7.66	2.00	0.00	0.00	0.01	0.00
7.67	2.00	0.00	0.00	0.01	0.00	7.68	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
7.69	2.00	0.00	0.00	0.01	0.00	7.70	2.00	0.00	0.00	0.01	0.00
7.71	2.00	0.00	0.00	0.01	0.00	7.72	2.00	0.00	0.00	0.01	0.00
7.73	2.00	0.00	0.00	0.01	0.00	7.74	2.00	0.00	0.00	0.01	0.00
7.75	2.00	0.00	0.00	0.01	0.00	7.76	2.00	0.00	0.00	0.01	0.00
7.77	2.00	0.00	0.00	0.01	0.00	7.78	2.00	0.00	0.00	0.01	0.00
7.79	2.00	0.00	0.00	0.01	0.00	7.80	2.00	0.00	0.00	0.01	0.00
7.81	2.00	0.00	0.00	0.01	0.00	7.82	2.00	0.00	0.00	0.01	0.00
7.83	2.00	0.00	0.00	0.01	0.00	7.84	2.00	0.00	0.00	0.01	0.00
7.85	2.00	0.00	0.00	0.01	0.00	7.86	2.00	0.00	0.00	0.01	0.00
7.87	1.87	0.00	0.00	0.01	0.00	7.88	1.83	0.00	0.00	0.01	0.00
7.89	1.98	0.00	0.00	0.01	0.00	7.90	1.67	0.00	0.00	0.01	0.00
7.91	1.83	0.00	0.00	0.01	0.00	7.92	1.63	0.00	0.00	0.01	0.00
7.93	1.47	0.00	0.00	0.01	0.00	7.94	1.41	0.00	0.00	0.01	0.00
7.95	2.00	0.00	0.00	0.01	0.00	7.96	2.00	0.00	0.00	0.01	0.00
7.97	2.00	0.00	0.00	0.01	0.00	7.98	2.00	0.00	0.00	0.01	0.00
7.99	2.00	0.00	0.00	0.01	0.00	8.00	2.00	0.00	0.00	0.01	0.00
8.01	2.00	0.00	0.00	0.01	0.00	8.02	2.00	0.00	0.00	0.01	0.00
8.03	2.00	0.00	0.00	0.01	0.00	8.04	2.00	0.00	0.00	0.01	0.00
8.05	2.00	0.00	0.00	0.01	0.00	8.06	2.00	0.00	0.00	0.01	0.00
8.07	2.00	0.00	0.00	0.01	0.00	8.08	2.00	0.00	0.00	0.01	0.00
8.09	2.00	0.00	0.00	0.01	0.00	8.10	2.00	0.00	0.00	0.01	0.00
8.11	2.00	0.00	0.00	0.01	0.00	8.12	2.00	0.00	0.00	0.01	0.00
8.13	2.00	0.00	0.00	0.01	0.00	8.14	2.00	0.00	0.00	0.01	0.00
8.15	1.07	0.00	0.00	0.01	0.00	8.16	1.07	0.00	0.00	0.01	0.00
8.17	2.00	0.00	0.00	0.01	0.00	8.18	2.00	0.00	0.00	0.01	0.00
8.19	2.00	0.00	0.00	0.01	0.00	8.20	2.00	0.00	0.00	0.01	0.00
8.21	2.00	0.00	0.00	0.01	0.00	8.22	2.00	0.00	0.00	0.01	0.00
8.23	2.00	0.00	0.00	0.01	0.00	8.24	1.12	0.00	0.00	0.01	0.00
8.25	1.28	0.00	0.00	0.01	0.00	8.26	1.33	0.00	0.00	0.01	0.00
8.27	1.51	0.00	0.00	0.01	0.00	8.28	1.61	0.00	0.00	0.01	0.00
8.29	1.59	0.00	0.00	0.01	0.00	8.30	1.63	0.00	0.00	0.01	0.00
8.31	1.63	0.00	0.00	0.01	0.00	8.32	1.58	0.00	0.00	0.01	0.00
8.33	1.59	0.00	0.00	0.01	0.00	8.34	1.57	0.00	0.00	0.01	0.00
8.35	1.60	0.00	0.00	0.01	0.00	8.36	1.59	0.00	0.00	0.01	0.00
8.37	1.63	0.00	0.00	0.01	0.00	8.38	1.70	0.00	0.00	0.01	0.00
8.39	1.73	0.00	0.00	0.01	0.00	8.40	1.93	0.00	0.00	0.01	0.00
8.41	1.93	0.00	0.00	0.01	0.00	8.42	2.00	0.00	0.00	0.01	0.00
8.43	2.00	0.00	0.00	0.01	0.00	8.44	2.00	0.00	0.00	0.01	0.00
8.45	2.00	0.00	0.00	0.01	0.00	8.46	2.00	0.00	0.00	0.01	0.00
8.47	2.00	0.00	0.00	0.01	0.00	8.48	2.00	0.00	0.00	0.01	0.00
8.49	2.00	0.00	0.00	0.01	0.00	8.50	2.00	0.00	0.00	0.01	0.00
8.51	1.94	0.00	0.00	0.01	0.00	8.52	1.84	0.00	0.00	0.01	0.00
8.53	1.77	0.00	0.00	0.01	0.00	8.54	1.82	0.00	0.00	0.01	0.00
8.55	1.83	0.00	0.00	0.01	0.00	8.56	1.80	0.00	0.00	0.01	0.00
8.57	1.81	0.00	0.00	0.01	0.00	8.58	1.82	0.00	0.00	0.01	0.00
8.59	1.87	0.00	0.00	0.01	0.00	8.60	2.00	0.00	0.00	0.01	0.00
8.61	2.00	0.00	0.00	0.01	0.00	8.62	2.00	0.00	0.00	0.01	0.00
8.63	2.00	0.00	0.00	0.01	0.00	8.64	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
8.65	2.00	0.00	0.00	0.01	0.00	8.66	2.00	0.00	0.00	0.01	0.00
8.67	2.00	0.00	0.00	0.01	0.00	8.68	2.00	0.00	0.00	0.01	0.00
8.69	2.00	0.00	0.00	0.01	0.00	8.70	2.00	0.00	0.00	0.01	0.00
8.71	2.00	0.00	0.00	0.01	0.00	8.72	2.00	0.00	0.00	0.01	0.00
8.73	2.00	0.00	0.00	0.01	0.00	8.74	2.00	0.00	0.00	0.01	0.00
8.75	2.00	0.00	0.00	0.01	0.00	8.76	2.00	0.00	0.00	0.01	0.00
8.77	2.00	0.00	0.00	0.01	0.00	8.78	2.00	0.00	0.00	0.01	0.00
8.79	2.00	0.00	0.00	0.01	0.00	8.80	2.00	0.00	0.00	0.01	0.00
8.81	2.00	0.00	0.00	0.01	0.00	8.82	2.00	0.00	0.00	0.01	0.00
8.83	2.00	0.00	0.00	0.01	0.00	8.84	1.93	0.00	0.00	0.01	0.00
8.85	1.85	0.00	0.00	0.01	0.00	8.86	1.76	0.00	0.00	0.01	0.00
8.87	1.80	0.00	0.00	0.01	0.00	8.88	1.67	0.00	0.00	0.01	0.00
8.89	1.75	0.00	0.00	0.01	0.00	8.90	1.63	0.00	0.00	0.01	0.00
8.91	1.60	0.00	0.00	0.01	0.00	8.92	1.67	0.00	0.00	0.01	0.00
8.93	1.53	0.00	0.00	0.01	0.00	8.94	1.52	0.00	0.00	0.01	0.00
8.95	1.44	0.00	0.00	0.01	0.00	8.96	1.43	0.00	0.00	0.01	0.00
8.97	2.00	0.00	0.00	0.01	0.00	8.98	2.00	0.00	0.00	0.01	0.00
8.99	2.00	0.00	0.00	0.01	0.00	9.00	2.00	0.00	0.00	0.01	0.00
9.01	2.00	0.00	0.00	0.01	0.00	9.02	2.00	0.00	0.00	0.01	0.00
9.03	2.00	0.00	0.00	0.01	0.00	9.04	2.00	0.00	0.00	0.01	0.00
9.05	2.00	0.00	0.00	0.01	0.00	9.06	2.00	0.00	0.00	0.01	0.00
9.07	2.00	0.00	0.00	0.01	0.00	9.08	2.00	0.00	0.00	0.01	0.00
9.09	2.00	0.00	0.00	0.01	0.00	9.10	2.00	0.00	0.00	0.01	0.00
9.11	2.00	0.00	0.00	0.01	0.00	9.12	2.00	0.00	0.00	0.01	0.00
9.13	2.00	0.00	0.00	0.01	0.00	9.14	2.00	0.00	0.00	0.01	0.00
9.15	2.00	0.00	0.00	0.01	0.00	9.16	2.00	0.00	0.00	0.01	0.00
9.17	2.00	0.00	0.00	0.01	0.00	9.18	2.00	0.00	0.00	0.01	0.00
9.19	2.00	0.00	0.00	0.01	0.00	9.20	2.00	0.00	0.00	0.01	0.00
9.21	2.00	0.00	0.00	0.01	0.00	9.22	2.00	0.00	0.00	0.01	0.00
9.23	2.00	0.00	0.00	0.01	0.00	9.24	2.00	0.00	0.00	0.01	0.00
9.25	2.00	0.00	0.00	0.01	0.00	9.26	2.00	0.00	0.00	0.01	0.00
9.27	2.00	0.00	0.00	0.01	0.00	9.28	2.00	0.00	0.00	0.01	0.00
9.29	2.00	0.00	0.00	0.01	0.00	9.30	2.00	0.00	0.00	0.01	0.00
9.31	2.00	0.00	0.00	0.01	0.00	9.32	2.00	0.00	0.00	0.01	0.00
9.33	2.00	0.00	0.00	0.01	0.00	9.34	2.00	0.00	0.00	0.01	0.00
9.35	2.00	0.00	0.00	0.01	0.00	9.36	2.00	0.00	0.00	0.01	0.00
9.37	2.00	0.00	0.00	0.01	0.00	9.38	2.00	0.00	0.00	0.01	0.00
9.39	2.00	0.00	0.00	0.01	0.00	9.40	2.00	0.00	0.00	0.01	0.00
9.41	2.00	0.00	0.00	0.01	0.00	9.42	2.00	0.00	0.00	0.01	0.00
9.43	2.00	0.00	0.00	0.01	0.00	9.44	2.00	0.00	0.00	0.01	0.00
9.45	2.00	0.00	0.00	0.01	0.00	9.46	2.00	0.00	0.00	0.01	0.00
9.47	2.00	0.00	0.00	0.01	0.00	9.48	2.00	0.00	0.00	0.01	0.00
9.49	2.00	0.00	0.00	0.01	0.00	9.50	2.00	0.00	0.00	0.01	0.00
9.51	2.00	0.00	0.00	0.01	0.00	9.52	2.00	0.00	0.00	0.01	0.00
9.53	2.00	0.00	0.00	0.01	0.00	9.54	1.29	0.00	0.00	0.01	0.00
9.55	1.39	0.00	0.00	0.01	0.00	9.56	1.47	0.00	0.00	0.01	0.00
9.57	1.67	0.00	0.00	0.01	0.00	9.58	1.65	0.00	0.00	0.01	0.00
9.59	1.66	0.00	0.00	0.01	0.00	9.60	1.66	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
9.61	1.56	0.00	0.00	0.01	0.00	9.62	1.45	0.00	0.00	0.01	0.00
9.63	1.41	0.00	0.00	0.01	0.00	9.64	1.37	0.00	0.00	0.01	0.00
9.65	1.33	0.00	0.00	0.01	0.00	9.66	2.00	0.00	0.00	0.01	0.00
9.67	2.00	0.00	0.00	0.01	0.00	9.68	2.00	0.00	0.00	0.01	0.00
9.69	2.00	0.00	0.00	0.01	0.00	9.70	2.00	0.00	0.00	0.01	0.00
9.71	2.00	0.00	0.00	0.01	0.00	9.72	2.00	0.00	0.00	0.01	0.00
9.73	2.00	0.00	0.00	0.01	0.00	9.74	2.00	0.00	0.00	0.01	0.00
9.75	2.00	0.00	0.00	0.01	0.00	9.76	2.00	0.00	0.00	0.01	0.00
9.77	2.00	0.00	0.00	0.01	0.00	9.78	2.00	0.00	0.00	0.01	0.00
9.79	2.00	0.00	0.00	0.01	0.00	9.80	2.00	0.00	0.00	0.01	0.00
9.81	2.00	0.00	0.00	0.01	0.00	9.82	2.00	0.00	0.00	0.01	0.00
9.83	2.00	0.00	0.00	0.01	0.00	9.84	2.00	0.00	0.00	0.01	0.00
9.85	2.00	0.00	0.00	0.01	0.00	9.86	2.00	0.00	0.00	0.01	0.00
9.87	2.00	0.00	0.00	0.01	0.00	9.88	2.00	0.00	0.00	0.01	0.00
9.89	2.00	0.00	0.00	0.01	0.00	9.90	2.00	0.00	0.00	0.01	0.00
9.91	2.00	0.00	0.00	0.01	0.00	9.92	2.00	0.00	0.00	0.01	0.00
9.93	2.00	0.00	0.00	0.01	0.00	9.94	2.00	0.00	0.00	0.01	0.00
9.95	2.00	0.00	0.00	0.01	0.00	9.96	2.00	0.00	0.00	0.01	0.00
9.97	2.00	0.00	0.00	0.01	0.00	9.98	2.00	0.00	0.00	0.01	0.00
9.99	2.00	0.00	0.00	0.01	0.00	10.00	2.00	0.00	0.00	0.01	0.00
10.01	2.00	0.00	0.00	0.01	0.00	10.02	2.00	0.00	0.00	0.01	0.00
10.03	2.00	0.00	0.00	0.01	0.00	10.04	2.00	0.00	0.00	0.01	0.00
10.05	2.00	0.00	0.00	0.01	0.00	10.06	2.00	0.00	0.00	0.01	0.00
10.07	2.00	0.00	0.00	0.01	0.00	10.08	2.00	0.00	0.00	0.01	0.00
10.09	2.00	0.00	0.00	0.01	0.00	10.10	2.00	0.00	0.00	0.01	0.00
10.11	2.00	0.00	0.00	0.01	0.00	10.12	2.00	0.00	0.00	0.01	0.00
10.13	2.00	0.00	0.00	0.01	0.00	10.14	2.00	0.00	0.00	0.01	0.00
10.15	2.00	0.00	0.00	0.01	0.00	10.16	2.00	0.00	0.00	0.01	0.00
10.17	2.00	0.00	0.00	0.01	0.00	10.18	2.00	0.00	0.00	0.01	0.00
10.19	2.00	0.00	0.00	0.01	0.00	10.20	2.00	0.00	0.00	0.01	0.00
10.21	2.00	0.00	0.00	0.01	0.00	10.22	2.00	0.00	0.00	0.01	0.00
10.23	2.00	0.00	0.00	0.01	0.00	10.24	2.00	0.00	0.00	0.01	0.00
10.25	2.00	0.00	0.00	0.01	0.00	10.26	2.00	0.00	0.00	0.01	0.00
10.27	2.00	0.00	0.00	0.01	0.00	10.28	2.00	0.00	0.00	0.01	0.00
10.29	2.00	0.00	0.00	0.01	0.00	10.30	2.00	0.00	0.00	0.01	0.00
10.31	2.00	0.00	0.00	0.01	0.00	10.32	2.00	0.00	0.00	0.01	0.00
10.33	2.00	0.00	0.00	0.01	0.00	10.34	2.00	0.00	0.00	0.01	0.00
10.35	2.00	0.00	0.00	0.01	0.00	10.36	2.00	0.00	0.00	0.01	0.00
10.37	2.00	0.00	0.00	0.01	0.00	10.38	2.00	0.00	0.00	0.01	0.00
10.39	2.00	0.00	0.00	0.01	0.00	10.40	2.00	0.00	0.00	0.01	0.00
10.41	2.00	0.00	0.00	0.01	0.00	10.42	2.00	0.00	0.00	0.01	0.00
10.43	2.00	0.00	0.00	0.01	0.00	10.44	2.00	0.00	0.00	0.01	0.00
10.45	2.00	0.00	0.00	0.01	0.00	10.46	1.12	0.00	0.00	0.01	0.00
10.47	1.14	0.00	0.00	0.01	0.00	10.48	1.16	0.00	0.00	0.01	0.00
10.49	1.18	0.00	0.00	0.01	0.00	10.50	1.20	0.00	0.00	0.01	0.00
10.51	1.20	0.00	0.00	0.01	0.00	10.52	2.00	0.00	0.00	0.01	0.00
10.53	2.00	0.00	0.00	0.01	0.00	10.54	2.00	0.00	0.00	0.01	0.00
10.55	2.00	0.00	0.00	0.01	0.00	10.56	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
10.57	2.00	0.00	0.00	0.01	0.00	10.58	2.00	0.00	0.00	0.01	0.00
10.59	2.00	0.00	0.00	0.01	0.00	10.60	2.00	0.00	0.00	0.01	0.00
10.61	2.00	0.00	0.00	0.01	0.00	10.62	2.00	0.00	0.00	0.01	0.00
10.63	2.00	0.00	0.00	0.01	0.00	10.64	2.00	0.00	0.00	0.01	0.00
10.65	2.00	0.00	0.00	0.01	0.00	10.66	2.00	0.00	0.00	0.01	0.00
10.67	2.00	0.00	0.00	0.01	0.00	10.68	2.00	0.00	0.00	0.01	0.00
10.69	2.00	0.00	0.00	0.01	0.00	10.70	2.00	0.00	0.00	0.01	0.00
10.71	2.00	0.00	0.00	0.01	0.00	10.72	2.00	0.00	0.00	0.01	0.00
10.73	2.00	0.00	0.00	0.01	0.00	10.74	2.00	0.00	0.00	0.01	0.00
10.75	2.00	0.00	0.00	0.01	0.00	10.76	2.00	0.00	0.00	0.01	0.00
10.77	2.00	0.00	0.00	0.01	0.00	10.78	2.00	0.00	0.00	0.01	0.00
10.79	2.00	0.00	0.00	0.01	0.00	10.80	2.00	0.00	0.00	0.01	0.00
10.81	2.00	0.00	0.00	0.01	0.00	10.82	2.00	0.00	0.00	0.01	0.00
10.83	2.00	0.00	0.00	0.01	0.00	10.84	2.00	0.00	0.00	0.01	0.00
10.85	2.00	0.00	0.00	0.01	0.00	10.86	2.00	0.00	0.00	0.01	0.00
10.87	2.00	0.00	0.00	0.01	0.00	10.88	2.00	0.00	0.00	0.01	0.00
10.89	2.00	0.00	0.00	0.01	0.00	10.90	2.00	0.00	0.00	0.01	0.00
10.91	2.00	0.00	0.00	0.01	0.00	10.92	2.00	0.00	0.00	0.01	0.00
10.93	2.00	0.00	0.00	0.01	0.00	10.94	2.00	0.00	0.00	0.01	0.00
10.95	2.00	0.00	0.00	0.01	0.00	10.96	2.00	0.00	0.00	0.01	0.00
10.97	2.00	0.00	0.00	0.01	0.00	10.98	2.00	0.00	0.00	0.01	0.00
10.99	2.00	0.00	0.00	0.01	0.00	11.00	2.00	0.00	0.00	0.01	0.00
11.01	2.00	0.00	0.00	0.01	0.00	11.02	2.00	0.00	0.00	0.01	0.00
11.03	2.00	0.00	0.00	0.01	0.00	11.04	2.00	0.00	0.00	0.01	0.00
11.05	2.00	0.00	0.00	0.01	0.00	11.06	2.00	0.00	0.00	0.01	0.00
11.07	1.30	0.00	0.00	0.01	0.00	11.08	1.28	0.00	0.00	0.01	0.00
11.09	1.39	0.00	0.00	0.01	0.00	11.10	1.45	0.00	0.00	0.01	0.00
11.11	1.45	0.00	0.00	0.01	0.00	11.12	1.45	0.00	0.00	0.01	0.00
11.13	1.46	0.00	0.00	0.01	0.00	11.14	1.03	0.00	0.00	0.01	0.00
11.15	1.06	0.00	0.00	0.01	0.00	11.16	1.08	0.00	0.00	0.01	0.00
11.17	1.15	0.00	0.00	0.01	0.00	11.18	1.19	0.00	0.00	0.01	0.00
11.19	1.23	0.00	0.00	0.01	0.00	11.20	1.32	0.00	0.00	0.01	0.00
11.21	1.35	0.00	0.00	0.01	0.00	11.22	1.37	0.00	0.00	0.01	0.00
11.23	1.37	0.00	0.00	0.01	0.00	11.24	1.36	0.00	0.00	0.01	0.00
11.25	1.33	0.00	0.00	0.01	0.00	11.26	1.32	0.00	0.00	0.01	0.00
11.27	1.30	0.00	0.00	0.01	0.00	11.28	1.30	0.00	0.00	0.01	0.00
11.29	1.59	0.00	0.00	0.01	0.00	11.30	1.64	0.00	0.00	0.01	0.00
11.31	1.67	0.00	0.00	0.01	0.00	11.32	1.70	0.00	0.00	0.01	0.00
11.33	1.75	0.00	0.00	0.01	0.00	11.34	1.77	0.00	0.00	0.01	0.00
11.35	1.79	0.00	0.00	0.01	0.00	11.36	1.81	0.00	0.00	0.01	0.00
11.37	1.85	0.00	0.00	0.01	0.00	11.38	1.85	0.00	0.00	0.01	0.00
11.39	1.89	0.00	0.00	0.01	0.00	11.40	1.89	0.00	0.00	0.01	0.00
11.41	1.89	0.00	0.00	0.01	0.00	11.42	1.85	0.00	0.00	0.01	0.00
11.43	1.87	0.00	0.00	0.01	0.00	11.44	1.81	0.00	0.00	0.01	0.00
11.45	1.76	0.00	0.00	0.01	0.00	11.46	1.66	0.00	0.00	0.01	0.00
11.47	1.39	0.00	0.00	0.01	0.00	11.48	1.40	0.00	0.00	0.01	0.00
11.49	1.69	0.00	0.00	0.01	0.00	11.50	1.73	0.00	0.00	0.01	0.00
11.51	1.76	0.00	0.00	0.01	0.00	11.52	1.77	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
11.53	1.76	0.00	0.00	0.01	0.00	11.54	1.73	0.00	0.00	0.01	0.00
11.55	1.70	0.00	0.00	0.01	0.00	11.56	1.69	0.00	0.00	0.01	0.00
11.57	1.71	0.00	0.00	0.01	0.00	11.58	1.73	0.00	0.00	0.01	0.00
11.59	1.80	0.00	0.00	0.01	0.00	11.60	1.76	0.00	0.00	0.01	0.00
11.61	1.80	0.00	0.00	0.01	0.00	11.62	1.70	0.00	0.00	0.01	0.00
11.63	1.69	0.00	0.00	0.01	0.00	11.64	1.59	0.00	0.00	0.01	0.00
11.65	1.58	0.00	0.00	0.01	0.00	11.66	1.55	0.00	0.00	0.01	0.00
11.67	1.55	0.00	0.00	0.01	0.00	11.68	1.59	0.00	0.00	0.01	0.00
11.69	1.65	0.00	0.00	0.01	0.00	11.70	1.73	0.00	0.00	0.01	0.00
11.71	1.73	0.00	0.00	0.01	0.00	11.72	1.68	0.00	0.00	0.01	0.00
11.73	1.63	0.00	0.00	0.01	0.00	11.74	1.64	0.00	0.00	0.01	0.00
11.75	1.62	0.00	0.00	0.01	0.00	11.76	1.58	0.00	0.00	0.01	0.00
11.77	1.61	0.00	0.00	0.01	0.00	11.78	1.71	0.00	0.00	0.01	0.00
11.79	1.74	0.00	0.00	0.01	0.00	11.80	1.83	0.00	0.00	0.01	0.00
11.81	1.82	0.00	0.00	0.01	0.00	11.82	1.83	0.00	0.00	0.01	0.00
11.83	1.82	0.00	0.00	0.01	0.00	11.84	1.79	0.00	0.00	0.01	0.00
11.85	1.71	0.00	0.00	0.01	0.00	11.86	1.64	0.00	0.00	0.01	0.00
11.87	1.61	0.00	0.00	0.01	0.00	11.88	1.61	0.00	0.00	0.01	0.00
11.89	1.64	0.00	0.00	0.01	0.00	11.90	1.67	0.00	0.00	0.01	0.00
11.91	1.67	0.00	0.00	0.01	0.00	11.92	1.70	0.00	0.00	0.01	0.00
11.93	1.74	0.00	0.00	0.01	0.00	11.94	1.65	0.00	0.00	0.01	0.00
11.95	1.92	0.00	0.00	0.01	0.00	11.96	1.92	0.00	0.00	0.01	0.00
11.97	1.97	0.00	0.00	0.01	0.00	11.98	1.97	0.00	0.00	0.01	0.00
11.99	1.95	0.00	0.00	0.01	0.00	12.00	1.95	0.00	0.00	0.01	0.00
12.01	1.95	0.00	0.00	0.01	0.00	12.02	1.91	0.00	0.00	0.01	0.00
12.03	1.69	0.00	0.00	0.01	0.00	12.04	1.67	0.00	0.00	0.01	0.00
12.05	1.67	0.00	0.00	0.01	0.00	12.06	1.67	0.00	0.00	0.01	0.00
12.07	1.84	0.00	0.00	0.01	0.00	12.08	1.87	0.00	0.00	0.01	0.00
12.09	1.92	0.00	0.00	0.01	0.00	12.10	1.97	0.00	0.00	0.01	0.00
12.11	2.00	0.00	0.00	0.01	0.00	12.12	1.99	0.00	0.00	0.01	0.00
12.13	2.00	0.00	0.00	0.01	0.00	12.14	2.00	0.00	0.00	0.01	0.00
12.15	1.95	0.00	0.00	0.01	0.00	12.16	1.95	0.00	0.00	0.01	0.00
12.17	1.91	0.00	0.00	0.01	0.00	12.18	1.93	0.00	0.00	0.01	0.00
12.19	1.96	0.00	0.00	0.01	0.00	12.20	2.00	0.00	0.00	0.01	0.00
12.21	2.00	0.00	0.00	0.01	0.00	12.22	2.00	0.00	0.00	0.01	0.00
12.23	2.00	0.00	0.00	0.01	0.00	12.24	2.00	0.00	0.00	0.01	0.00
12.25	2.00	0.00	0.00	0.01	0.00	12.26	2.00	0.00	0.00	0.01	0.00
12.27	2.00	0.00	0.00	0.01	0.00	12.28	2.00	0.00	0.00	0.01	0.00
12.29	2.00	0.00	0.00	0.01	0.00	12.30	1.98	0.00	0.00	0.01	0.00
12.31	1.94	0.00	0.00	0.01	0.00	12.32	1.87	0.00	0.00	0.01	0.00
12.33	1.85	0.00	0.00	0.01	0.00	12.34	1.86	0.00	0.00	0.01	0.00
12.35	1.88	0.00	0.00	0.01	0.00	12.36	1.89	0.00	0.00	0.01	0.00
12.37	1.93	0.00	0.00	0.01	0.00	12.38	1.96	0.00	0.00	0.01	0.00
12.39	2.00	0.00	0.00	0.01	0.00	12.40	2.00	0.00	0.00	0.01	0.00
12.41	2.00	0.00	0.00	0.01	0.00	12.42	2.00	0.00	0.00	0.01	0.00
12.43	2.00	0.00	0.00	0.01	0.00	12.44	2.00	0.00	0.00	0.01	0.00
12.45	2.00	0.00	0.00	0.01	0.00	12.46	1.93	0.00	0.00	0.01	0.00
12.47	1.77	0.00	0.00	0.01	0.00	12.48	1.71	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
12.49	1.68	0.00	0.00	0.01	0.00	12.50	1.66	0.00	0.00	0.01	0.00
12.51	1.68	0.00	0.00	0.01	0.00	12.52	1.78	0.00	0.00	0.01	0.00
12.53	1.83	0.00	0.00	0.01	0.00	12.54	2.00	0.00	0.00	0.01	0.00
12.55	2.00	0.00	0.00	0.01	0.00	12.56	2.00	0.00	0.00	0.01	0.00
12.57	2.00	0.00	0.00	0.01	0.00	12.58	2.00	0.00	0.00	0.01	0.00
12.59	2.00	0.00	0.00	0.01	0.00	12.60	2.00	0.00	0.00	0.01	0.00
12.61	2.00	0.00	0.00	0.01	0.00	12.62	2.00	0.00	0.00	0.01	0.00
12.63	2.00	0.00	0.00	0.01	0.00	12.64	2.00	0.00	0.00	0.01	0.00
12.65	2.00	0.00	0.00	0.01	0.00	12.66	2.00	0.00	0.00	0.01	0.00
12.67	2.00	0.00	0.00	0.01	0.00	12.68	2.00	0.00	0.00	0.01	0.00
12.69	2.00	0.00	0.00	0.01	0.00	12.70	2.00	0.00	0.00	0.01	0.00
12.71	2.00	0.00	0.00	0.01	0.00	12.72	2.00	0.00	0.00	0.01	0.00
12.73	2.00	0.00	0.00	0.01	0.00	12.74	2.00	0.00	0.00	0.01	0.00
12.75	2.00	0.00	0.00	0.01	0.00	12.76	2.00	0.00	0.00	0.01	0.00
12.77	2.00	0.00	0.00	0.01	0.00	12.78	2.00	0.00	0.00	0.01	0.00
12.79	2.00	0.00	0.00	0.01	0.00	12.80	2.00	0.00	0.00	0.01	0.00
12.81	2.00	0.00	0.00	0.01	0.00	12.82	2.00	0.00	0.00	0.01	0.00
12.83	2.00	0.00	0.00	0.01	0.00	12.84	2.00	0.00	0.00	0.01	0.00
12.85	2.00	0.00	0.00	0.01	0.00	12.86	2.00	0.00	0.00	0.01	0.00
12.87	2.00	0.00	0.00	0.01	0.00	12.88	2.00	0.00	0.00	0.01	0.00
12.89	2.00	0.00	0.00	0.01	0.00	12.90	2.00	0.00	0.00	0.01	0.00
12.91	2.00	0.00	0.00	0.01	0.00	12.92	2.00	0.00	0.00	0.01	0.00
12.93	2.00	0.00	0.00	0.01	0.00	12.94	2.00	0.00	0.00	0.01	0.00
12.95	2.00	0.00	0.00	0.01	0.00	12.96	2.00	0.00	0.00	0.01	0.00
12.97	2.00	0.00	0.00	0.01	0.00	12.98	2.00	0.00	0.00	0.01	0.00
12.99	2.00	0.00	0.00	0.01	0.00	13.00	2.00	0.00	0.00	0.01	0.00
13.01	2.00	0.00	0.00	0.01	0.00	13.02	2.00	0.00	0.00	0.01	0.00
13.03	2.00	0.00	0.00	0.01	0.00	13.04	2.00	0.00	0.00	0.01	0.00
13.05	2.00	0.00	0.00	0.01	0.00	13.06	2.00	0.00	0.00	0.01	0.00
13.07	2.00	0.00	0.00	0.01	0.00	13.08	2.00	0.00	0.00	0.01	0.00
13.09	2.00	0.00	0.00	0.01	0.00	13.10	2.00	0.00	0.00	0.01	0.00
13.11	2.00	0.00	0.00	0.01	0.00	13.12	2.00	0.00	0.00	0.01	0.00
13.13	2.00	0.00	0.00	0.01	0.00	13.14	2.00	0.00	0.00	0.01	0.00
13.15	2.00	0.00	0.00	0.01	0.00	13.16	2.00	0.00	0.00	0.01	0.00
13.17	2.00	0.00	0.00	0.01	0.00	13.18	2.00	0.00	0.00	0.01	0.00
13.19	2.00	0.00	0.00	0.01	0.00	13.20	2.00	0.00	0.00	0.01	0.00
13.21	2.00	0.00	0.00	0.01	0.00	13.22	2.00	0.00	0.00	0.01	0.00
13.23	2.00	0.00	0.00	0.01	0.00	13.24	2.00	0.00	0.00	0.01	0.00
13.25	2.00	0.00	0.00	0.01	0.00	13.26	2.00	0.00	0.00	0.01	0.00
13.27	2.00	0.00	0.00	0.01	0.00	13.28	2.00	0.00	0.00	0.01	0.00
13.29	2.00	0.00	0.00	0.01	0.00	13.30	2.00	0.00	0.00	0.01	0.00
13.31	2.00	0.00	0.00	0.01	0.00	13.32	2.00	0.00	0.00	0.01	0.00
13.33	2.00	0.00	0.00	0.01	0.00	13.34	2.00	0.00	0.00	0.01	0.00
13.35	2.00	0.00	0.00	0.01	0.00	13.36	2.00	0.00	0.00	0.01	0.00
13.37	2.00	0.00	0.00	0.01	0.00	13.38	2.00	0.00	0.00	0.01	0.00
13.39	2.00	0.00	0.00	0.01	0.00	13.40	2.00	0.00	0.00	0.01	0.00
13.41	2.00	0.00	0.00	0.01	0.00	13.42	2.00	0.00	0.00	0.01	0.00
13.43	2.00	0.00	0.00	0.01	0.00	13.44	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
13.45	2.00	0.00	0.00	0.01	0.00	13.46	2.00	0.00	0.00	0.01	0.00
13.47	2.00	0.00	0.00	0.01	0.00	13.48	2.00	0.00	0.00	0.01	0.00
13.49	2.00	0.00	0.00	0.01	0.00	13.50	2.00	0.00	0.00	0.01	0.00
13.51	2.00	0.00	0.00	0.01	0.00	13.52	2.00	0.00	0.00	0.01	0.00
13.53	2.00	0.00	0.00	0.01	0.00	13.54	2.00	0.00	0.00	0.01	0.00
13.55	2.00	0.00	0.00	0.01	0.00	13.56	2.00	0.00	0.00	0.01	0.00
13.57	2.00	0.00	0.00	0.01	0.00	13.58	2.00	0.00	0.00	0.01	0.00
13.59	2.00	0.00	0.00	0.01	0.00	13.60	2.00	0.00	0.00	0.01	0.00
13.61	2.00	0.00	0.00	0.01	0.00	13.62	2.00	0.00	0.00	0.01	0.00
13.63	2.00	0.00	0.00	0.01	0.00	13.64	2.00	0.00	0.00	0.01	0.00
13.65	2.00	0.00	0.00	0.01	0.00	13.66	2.00	0.00	0.00	0.01	0.00
13.67	2.00	0.00	0.00	0.01	0.00	13.68	2.00	0.00	0.00	0.01	0.00
13.69	2.00	0.00	0.00	0.01	0.00	13.70	2.00	0.00	0.00	0.01	0.00
13.71	2.00	0.00	0.00	0.01	0.00	13.72	2.00	0.00	0.00	0.01	0.00
13.73	2.00	0.00	0.00	0.01	0.00	13.74	2.00	0.00	0.00	0.01	0.00
13.75	2.00	0.00	0.00	0.01	0.00	13.76	2.00	0.00	0.00	0.01	0.00
13.77	2.00	0.00	0.00	0.01	0.00	13.78	1.78	0.00	0.00	0.01	0.00
13.79	1.82	0.00	0.00	0.01	0.00	13.80	1.85	0.00	0.00	0.01	0.00
13.81	1.87	0.00	0.00	0.01	0.00	13.82	2.00	0.00	0.00	0.01	0.00
13.83	2.00	0.00	0.00	0.01	0.00	13.84	2.00	0.00	0.00	0.01	0.00
13.85	2.00	0.00	0.00	0.01	0.00	13.86	2.00	0.00	0.00	0.01	0.00
13.87	1.98	0.00	0.00	0.01	0.00	13.88	1.99	0.00	0.00	0.01	0.00
13.89	2.00	0.00	0.00	0.01	0.00	13.90	2.00	0.00	0.00	0.01	0.00
13.91	2.00	0.00	0.00	0.01	0.00	13.92	2.00	0.00	0.00	0.01	0.00
13.93	2.00	0.00	0.00	0.01	0.00	13.94	2.00	0.00	0.00	0.01	0.00
13.95	2.00	0.00	0.00	0.01	0.00	13.96	2.00	0.00	0.00	0.01	0.00
13.97	2.00	0.00	0.00	0.01	0.00	13.98	2.00	0.00	0.00	0.01	0.00
13.99	2.00	0.00	0.00	0.01	0.00	14.00	2.00	0.00	0.00	0.01	0.00
14.01	2.00	0.00	0.00	0.01	0.00	14.02	2.00	0.00	0.00	0.01	0.00
14.03	2.00	0.00	0.00	0.01	0.00	14.04	2.00	0.00	0.00	0.01	0.00
14.05	2.00	0.00	0.00	0.01	0.00	14.06	2.00	0.00	0.00	0.01	0.00
14.07	2.00	0.00	0.00	0.01	0.00	14.08	2.00	0.00	0.00	0.01	0.00
14.09	2.00	0.00	0.00	0.01	0.00	14.10	2.00	0.00	0.00	0.01	0.00
14.11	2.00	0.00	0.00	0.01	0.00	14.12	2.00	0.00	0.00	0.01	0.00
14.13	2.00	0.00	0.00	0.01	0.00	14.14	2.00	0.00	0.00	0.01	0.00
14.15	1.97	0.00	0.00	0.01	0.00	14.16	1.94	0.00	0.00	0.01	0.00
14.17	1.93	0.00	0.00	0.01	0.00	14.18	1.92	0.00	0.00	0.01	0.00
14.19	1.90	0.00	0.00	0.01	0.00	14.20	1.93	0.00	0.00	0.01	0.00
14.21	1.91	0.00	0.00	0.01	0.00	14.22	1.96	0.00	0.00	0.01	0.00
14.23	1.96	0.00	0.00	0.01	0.00	14.24	2.00	0.00	0.00	0.01	0.00
14.25	2.00	0.00	0.00	0.01	0.00	14.26	2.00	0.00	0.00	0.01	0.00
14.27	1.85	0.00	0.00	0.01	0.00	14.28	1.85	0.00	0.00	0.01	0.00
14.29	1.84	0.00	0.00	0.01	0.00	14.30	1.85	0.00	0.00	0.01	0.00
14.31	1.85	0.00	0.00	0.01	0.00	14.32	1.86	0.00	0.00	0.01	0.00
14.33	1.86	0.00	0.00	0.01	0.00	14.34	1.88	0.00	0.00	0.01	0.00
14.35	1.90	0.00	0.00	0.01	0.00	14.36	1.94	0.00	0.00	0.01	0.00
14.37	2.00	0.00	0.00	0.01	0.00	14.38	2.00	0.00	0.00	0.01	0.00
14.39	2.00	0.00	0.00	0.01	0.00	14.40	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
14.41	2.00	0.00	0.00	0.01	0.00	14.42	2.00	0.00	0.00	0.01	0.00
14.43	2.00	0.00	0.00	0.01	0.00	14.44	2.00	0.00	0.00	0.01	0.00
14.45	2.00	0.00	0.00	0.01	0.00	14.46	2.00	0.00	0.00	0.01	0.00
14.47	2.00	0.00	0.00	0.01	0.00	14.48	2.00	0.00	0.00	0.01	0.00
14.49	2.00	0.00	0.00	0.01	0.00	14.50	2.00	0.00	0.00	0.01	0.00
14.51	2.00	0.00	0.00	0.01	0.00	14.52	2.00	0.00	0.00	0.01	0.00
14.53	1.92	0.00	0.00	0.01	0.00	14.54	1.88	0.00	0.00	0.01	0.00
14.55	1.88	0.00	0.00	0.01	0.00	14.56	1.85	0.00	0.00	0.01	0.00
14.57	1.83	0.00	0.00	0.01	0.00	14.58	1.98	0.00	0.00	0.01	0.00
14.59	1.99	0.00	0.00	0.01	0.00	14.60	2.00	0.00	0.00	0.01	0.00
14.61	2.00	0.00	0.00	0.01	0.00	14.62	2.00	0.00	0.00	0.01	0.00
14.63	2.00	0.00	0.00	0.01	0.00	14.64	2.00	0.00	0.00	0.01	0.00
14.65	2.00	0.00	0.00	0.01	0.00	14.66	2.00	0.00	0.00	0.01	0.00
14.67	2.00	0.00	0.00	0.01	0.00	14.68	2.00	0.00	0.00	0.01	0.00
14.69	2.00	0.00	0.00	0.01	0.00	14.70	2.00	0.00	0.00	0.01	0.00
14.71	2.00	0.00	0.00	0.01	0.00	14.72	2.00	0.00	0.00	0.01	0.00
14.73	2.00	0.00	0.00	0.01	0.00	14.74	2.00	0.00	0.00	0.01	0.00
14.75	2.00	0.00	0.00	0.01	0.00	14.76	2.00	0.00	0.00	0.01	0.00
14.77	1.99	0.00	0.00	0.01	0.00	14.78	1.75	0.00	0.00	0.01	0.00
14.79	1.75	0.00	0.00	0.01	0.00	14.80	1.88	0.00	0.00	0.01	0.00
14.81	2.00	0.00	0.00	0.01	0.00	14.82	2.00	0.00	0.00	0.01	0.00
14.83	2.00	0.00	0.00	0.01	0.00	14.84	2.00	0.00	0.00	0.01	0.00
14.85	2.00	0.00	0.00	0.01	0.00	14.86	2.00	0.00	0.00	0.01	0.00
14.87	2.00	0.00	0.00	0.01	0.00	14.88	2.00	0.00	0.00	0.01	0.00
14.89	2.00	0.00	0.00	0.01	0.00	14.90	2.00	0.00	0.00	0.01	0.00
14.91	2.00	0.00	0.00	0.01	0.00	14.92	2.00	0.00	0.00	0.01	0.00
14.93	2.00	0.00	0.00	0.01	0.00	14.94	2.00	0.00	0.00	0.01	0.00
14.95	2.00	0.00	0.00	0.01	0.00	14.96	2.00	0.00	0.00	0.01	0.00
14.97	2.00	0.00	0.00	0.01	0.00	14.98	2.00	0.00	0.00	0.01	0.00
14.99	2.00	0.00	0.00	0.01	0.00	15.00	2.00	0.00	0.00	0.01	0.00
15.01	2.00	0.00	0.00	0.01	0.00	15.02	2.00	0.00	0.00	0.01	0.00
15.03	2.00	0.00	0.00	0.01	0.00	15.04	2.00	0.00	0.00	0.01	0.00
15.05	1.96	0.00	0.00	0.01	0.00	15.06	1.98	0.00	0.00	0.01	0.00
15.07	2.00	0.00	0.00	0.01	0.00	15.08	2.00	0.00	0.00	0.01	0.00
15.09	2.00	0.00	0.00	0.01	0.00	15.10	2.00	0.00	0.00	0.01	0.00
15.11	2.00	0.00	0.00	0.01	0.00	15.12	2.00	0.00	0.00	0.01	0.00
15.13	2.00	0.00	0.00	0.01	0.00	15.14	2.00	0.00	0.00	0.01	0.00
15.15	2.00	0.00	0.00	0.01	0.00	15.16	2.00	0.00	0.00	0.01	0.00
15.17	2.00	0.00	0.00	0.01	0.00	15.18	2.00	0.00	0.00	0.01	0.00
15.19	2.00	0.00	0.00	0.01	0.00	15.20	2.00	0.00	0.00	0.01	0.00
15.21	2.00	0.00	0.00	0.01	0.00	15.22	2.00	0.00	0.00	0.01	0.00
15.23	2.00	0.00	0.00	0.01	0.00	15.24	2.00	0.00	0.00	0.01	0.00
15.25	2.00	0.00	0.00	0.01	0.00	15.26	2.00	0.00	0.00	0.01	0.00
15.27	2.00	0.00	0.00	0.01	0.00	15.28	2.00	0.00	0.00	0.01	0.00
15.29	2.00	0.00	0.00	0.01	0.00	15.30	2.00	0.00	0.00	0.01	0.00
15.31	1.98	0.00	0.00	0.01	0.00	15.32	1.77	0.00	0.00	0.01	0.00
15.33	1.69	0.00	0.00	0.01	0.00	15.34	2.00	0.00	0.00	0.01	0.00
15.35	2.00	0.00	0.00	0.01	0.00	15.36	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
15.37	2.00	0.00	0.00	0.01	0.00	15.38	2.00	0.00	0.00	0.01	0.00
15.39	2.00	0.00	0.00	0.01	0.00	15.40	2.00	0.00	0.00	0.01	0.00
15.41	2.00	0.00	0.00	0.01	0.00	15.42	2.00	0.00	0.00	0.01	0.00
15.43	2.00	0.00	0.00	0.01	0.00	15.44	2.00	0.00	0.00	0.01	0.00
15.45	2.00	0.00	0.00	0.01	0.00	15.46	2.00	0.00	0.00	0.01	0.00
15.47	2.00	0.00	0.00	0.01	0.00	15.48	2.00	0.00	0.00	0.01	0.00
15.49	2.00	0.00	0.00	0.01	0.00	15.50	2.00	0.00	0.00	0.01	0.00
15.51	2.00	0.00	0.00	0.01	0.00	15.52	2.00	0.00	0.00	0.01	0.00
15.53	2.00	0.00	0.00	0.01	0.00	15.54	2.00	0.00	0.00	0.01	0.00
15.55	2.00	0.00	0.00	0.01	0.00	15.56	2.00	0.00	0.00	0.01	0.00
15.57	2.00	0.00	0.00	0.01	0.00	15.58	2.00	0.00	0.00	0.01	0.00
15.59	2.00	0.00	0.00	0.01	0.00	15.60	2.00	0.00	0.00	0.01	0.00
15.61	2.00	0.00	0.00	0.01	0.00	15.62	2.00	0.00	0.00	0.01	0.00
15.63	2.00	0.00	0.00	0.01	0.00	15.64	2.00	0.00	0.00	0.01	0.00
15.65	2.00	0.00	0.00	0.01	0.00	15.66	2.00	0.00	0.00	0.01	0.00
15.67	2.00	0.00	0.00	0.01	0.00	15.68	2.00	0.00	0.00	0.01	0.00
15.69	2.00	0.00	0.00	0.01	0.00	15.70	2.00	0.00	0.00	0.01	0.00
15.71	2.00	0.00	0.00	0.01	0.00	15.72	2.00	0.00	0.00	0.01	0.00
15.73	2.00	0.00	0.00	0.01	0.00	15.74	2.00	0.00	0.00	0.01	0.00
15.75	1.36	0.00	0.00	0.01	0.00	15.76	1.53	0.00	0.00	0.01	0.00
15.77	1.57	0.00	0.00	0.01	0.00	15.78	1.68	0.00	0.00	0.01	0.00
15.79	1.68	0.00	0.00	0.01	0.00	15.80	1.69	0.00	0.00	0.01	0.00
15.81	1.65	0.00	0.00	0.01	0.00	15.82	1.67	0.00	0.00	0.01	0.00
15.83	1.62	0.00	0.00	0.01	0.00	15.84	1.68	0.00	0.00	0.01	0.00
15.85	1.73	0.00	0.00	0.01	0.00	15.86	1.81	0.00	0.00	0.01	0.00
15.87	1.83	0.00	0.00	0.01	0.00	15.88	1.78	0.00	0.00	0.01	0.00
15.89	1.62	0.00	0.00	0.01	0.00	15.90	2.00	0.00	0.00	0.01	0.00
15.91	2.00	0.00	0.00	0.01	0.00	15.92	2.00	0.00	0.00	0.01	0.00
15.93	2.00	0.00	0.00	0.01	0.00	15.94	2.00	0.00	0.00	0.01	0.00
15.95	2.00	0.00	0.00	0.01	0.00	15.96	2.00	0.00	0.00	0.01	0.00
15.97	2.00	0.00	0.00	0.01	0.00	15.98	2.00	0.00	0.00	0.01	0.00
15.99	2.00	0.00	0.00	0.01	0.00	16.00	2.00	0.00	0.00	0.01	0.00
16.01	2.00	0.00	0.00	0.01	0.00	16.02	2.00	0.00	0.00	0.01	0.00
16.03	2.00	0.00	0.00	0.01	0.00	16.04	2.00	0.00	0.00	0.01	0.00
16.05	2.00	0.00	0.00	0.01	0.00	16.06	2.00	0.00	0.00	0.01	0.00
16.07	2.00	0.00	0.00	0.01	0.00	16.08	2.00	0.00	0.00	0.01	0.00
16.09	2.00	0.00	0.00	0.01	0.00	16.10	2.00	0.00	0.00	0.01	0.00
16.11	2.00	0.00	0.00	0.01	0.00	16.12	2.00	0.00	0.00	0.01	0.00
16.13	2.00	0.00	0.00	0.01	0.00	16.14	2.00	0.00	0.00	0.01	0.00
16.15	2.00	0.00	0.00	0.01	0.00	16.16	2.00	0.00	0.00	0.01	0.00
16.17	2.00	0.00	0.00	0.01	0.00	16.18	2.00	0.00	0.00	0.01	0.00
16.19	2.00	0.00	0.00	0.01	0.00	16.20	2.00	0.00	0.00	0.01	0.00
16.21	2.00	0.00	0.00	0.01	0.00	16.22	2.00	0.00	0.00	0.01	0.00
16.23	2.00	0.00	0.00	0.01	0.00	16.24	2.00	0.00	0.00	0.01	0.00
16.25	2.00	0.00	0.00	0.01	0.00	16.26	2.00	0.00	0.00	0.01	0.00
16.27	2.00	0.00	0.00	0.01	0.00	16.28	2.00	0.00	0.00	0.01	0.00
16.29	2.00	0.00	0.00	0.01	0.00	16.30	2.00	0.00	0.00	0.01	0.00
16.31	2.00	0.00	0.00	0.01	0.00	16.32	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
16.33	2.00	0.00	0.00	0.01	0.00	16.34	2.00	0.00	0.00	0.01	0.00
16.35	2.00	0.00	0.00	0.01	0.00	16.36	2.00	0.00	0.00	0.01	0.00
16.37	2.00	0.00	0.00	0.01	0.00	16.38	2.00	0.00	0.00	0.01	0.00
16.39	2.00	0.00	0.00	0.01	0.00	16.40	2.00	0.00	0.00	0.01	0.00
16.41	2.00	0.00	0.00	0.01	0.00	16.42	2.00	0.00	0.00	0.01	0.00
16.43	2.00	0.00	0.00	0.01	0.00	16.44	2.00	0.00	0.00	0.01	0.00
16.45	2.00	0.00	0.00	0.01	0.00	16.46	2.00	0.00	0.00	0.01	0.00
16.47	2.00	0.00	0.00	0.01	0.00	16.48	2.00	0.00	0.00	0.01	0.00
16.49	2.00	0.00	0.00	0.01	0.00	16.50	2.00	0.00	0.00	0.01	0.00
16.51	2.00	0.00	0.00	0.01	0.00	16.52	2.00	0.00	0.00	0.01	0.00
16.53	2.00	0.00	0.00	0.01	0.00	16.54	2.00	0.00	0.00	0.01	0.00
16.55	2.00	0.00	0.00	0.01	0.00	16.56	2.00	0.00	0.00	0.01	0.00
16.57	2.00	0.00	0.00	0.01	0.00	16.58	2.00	0.00	0.00	0.01	0.00
16.59	2.00	0.00	0.00	0.01	0.00	16.60	2.00	0.00	0.00	0.01	0.00
16.61	2.00	0.00	0.00	0.01	0.00	16.62	2.00	0.00	0.00	0.01	0.00
16.63	1.51	0.00	0.00	0.01	0.00	16.64	1.66	0.00	0.00	0.01	0.00
16.65	1.80	0.00	0.00	0.01	0.00	16.66	1.83	0.00	0.00	0.01	0.00
16.67	1.96	0.00	0.00	0.01	0.00	16.68	1.99	0.00	0.00	0.01	0.00
16.69	2.00	0.00	0.00	0.01	0.00	16.70	2.00	0.00	0.00	0.01	0.00
16.71	1.98	0.00	0.00	0.01	0.00	16.72	1.96	0.00	0.00	0.01	0.00
16.73	1.94	0.00	0.00	0.01	0.00	16.74	1.92	0.00	0.00	0.01	0.00
16.75	2.00	0.00	0.00	0.01	0.00	16.76	2.00	0.00	0.00	0.01	0.00
16.77	2.00	0.00	0.00	0.01	0.00	16.78	2.00	0.00	0.00	0.01	0.00
16.79	2.00	0.00	0.00	0.01	0.00	16.80	2.00	0.00	0.00	0.01	0.00
16.81	2.00	0.00	0.00	0.01	0.00	16.82	2.00	0.00	0.00	0.01	0.00
16.83	2.00	0.00	0.00	0.01	0.00	16.84	2.00	0.00	0.00	0.01	0.00
16.85	2.00	0.00	0.00	0.01	0.00	16.86	2.00	0.00	0.00	0.01	0.00
16.87	2.00	0.00	0.00	0.01	0.00	16.88	2.00	0.00	0.00	0.01	0.00
16.89	2.00	0.00	0.00	0.01	0.00	16.90	2.00	0.00	0.00	0.01	0.00
16.91	2.00	0.00	0.00	0.01	0.00	16.92	2.00	0.00	0.00	0.01	0.00
16.93	2.00	0.00	0.00	0.01	0.00	16.94	2.00	0.00	0.00	0.01	0.00
16.95	2.00	0.00	0.00	0.01	0.00	16.96	2.00	0.00	0.00	0.01	0.00
16.97	2.00	0.00	0.00	0.01	0.00	16.98	2.00	0.00	0.00	0.01	0.00
16.99	2.00	0.00	0.00	0.01	0.00	17.00	2.00	0.00	0.00	0.01	0.00
17.01	2.00	0.00	0.00	0.01	0.00	17.02	2.00	0.00	0.00	0.01	0.00
17.03	2.00	0.00	0.00	0.01	0.00	17.04	2.00	0.00	0.00	0.01	0.00
17.05	2.00	0.00	0.00	0.01	0.00	17.06	2.00	0.00	0.00	0.01	0.00
17.07	2.00	0.00	0.00	0.01	0.00	17.08	2.00	0.00	0.00	0.01	0.00
17.09	2.00	0.00	0.00	0.01	0.00	17.10	2.00	0.00	0.00	0.01	0.00
17.11	2.00	0.00	0.00	0.01	0.00	17.12	2.00	0.00	0.00	0.01	0.00
17.13	2.00	0.00	0.00	0.01	0.00	17.14	2.00	0.00	0.00	0.01	0.00
17.15	2.00	0.00	0.00	0.01	0.00	17.16	2.00	0.00	0.00	0.01	0.00
17.17	2.00	0.00	0.00	0.01	0.00	17.18	2.00	0.00	0.00	0.01	0.00
17.19	2.00	0.00	0.00	0.01	0.00	17.20	2.00	0.00	0.00	0.01	0.00
17.21	2.00	0.00	0.00	0.01	0.00	17.22	2.00	0.00	0.00	0.01	0.00
17.23	2.00	0.00	0.00	0.01	0.00	17.24	2.00	0.00	0.00	0.01	0.00
17.25	2.00	0.00	0.00	0.01	0.00	17.26	2.00	0.00	0.00	0.01	0.00
17.27	2.00	0.00	0.00	0.01	0.00	17.28	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
17.29	2.00	0.00	0.00	0.01	0.00	17.30	2.00	0.00	0.00	0.01	0.00
17.31	2.00	0.00	0.00	0.01	0.00	17.32	2.00	0.00	0.00	0.01	0.00
17.33	2.00	0.00	0.00	0.01	0.00	17.34	2.00	0.00	0.00	0.01	0.00
17.35	2.00	0.00	0.00	0.01	0.00	17.36	2.00	0.00	0.00	0.01	0.00
17.37	2.00	0.00	0.00	0.01	0.00	17.38	2.00	0.00	0.00	0.01	0.00
17.39	2.00	0.00	0.00	0.01	0.00	17.40	2.00	0.00	0.00	0.01	0.00
17.41	2.00	0.00	0.00	0.01	0.00	17.42	2.00	0.00	0.00	0.01	0.00
17.43	2.00	0.00	0.00	0.01	0.00	17.44	2.00	0.00	0.00	0.01	0.00
17.45	2.00	0.00	0.00	0.01	0.00	17.46	2.00	0.00	0.00	0.01	0.00
17.47	2.00	0.00	0.00	0.01	0.00	17.48	2.00	0.00	0.00	0.01	0.00
17.49	2.00	0.00	0.00	0.01	0.00	17.50	2.00	0.00	0.00	0.01	0.00
17.51	2.00	0.00	0.00	0.01	0.00	17.52	2.00	0.00	0.00	0.01	0.00
17.53	2.00	0.00	0.00	0.01	0.00	17.54	2.00	0.00	0.00	0.01	0.00
17.55	2.00	0.00	0.00	0.01	0.00	17.56	2.00	0.00	0.00	0.01	0.00
17.57	2.00	0.00	0.00	0.01	0.00	17.58	2.00	0.00	0.00	0.01	0.00
17.59	2.00	0.00	0.00	0.01	0.00	17.60	2.00	0.00	0.00	0.01	0.00
17.61	2.00	0.00	0.00	0.01	0.00	17.62	2.00	0.00	0.00	0.01	0.00
17.63	2.00	0.00	0.00	0.01	0.00	17.64	2.00	0.00	0.00	0.01	0.00
17.65	2.00	0.00	0.00	0.01	0.00	17.66	2.00	0.00	0.00	0.01	0.00
17.67	2.00	0.00	0.00	0.01	0.00	17.68	2.00	0.00	0.00	0.01	0.00
17.69	2.00	0.00	0.00	0.01	0.00	17.70	2.00	0.00	0.00	0.01	0.00
17.71	2.00	0.00	0.00	0.01	0.00	17.72	2.00	0.00	0.00	0.01	0.00
17.73	2.00	0.00	0.00	0.01	0.00	17.74	2.00	0.00	0.00	0.01	0.00
17.75	2.00	0.00	0.00	0.01	0.00	17.76	2.00	0.00	0.00	0.01	0.00
17.77	2.00	0.00	0.00	0.01	0.00	17.78	2.00	0.00	0.00	0.01	0.00
17.79	2.00	0.00	0.00	0.01	0.00	17.80	2.00	0.00	0.00	0.01	0.00
17.81	2.00	0.00	0.00	0.01	0.00	17.82	2.00	0.00	0.00	0.01	0.00
17.83	2.00	0.00	0.00	0.01	0.00	17.84	2.00	0.00	0.00	0.01	0.00
17.85	2.00	0.00	0.00	0.01	0.00	17.86	2.00	0.00	0.00	0.01	0.00
17.87	2.00	0.00	0.00	0.01	0.00	17.88	2.00	0.00	0.00	0.01	0.00
17.89	2.00	0.00	0.00	0.01	0.00	17.90	2.00	0.00	0.00	0.01	0.00
17.91	2.00	0.00	0.00	0.01	0.00	17.92	2.00	0.00	0.00	0.01	0.00
17.93	2.00	0.00	0.00	0.01	0.00	17.94	2.00	0.00	0.00	0.01	0.00
17.95	2.00	0.00	0.00	0.01	0.00	17.96	2.00	0.00	0.00	0.01	0.00
17.97	2.00	0.00	0.00	0.01	0.00	17.98	2.00	0.00	0.00	0.01	0.00
17.99	2.00	0.00	0.00	0.01	0.00	18.00	2.00	0.00	0.00	0.01	0.00
18.01	2.00	0.00	0.00	0.01	0.00	18.02	2.00	0.00	0.00	0.01	0.00
18.03	2.00	0.00	0.00	0.01	0.00	18.04	2.00	0.00	0.00	0.01	0.00
18.05	2.00	0.00	0.00	0.01	0.00	18.06	2.00	0.00	0.00	0.01	0.00
18.07	2.00	0.00	0.00	0.01	0.00	18.08	2.00	0.00	0.00	0.01	0.00
18.09	2.00	0.00	0.00	0.01	0.00	18.10	2.00	0.00	0.00	0.01	0.00
18.11	2.00	0.00	0.00	0.01	0.00	18.12	2.00	0.00	0.00	0.01	0.00
18.13	2.00	0.00	0.00	0.01	0.00	18.14	2.00	0.00	0.00	0.01	0.00
18.15	2.00	0.00	0.00	0.01	0.00	18.16	2.00	0.00	0.00	0.01	0.00
18.17	2.00	0.00	0.00	0.01	0.00	18.18	2.00	0.00	0.00	0.01	0.00
18.19	2.00	0.00	0.00	0.01	0.00	18.20	2.00	0.00	0.00	0.01	0.00
18.21	2.00	0.00	0.00	0.01	0.00	18.22	2.00	0.00	0.00	0.01	0.00
18.23	2.00	0.00	0.00	0.01	0.00	18.24	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
18.25	2.00	0.00	0.00	0.01	0.00	18.26	2.00	0.00	0.00	0.01	0.00
18.27	2.00	0.00	0.00	0.01	0.00	18.28	2.00	0.00	0.00	0.01	0.00
18.29	2.00	0.00	0.00	0.01	0.00	18.30	2.00	0.00	0.00	0.01	0.00
18.31	2.00	0.00	0.00	0.01	0.00	18.32	2.00	0.00	0.00	0.01	0.00
18.33	2.00	0.00	0.00	0.01	0.00	18.34	2.00	0.00	0.00	0.01	0.00
18.35	2.00	0.00	0.00	0.01	0.00	18.36	2.00	0.00	0.00	0.01	0.00
18.37	2.00	0.00	0.00	0.01	0.00	18.38	2.00	0.00	0.00	0.01	0.00
18.39	2.00	0.00	0.00	0.01	0.00	18.40	2.00	0.00	0.00	0.01	0.00
18.41	2.00	0.00	0.00	0.01	0.00	18.42	2.00	0.00	0.00	0.01	0.00
18.43	2.00	0.00	0.00	0.01	0.00	18.44	2.00	0.00	0.00	0.01	0.00
18.45	2.00	0.00	0.00	0.01	0.00	18.46	2.00	0.00	0.00	0.01	0.00
18.47	2.00	0.00	0.00	0.01	0.00	18.48	2.00	0.00	0.00	0.01	0.00
18.49	2.00	0.00	0.00	0.01	0.00	18.50	2.00	0.00	0.00	0.01	0.00
18.51	2.00	0.00	0.00	0.01	0.00	18.52	2.00	0.00	0.00	0.01	0.00
18.53	2.00	0.00	0.00	0.01	0.00	18.54	2.00	0.00	0.00	0.01	0.00
18.55	2.00	0.00	0.00	0.01	0.00	18.56	2.00	0.00	0.00	0.01	0.00
18.57	2.00	0.00	0.00	0.01	0.00	18.58	2.00	0.00	0.00	0.01	0.00
18.59	2.00	0.00	0.00	0.01	0.00	18.60	2.00	0.00	0.00	0.01	0.00
18.61	2.00	0.00	0.00	0.01	0.00	18.62	2.00	0.00	0.00	0.01	0.00
18.63	2.00	0.00	0.00	0.01	0.00	18.64	2.00	0.00	0.00	0.01	0.00
18.65	2.00	0.00	0.00	0.01	0.00	18.66	2.00	0.00	0.00	0.01	0.00
18.67	2.00	0.00	0.00	0.01	0.00	18.68	2.00	0.00	0.00	0.01	0.00
18.69	2.00	0.00	0.00	0.01	0.00	18.70	2.00	0.00	0.00	0.01	0.00
18.71	2.00	0.00	0.00	0.01	0.00	18.72	2.00	0.00	0.00	0.01	0.00
18.73	2.00	0.00	0.00	0.01	0.00	18.74	2.00	0.00	0.00	0.01	0.00
18.75	2.00	0.00	0.00	0.01	0.00	18.76	2.00	0.00	0.00	0.01	0.00
18.77	2.00	0.00	0.00	0.01	0.00	18.78	2.00	0.00	0.00	0.01	0.00
18.79	2.00	0.00	0.00	0.01	0.00	18.80	2.00	0.00	0.00	0.01	0.00
18.81	2.00	0.00	0.00	0.01	0.00	18.82	2.00	0.00	0.00	0.01	0.00
18.83	2.00	0.00	0.00	0.01	0.00	18.84	2.00	0.00	0.00	0.01	0.00
18.85	2.00	0.00	0.00	0.01	0.00	18.86	2.00	0.00	0.00	0.01	0.00
18.87	2.00	0.00	0.00	0.01	0.00	18.88	2.00	0.00	0.00	0.01	0.00
18.89	2.00	0.00	0.00	0.01	0.00	18.90	2.00	0.00	0.00	0.01	0.00
18.91	2.00	0.00	0.00	0.01	0.00	18.92	2.00	0.00	0.00	0.01	0.00
18.93	2.00	0.00	0.00	0.01	0.00	18.94	2.00	0.00	0.00	0.01	0.00
18.95	2.00	0.00	0.00	0.01	0.00	18.96	2.00	0.00	0.00	0.01	0.00
18.97	1.67	0.00	0.00	0.01	0.00	18.98	1.69	0.00	0.00	0.01	0.00
18.99	1.77	0.00	0.00	0.01	0.00	19.00	1.80	0.00	0.00	0.01	0.00
19.01	1.87	0.00	0.00	0.01	0.00	19.02	1.88	0.00	0.00	0.01	0.00
19.03	1.86	0.00	0.00	0.01	0.00	19.04	1.84	0.00	0.00	0.01	0.00
19.05	1.77	0.00	0.00	0.01	0.00	19.06	1.75	0.00	0.00	0.01	0.00
19.07	1.71	0.00	0.00	0.01	0.00	19.08	2.00	0.00	0.00	0.01	0.00
19.09	2.00	0.00	0.00	0.01	0.00	19.10	2.00	0.00	0.00	0.01	0.00
19.11	2.00	0.00	0.00	0.01	0.00	19.12	2.00	0.00	0.00	0.01	0.00
19.13	2.00	0.00	0.00	0.01	0.00	19.14	2.00	0.00	0.00	0.01	0.00
19.15	2.00	0.00	0.00	0.01	0.00	19.16	1.88	0.00	0.00	0.01	0.00
19.17	1.98	0.00	0.00	0.01	0.00	19.18	2.00	0.00	0.00	0.01	0.00
19.19	2.00	0.00	0.00	0.01	0.00	19.20	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
19.21	2.00	0.00	0.00	0.01	0.00	19.22	2.00	0.00	0.00	0.01	0.00
19.23	2.00	0.00	0.00	0.01	0.00	19.24	2.00	0.00	0.00	0.01	0.00
19.25	2.00	0.00	0.00	0.01	0.00	19.26	2.00	0.00	0.00	0.01	0.00
19.27	2.00	0.00	0.00	0.01	0.00	19.28	2.00	0.00	0.00	0.01	0.00
19.29	2.00	0.00	0.00	0.01	0.00	19.30	2.00	0.00	0.00	0.01	0.00
19.31	2.00	0.00	0.00	0.01	0.00	19.32	2.00	0.00	0.00	0.01	0.00
19.33	2.00	0.00	0.00	0.01	0.00	19.34	2.00	0.00	0.00	0.01	0.00
19.35	2.00	0.00	0.00	0.01	0.00	19.36	2.00	0.00	0.00	0.01	0.00
19.37	2.00	0.00	0.00	0.01	0.00	19.38	2.00	0.00	0.00	0.01	0.00
19.39	2.00	0.00	0.00	0.01	0.00	19.40	2.00	0.00	0.00	0.01	0.00
19.41	2.00	0.00	0.00	0.01	0.00	19.42	2.00	0.00	0.00	0.01	0.00
19.43	2.00	0.00	0.00	0.01	0.00	19.44	1.97	0.00	0.00	0.01	0.00
19.45	1.94	0.00	0.00	0.01	0.00	19.46	1.94	0.00	0.00	0.01	0.00
19.47	1.90	0.00	0.00	0.01	0.00	19.48	1.89	0.00	0.00	0.01	0.00
19.49	1.93	0.00	0.00	0.01	0.00	19.50	1.96	0.00	0.00	0.01	0.00
19.51	2.00	0.00	0.00	0.01	0.00	19.52	2.00	0.00	0.00	0.01	0.00
19.53	2.00	0.00	0.00	0.01	0.00	19.54	2.00	0.00	0.00	0.01	0.00
19.55	2.00	0.00	0.00	0.01	0.00	19.56	2.00	0.00	0.00	0.01	0.00
19.57	2.00	0.00	0.00	0.01	0.00	19.58	2.00	0.00	0.00	0.01	0.00
19.59	2.00	0.00	0.00	0.01	0.00	19.60	2.00	0.00	0.00	0.01	0.00
19.61	2.00	0.00	0.00	0.01	0.00	19.62	2.00	0.00	0.00	0.01	0.00
19.63	2.00	0.00	0.00	0.01	0.00	19.64	2.00	0.00	0.00	0.01	0.00
19.65	1.92	0.00	0.00	0.01	0.00	19.66	1.92	0.00	0.00	0.01	0.00
19.67	1.92	0.00	0.00	0.01	0.00	19.68	1.91	0.00	0.00	0.01	0.00
19.69	1.91	0.00	0.00	0.01	0.00	19.70	1.90	0.00	0.00	0.01	0.00
19.71	1.91	0.00	0.00	0.01	0.00	19.72	1.91	0.00	0.00	0.01	0.00
19.73	1.91	0.00	0.00	0.01	0.00	19.74	1.91	0.00	0.00	0.01	0.00
19.75	2.00	0.00	0.00	0.01	0.00	19.76	2.00	0.00	0.00	0.01	0.00
19.77	2.00	0.00	0.00	0.01	0.00	19.78	2.00	0.00	0.00	0.01	0.00
19.79	2.00	0.00	0.00	0.01	0.00	19.80	2.00	0.00	0.00	0.01	0.00
19.81	2.00	0.00	0.00	0.01	0.00	19.82	2.00	0.00	0.00	0.01	0.00
19.83	2.00	0.00	0.00	0.01	0.00	19.84	2.00	0.00	0.00	0.01	0.00
19.85	2.00	0.00	0.00	0.01	0.00	19.86	2.00	0.00	0.00	0.01	0.00
19.87	2.00	0.00	0.00	0.01	0.00	19.88	2.00	0.00	0.00	0.01	0.00
19.89	2.00	0.00	0.00	0.01	0.00	19.90	2.00	0.00	0.00	0.01	0.00
19.91	2.00	0.00	0.00	0.01	0.00	19.92	2.00	0.00	0.00	0.01	0.00
19.93	2.00	0.00	0.00	0.01	0.00	19.94	2.00	0.00	0.00	0.01	0.00
19.95	2.00	0.00	0.00	0.01	0.00	19.96	2.00	0.00	0.00	0.01	0.00
19.97	2.00	0.00	0.00	0.01	0.00	19.98	2.00	0.00	0.00	0.01	0.00
19.99	2.00	0.00	0.00	0.01	0.00	20.00	2.00	0.00	0.00	0.01	0.00

Overall liquefaction potential: 0.00

LPI_{ISH} > 5.0 - Liquefaction manifestation is expected

Abbreviations

FS: Calculated factor of safety for test point
d_z: Layer thickness (m)
LPI: Liquefaction potential index value for test point

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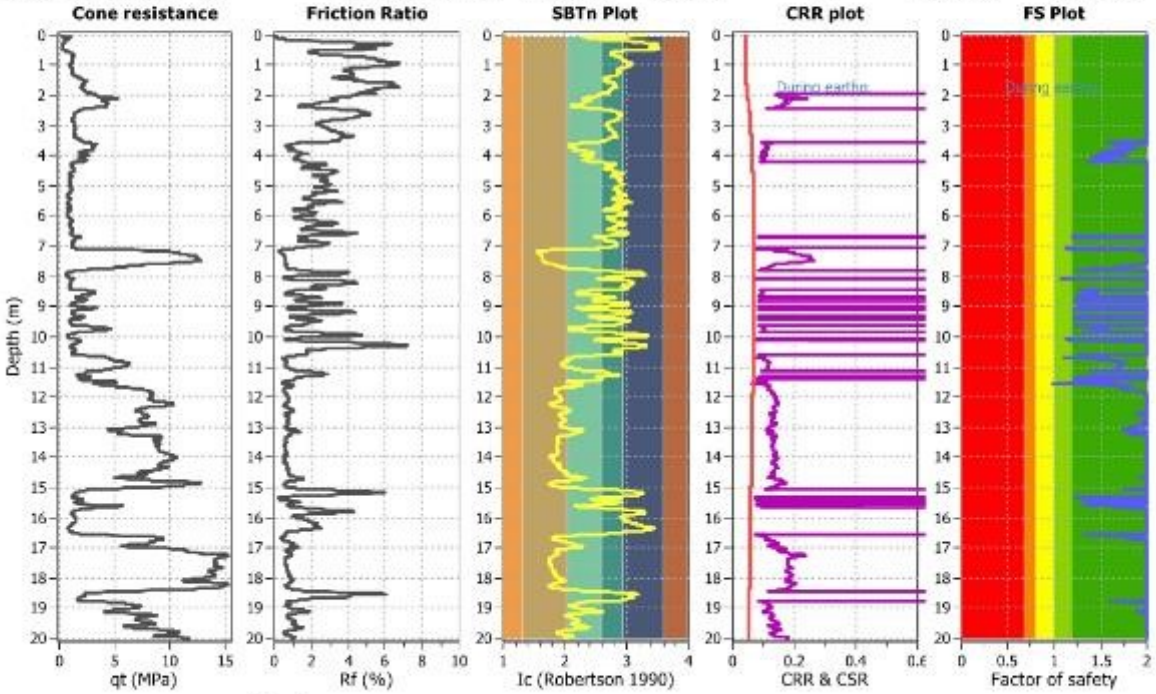
LIQUEFACTION ANALYSIS REPORT

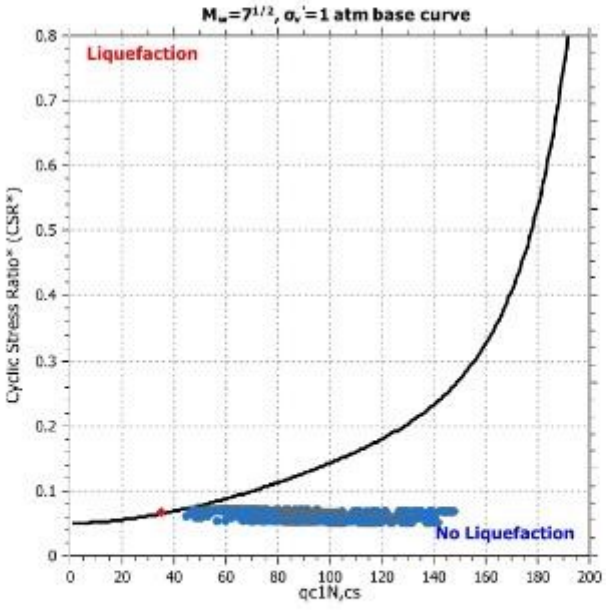
Project title : **Location :**

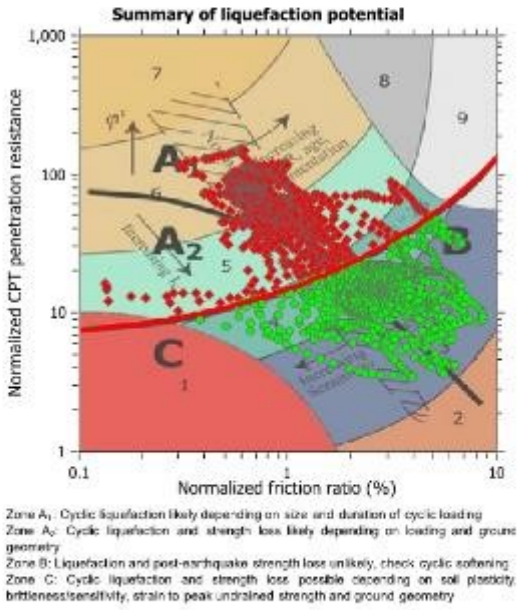
CPT file : CPTU3 - Basic

Input parameters and analysis data

Analysis method:	I&B (2008)	G.W.T. (in-situ):	1.40 m	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	R&W (1998)	G.W.T. (earthq.):	1.40 m	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	5.45	Ic cut-off value:	2.60	Trans. detect. applied:	No	MSF method:	Method based
Peak ground acceleration:	0.12	Unit weight calculation:	Based on SBT	K_o applied:	Yes		

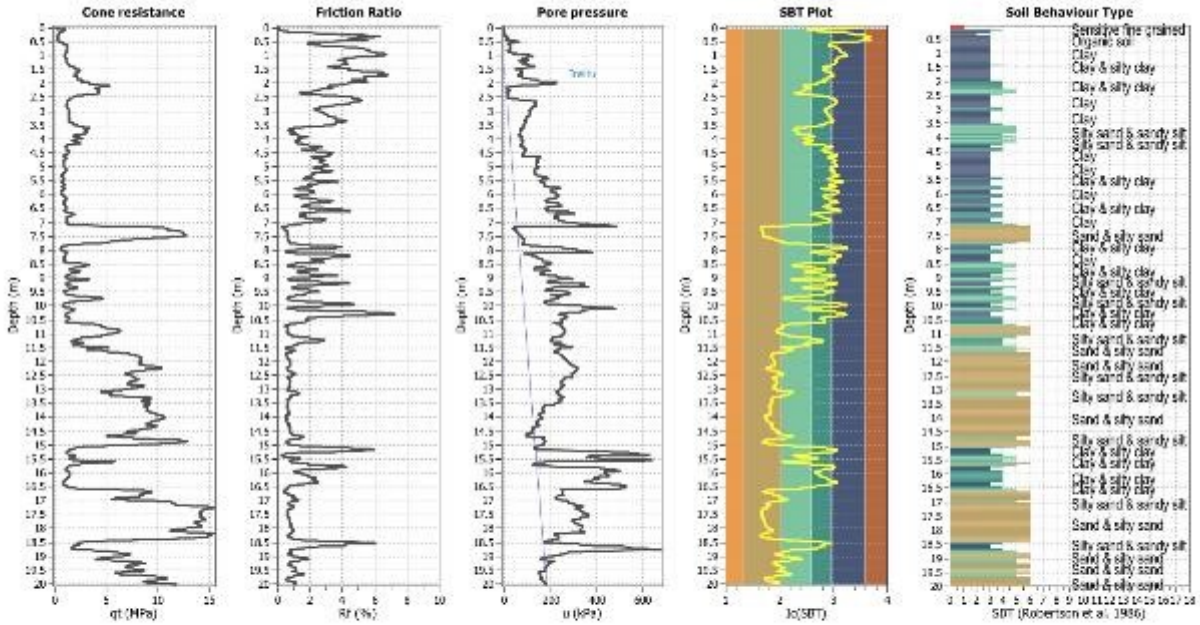






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



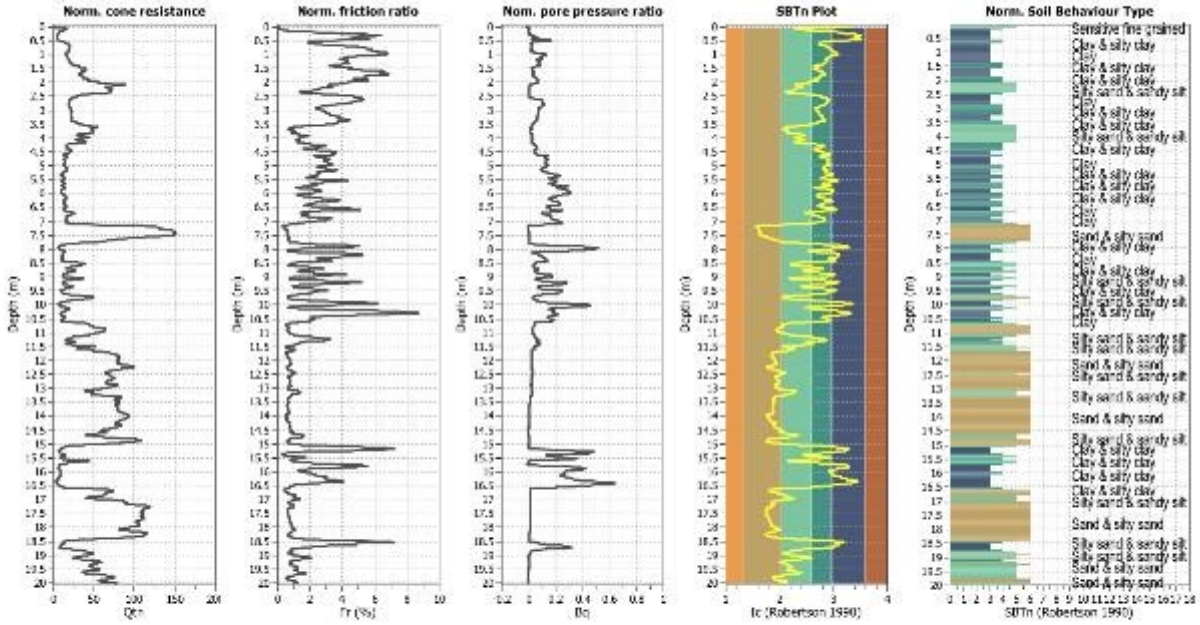
Input parameters and analysis data

Analysis method:	ISBI (2016)	Depth to GWT (erthq.):	1.40 m	Fill weight:	N/A
Flow correction method:	RAW (1998)	Average results interval:	3	Transition layers applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	$K_{c,200}$ limit:	Yes
Earthquake magnitude M_w:	5.45	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.12	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.40 m	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravelly sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



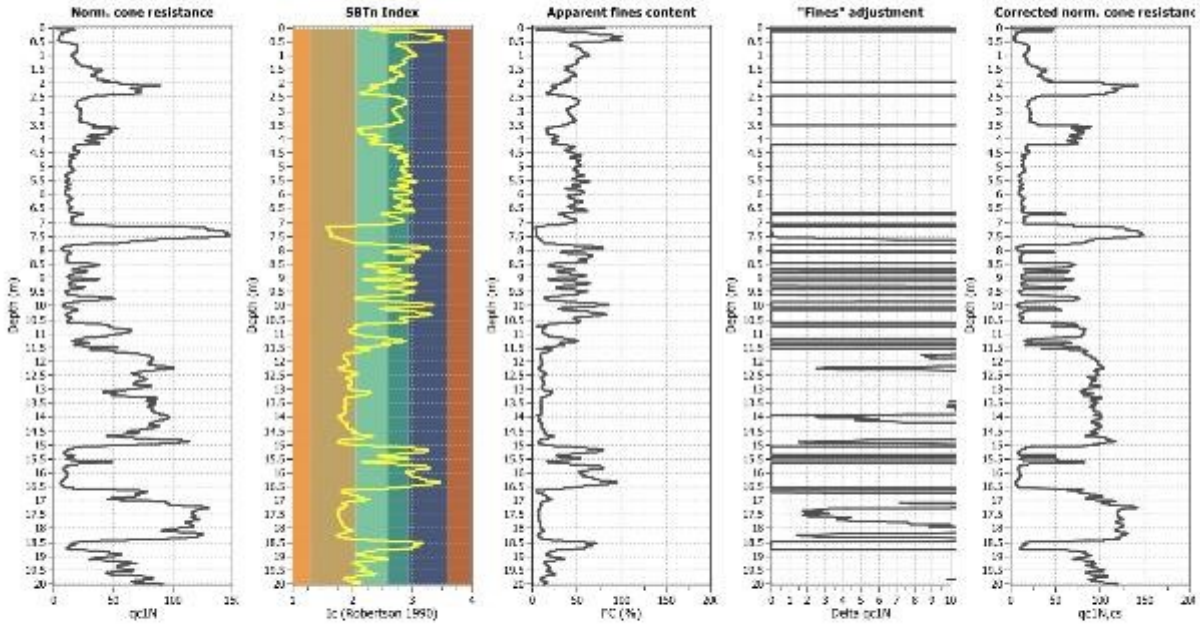
Input parameters and analysis data

Analysis method:	ISBI (2016)	Depth to GWT (erthq.):	1.40 m	Fill weight:	N/A
Flow correction method:	RAW (1998)	Average results interval:	3	Transition layers applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	$K_{c,200}$ limit:	Yes
Earthquake magnitude M_w:	5.45	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.12	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.40 m	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravelly sand to sand
8. Very stiff sand to
9. Very stiff fine grained

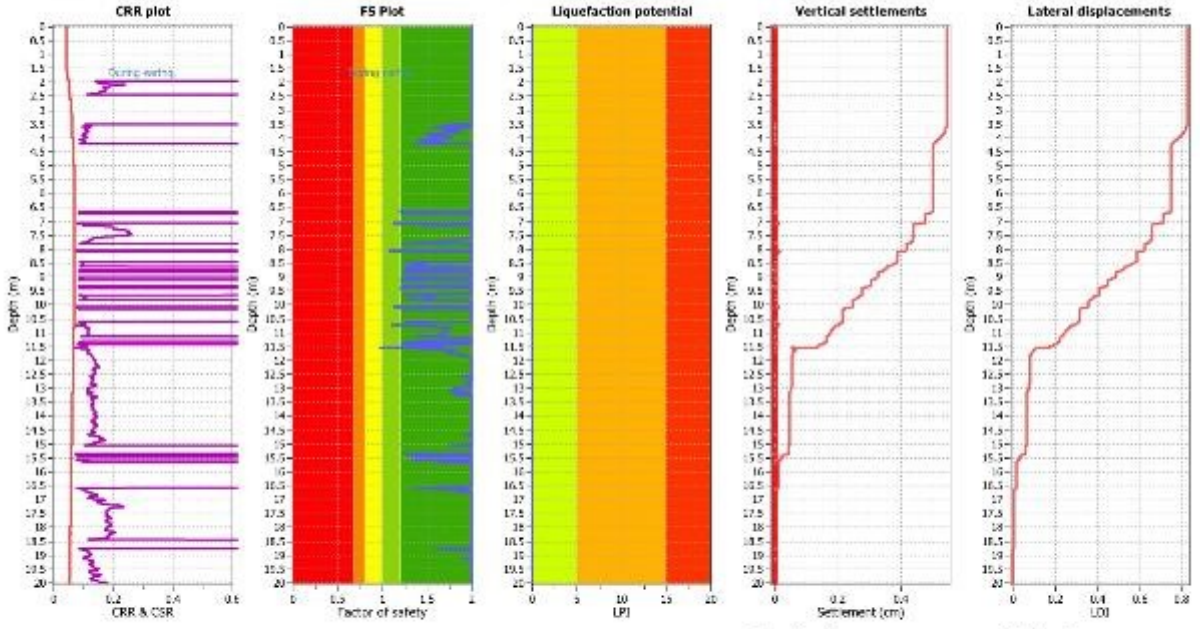
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	IBB (2016)	Depth to GWT (erthq.):	1.40 m	Fill weight:	N/A
Flow correction method:	RAW (1998)	Average results interval:	3	Transition layers applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w:	5.45	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.12	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.40 m	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	IBB (2016)	Depth to GWT (erthq.):	1.40 m	Fill weight:	N/A
Flow correction method:	RAW (1998)	Average results interval:	3	Transition layers applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w:	5.45	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.12	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.40 m	Fill height:	N/A	Limit depth:	N/A

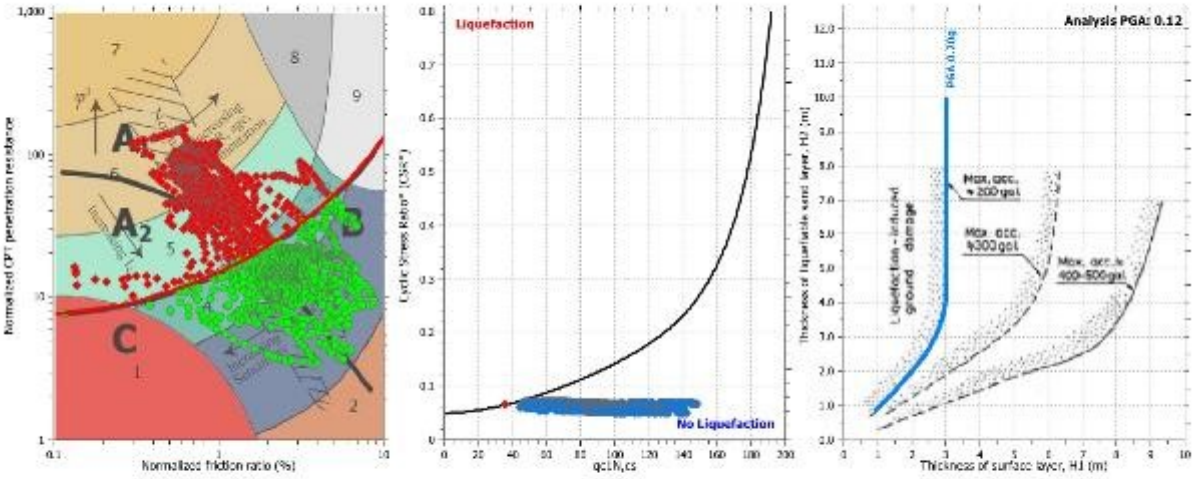
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlikely to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

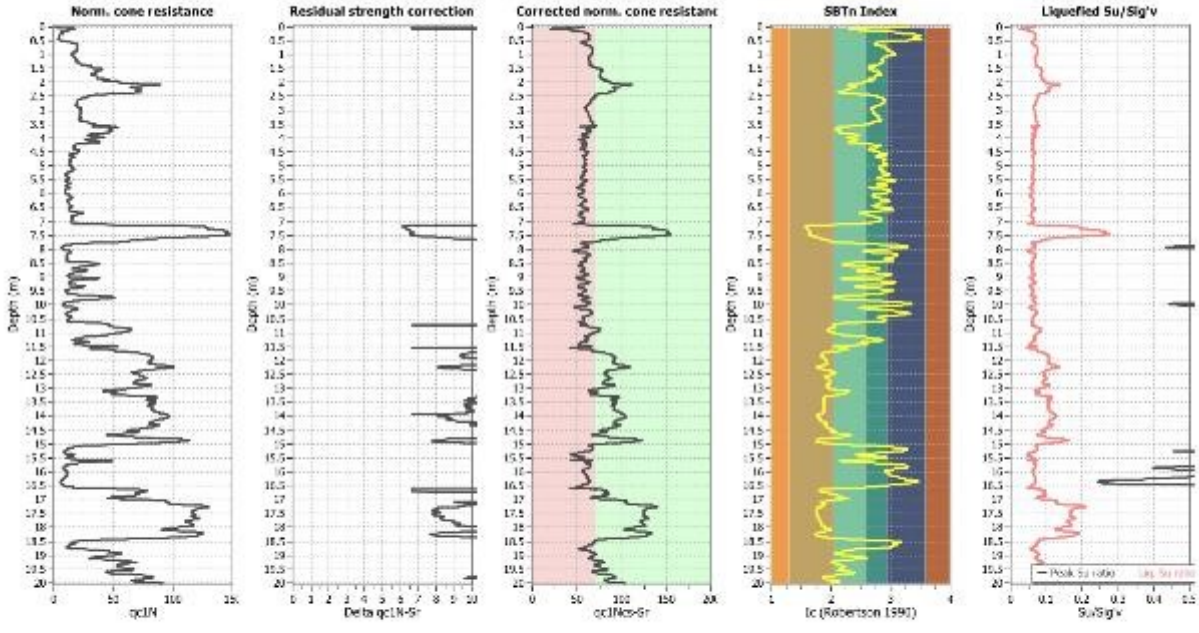
Liquefaction analysis summary plots



Input parameters and analysis data

Analysis method:	I&B (2008)	Depth to GWT (erthq.):	1.40 m	Fill weight:	N/A
Flow correction method:	RAW (1998)	Average results interval:	3	Transition layers applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w:	5.45	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.12	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.40 m	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

Analysis method:	I&B (2008)	Depth to GWT (erthq.):	1.40 m	Fill weight:	N/A
Flow correction method:	RAW (1998)	Average results interval:	3	Transition layers applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w:	5.45	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.12	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	1.40 m	Fill height:	N/A	Limit depth:	N/A

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
0.01	2.00	0.00	0.00	0.01	0.00	0.02	2.00	0.00	0.00	0.01	0.00
0.03	2.00	0.00	0.00	0.01	0.00	0.04	2.00	0.00	0.00	0.01	0.00
0.05	2.00	0.00	0.00	0.01	0.00	0.06	2.00	0.00	0.00	0.01	0.00
0.07	2.00	0.00	0.00	0.01	0.00	0.08	2.00	0.00	0.00	0.01	0.00
0.09	2.00	0.00	0.00	0.01	0.00	0.10	2.00	0.00	0.00	0.01	0.00
0.11	2.00	0.00	0.00	0.01	0.00	0.12	2.00	0.00	0.00	0.01	0.00
0.13	2.00	0.00	0.00	0.01	0.00	0.14	2.00	0.00	0.00	0.01	0.00
0.15	2.00	0.00	0.00	0.01	0.00	0.16	2.00	0.00	0.00	0.01	0.00
0.17	2.00	0.00	0.00	0.01	0.00	0.18	2.00	0.00	0.00	0.01	0.00
0.19	2.00	0.00	0.00	0.01	0.00	0.20	2.00	0.00	0.00	0.01	0.00
0.21	2.00	0.00	0.00	0.01	0.00	0.22	2.00	0.00	0.00	0.01	0.00
0.23	2.00	0.00	0.00	0.01	0.00	0.24	2.00	0.00	0.00	0.01	0.00
0.25	2.00	0.00	0.00	0.01	0.00	0.26	2.00	0.00	0.00	0.01	0.00
0.27	2.00	0.00	0.00	0.01	0.00	0.28	2.00	0.00	0.00	0.01	0.00
0.29	2.00	0.00	0.00	0.01	0.00	0.30	2.00	0.00	0.00	0.01	0.00
0.31	2.00	0.00	0.00	0.01	0.00	0.32	2.00	0.00	0.00	0.01	0.00
0.33	2.00	0.00	0.00	0.01	0.00	0.34	2.00	0.00	0.00	0.01	0.00
0.35	2.00	0.00	0.00	0.01	0.00	0.36	2.00	0.00	0.00	0.01	0.00
0.37	2.00	0.00	0.00	0.01	0.00	0.38	2.00	0.00	0.00	0.01	0.00
0.39	2.00	0.00	0.00	0.01	0.00	0.40	2.00	0.00	0.00	0.01	0.00
0.41	2.00	0.00	0.00	0.01	0.00	0.42	2.00	0.00	0.00	0.01	0.00
0.43	2.00	0.00	0.00	0.01	0.00	0.44	2.00	0.00	0.00	0.01	0.00
0.45	2.00	0.00	0.00	0.01	0.00	0.46	2.00	0.00	0.00	0.01	0.00
0.47	2.00	0.00	0.00	0.01	0.00	0.48	2.00	0.00	0.00	0.01	0.00
0.49	2.00	0.00	0.00	0.01	0.00	0.50	2.00	0.00	0.00	0.01	0.00
0.51	2.00	0.00	0.00	0.01	0.00	0.52	2.00	0.00	0.00	0.01	0.00
0.53	2.00	0.00	0.00	0.01	0.00	0.54	2.00	0.00	0.00	0.01	0.00
0.55	2.00	0.00	0.00	0.01	0.00	0.56	2.00	0.00	0.00	0.01	0.00
0.57	2.00	0.00	0.00	0.01	0.00	0.58	2.00	0.00	0.00	0.01	0.00
0.59	2.00	0.00	0.00	0.01	0.00	0.60	2.00	0.00	0.00	0.01	0.00
0.61	2.00	0.00	0.00	0.01	0.00	0.62	2.00	0.00	0.00	0.01	0.00
0.63	2.00	0.00	0.00	0.01	0.00	0.64	2.00	0.00	0.00	0.01	0.00
0.65	2.00	0.00	0.00	0.01	0.00	0.66	2.00	0.00	0.00	0.01	0.00
0.67	2.00	0.00	0.00	0.01	0.00	0.68	2.00	0.00	0.00	0.01	0.00
0.69	2.00	0.00	0.00	0.01	0.00	0.70	2.00	0.00	0.00	0.01	0.00
0.71	2.00	0.00	0.00	0.01	0.00	0.72	2.00	0.00	0.00	0.01	0.00
0.73	2.00	0.00	0.00	0.01	0.00	0.74	2.00	0.00	0.00	0.01	0.00
0.75	2.00	0.00	0.00	0.01	0.00	0.76	2.00	0.00	0.00	0.01	0.00
0.77	2.00	0.00	0.00	0.01	0.00	0.78	2.00	0.00	0.00	0.01	0.00
0.79	2.00	0.00	0.00	0.01	0.00	0.80	2.00	0.00	0.00	0.01	0.00
0.81	2.00	0.00	0.00	0.01	0.00	0.82	2.00	0.00	0.00	0.01	0.00
0.83	2.00	0.00	0.00	0.01	0.00	0.84	2.00	0.00	0.00	0.01	0.00
0.85	2.00	0.00	0.00	0.01	0.00	0.86	2.00	0.00	0.00	0.01	0.00
0.87	2.00	0.00	0.00	0.01	0.00	0.88	2.00	0.00	0.00	0.01	0.00
0.89	2.00	0.00	0.00	0.01	0.00	0.90	2.00	0.00	0.00	0.01	0.00
0.91	2.00	0.00	0.00	0.01	0.00	0.92	2.00	0.00	0.00	0.01	0.00
0.93	2.00	0.00	0.00	0.01	0.00	0.94	2.00	0.00	0.00	0.01	0.00
0.95	2.00	0.00	0.00	0.01	0.00	0.96	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
0.97	2.00	0.00	0.00	0.01	0.00	0.98	2.00	0.00	0.00	0.01	0.00
0.99	2.00	0.00	0.00	0.01	0.00	1.00	2.00	0.00	0.00	0.01	0.00
1.01	2.00	0.00	0.00	0.01	0.00	1.02	2.00	0.00	0.00	0.01	0.00
1.03	2.00	0.00	0.00	0.01	0.00	1.04	2.00	0.00	0.00	0.01	0.00
1.05	2.00	0.00	0.00	0.01	0.00	1.06	2.00	0.00	0.00	0.01	0.00
1.07	2.00	0.00	0.00	0.01	0.00	1.08	2.00	0.00	0.00	0.01	0.00
1.09	2.00	0.00	0.00	0.01	0.00	1.10	2.00	0.00	0.00	0.01	0.00
1.11	2.00	0.00	0.00	0.01	0.00	1.12	2.00	0.00	0.00	0.01	0.00
1.13	2.00	0.00	0.00	0.01	0.00	1.14	2.00	0.00	0.00	0.01	0.00
1.15	2.00	0.00	0.00	0.01	0.00	1.16	2.00	0.00	0.00	0.01	0.00
1.17	2.00	0.00	0.00	0.01	0.00	1.18	2.00	0.00	0.00	0.01	0.00
1.19	2.00	0.00	0.00	0.01	0.00	1.20	2.00	0.00	0.00	0.01	0.00
1.21	2.00	0.00	0.00	0.01	0.00	1.22	2.00	0.00	0.00	0.01	0.00
1.23	2.00	0.00	0.00	0.01	0.00	1.24	2.00	0.00	0.00	0.01	0.00
1.25	2.00	0.00	0.00	0.01	0.00	1.26	2.00	0.00	0.00	0.01	0.00
1.27	2.00	0.00	0.00	0.01	0.00	1.28	2.00	0.00	0.00	0.01	0.00
1.29	2.00	0.00	0.00	0.01	0.00	1.30	2.00	0.00	0.00	0.01	0.00
1.31	2.00	0.00	0.00	0.01	0.00	1.32	2.00	0.00	0.00	0.01	0.00
1.33	2.00	0.00	0.00	0.01	0.00	1.34	2.00	0.00	0.00	0.01	0.00
1.35	2.00	0.00	0.00	0.01	0.00	1.36	2.00	0.00	0.00	0.01	0.00
1.37	2.00	0.00	0.00	0.01	0.00	1.38	2.00	0.00	0.00	0.01	0.00
1.39	2.00	0.00	0.00	0.01	0.00	1.40	2.00	0.00	0.00	0.01	0.00
1.41	2.00	0.00	0.00	0.01	0.00	1.42	2.00	0.00	0.00	0.01	0.00
1.43	2.00	0.00	0.00	0.01	0.00	1.44	2.00	0.00	0.00	0.01	0.00
1.45	2.00	0.00	0.00	0.01	0.00	1.46	2.00	0.00	0.00	0.01	0.00
1.47	2.00	0.00	0.00	0.01	0.00	1.48	2.00	0.00	0.00	0.01	0.00
1.49	2.00	0.00	0.00	0.01	0.00	1.50	2.00	0.00	0.00	0.01	0.00
1.51	2.00	0.00	0.00	0.01	0.00	1.52	2.00	0.00	0.00	0.01	0.00
1.53	2.00	0.00	0.00	0.01	0.00	1.54	2.00	0.00	0.00	0.01	0.00
1.55	2.00	0.00	0.00	0.01	0.00	1.56	2.00	0.00	0.00	0.01	0.00
1.57	2.00	0.00	0.00	0.01	0.00	1.58	2.00	0.00	0.00	0.01	0.00
1.59	2.00	0.00	0.00	0.01	0.00	1.60	2.00	0.00	0.00	0.01	0.00
1.61	2.00	0.00	0.00	0.01	0.00	1.62	2.00	0.00	0.00	0.01	0.00
1.63	2.00	0.00	0.00	0.01	0.00	1.64	2.00	0.00	0.00	0.01	0.00
1.65	2.00	0.00	0.00	0.01	0.00	1.66	2.00	0.00	0.00	0.01	0.00
1.67	2.00	0.00	0.00	0.01	0.00	1.68	2.00	0.00	0.00	0.01	0.00
1.69	2.00	0.00	0.00	0.01	0.00	1.70	2.00	0.00	0.00	0.01	0.00
1.71	2.00	0.00	0.00	0.01	0.00	1.72	2.00	0.00	0.00	0.01	0.00
1.73	2.00	0.00	0.00	0.01	0.00	1.74	2.00	0.00	0.00	0.01	0.00
1.75	2.00	0.00	0.00	0.01	0.00	1.76	2.00	0.00	0.00	0.01	0.00
1.77	2.00	0.00	0.00	0.01	0.00	1.78	2.00	0.00	0.00	0.01	0.00
1.79	2.00	0.00	0.00	0.01	0.00	1.80	2.00	0.00	0.00	0.01	0.00
1.81	2.00	0.00	0.00	0.01	0.00	1.82	2.00	0.00	0.00	0.01	0.00
1.83	2.00	0.00	0.00	0.01	0.00	1.84	2.00	0.00	0.00	0.01	0.00
1.85	2.00	0.00	0.00	0.01	0.00	1.86	2.00	0.00	0.00	0.01	0.00
1.87	2.00	0.00	0.00	0.01	0.00	1.88	2.00	0.00	0.00	0.01	0.00
1.89	2.00	0.00	0.00	0.01	0.00	1.90	2.00	0.00	0.00	0.01	0.00
1.91	2.00	0.00	0.00	0.01	0.00	1.92	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
1.93	2.00	0.00	0.00	0.01	0.00	1.94	2.00	0.00	0.00	0.01	0.00
1.95	2.00	0.00	0.00	0.01	0.00	1.96	2.00	0.00	0.00	0.01	0.00
1.97	2.00	0.00	0.00	0.01	0.00	1.98	2.00	0.00	0.00	0.01	0.00
1.99	2.00	0.00	0.00	0.01	0.00	2.00	2.00	0.00	0.00	0.01	0.00
2.01	2.00	0.00	0.00	0.01	0.00	2.02	2.00	0.00	0.00	0.01	0.00
2.03	2.00	0.00	0.00	0.01	0.00	2.04	2.00	0.00	0.00	0.01	0.00
2.05	2.00	0.00	0.00	0.01	0.00	2.06	2.00	0.00	0.00	0.01	0.00
2.07	2.00	0.00	0.00	0.01	0.00	2.08	2.00	0.00	0.00	0.01	0.00
2.09	2.00	0.00	0.00	0.01	0.00	2.10	2.00	0.00	0.00	0.01	0.00
2.11	2.00	0.00	0.00	0.01	0.00	2.12	2.00	0.00	0.00	0.01	0.00
2.13	2.00	0.00	0.00	0.01	0.00	2.14	2.00	0.00	0.00	0.01	0.00
2.15	2.00	0.00	0.00	0.01	0.00	2.16	2.00	0.00	0.00	0.01	0.00
2.17	2.00	0.00	0.00	0.01	0.00	2.18	2.00	0.00	0.00	0.01	0.00
2.19	2.00	0.00	0.00	0.01	0.00	2.20	2.00	0.00	0.00	0.01	0.00
2.21	2.00	0.00	0.00	0.01	0.00	2.22	2.00	0.00	0.00	0.01	0.00
2.23	2.00	0.00	0.00	0.01	0.00	2.24	2.00	0.00	0.00	0.01	0.00
2.25	2.00	0.00	0.00	0.01	0.00	2.26	2.00	0.00	0.00	0.01	0.00
2.27	2.00	0.00	0.00	0.01	0.00	2.28	2.00	0.00	0.00	0.01	0.00
2.29	2.00	0.00	0.00	0.01	0.00	2.30	2.00	0.00	0.00	0.01	0.00
2.31	2.00	0.00	0.00	0.01	0.00	2.32	2.00	0.00	0.00	0.01	0.00
2.33	2.00	0.00	0.00	0.01	0.00	2.34	2.00	0.00	0.00	0.01	0.00
2.35	2.00	0.00	0.00	0.01	0.00	2.36	2.00	0.00	0.00	0.01	0.00
2.37	2.00	0.00	0.00	0.01	0.00	2.38	2.00	0.00	0.00	0.01	0.00
2.39	2.00	0.00	0.00	0.01	0.00	2.40	2.00	0.00	0.00	0.01	0.00
2.41	2.00	0.00	0.00	0.01	0.00	2.42	2.00	0.00	0.00	0.01	0.00
2.43	2.00	0.00	0.00	0.01	0.00	2.44	2.00	0.00	0.00	0.01	0.00
2.45	2.00	0.00	0.00	0.01	0.00	2.46	2.00	0.00	0.00	0.01	0.00
2.47	2.00	0.00	0.00	0.01	0.00	2.48	2.00	0.00	0.00	0.01	0.00
2.49	2.00	0.00	0.00	0.01	0.00	2.50	2.00	0.00	0.00	0.01	0.00
2.51	2.00	0.00	0.00	0.01	0.00	2.52	2.00	0.00	0.00	0.01	0.00
2.53	2.00	0.00	0.00	0.01	0.00	2.54	2.00	0.00	0.00	0.01	0.00
2.55	2.00	0.00	0.00	0.01	0.00	2.56	2.00	0.00	0.00	0.01	0.00
2.57	2.00	0.00	0.00	0.01	0.00	2.58	2.00	0.00	0.00	0.01	0.00
2.59	2.00	0.00	0.00	0.01	0.00	2.60	2.00	0.00	0.00	0.01	0.00
2.61	2.00	0.00	0.00	0.01	0.00	2.62	2.00	0.00	0.00	0.01	0.00
2.63	2.00	0.00	0.00	0.01	0.00	2.64	2.00	0.00	0.00	0.01	0.00
2.65	2.00	0.00	0.00	0.01	0.00	2.66	2.00	0.00	0.00	0.01	0.00
2.67	2.00	0.00	0.00	0.01	0.00	2.68	2.00	0.00	0.00	0.01	0.00
2.69	2.00	0.00	0.00	0.01	0.00	2.70	2.00	0.00	0.00	0.01	0.00
2.71	2.00	0.00	0.00	0.01	0.00	2.72	2.00	0.00	0.00	0.01	0.00
2.73	2.00	0.00	0.00	0.01	0.00	2.74	2.00	0.00	0.00	0.01	0.00
2.75	2.00	0.00	0.00	0.01	0.00	2.76	2.00	0.00	0.00	0.01	0.00
2.77	2.00	0.00	0.00	0.01	0.00	2.78	2.00	0.00	0.00	0.01	0.00
2.79	2.00	0.00	0.00	0.01	0.00	2.80	2.00	0.00	0.00	0.01	0.00
2.81	2.00	0.00	0.00	0.01	0.00	2.82	2.00	0.00	0.00	0.01	0.00
2.83	2.00	0.00	0.00	0.01	0.00	2.84	2.00	0.00	0.00	0.01	0.00
2.85	2.00	0.00	0.00	0.01	0.00	2.86	2.00	0.00	0.00	0.01	0.00
2.87	2.00	0.00	0.00	0.01	0.00	2.88	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
2.89	2.00	0.00	0.00	0.01	0.00	2.90	2.00	0.00	0.00	0.01	0.00
2.91	2.00	0.00	0.00	0.01	0.00	2.92	2.00	0.00	0.00	0.01	0.00
2.93	2.00	0.00	0.00	0.01	0.00	2.94	2.00	0.00	0.00	0.01	0.00
2.95	2.00	0.00	0.00	0.01	0.00	2.96	2.00	0.00	0.00	0.01	0.00
2.97	2.00	0.00	0.00	0.01	0.00	2.98	2.00	0.00	0.00	0.01	0.00
2.99	2.00	0.00	0.00	0.01	0.00	3.00	2.00	0.00	0.00	0.01	0.00
3.01	2.00	0.00	0.00	0.01	0.00	3.02	2.00	0.00	0.00	0.01	0.00
3.03	2.00	0.00	0.00	0.01	0.00	3.04	2.00	0.00	0.00	0.01	0.00
3.05	2.00	0.00	0.00	0.01	0.00	3.06	2.00	0.00	0.00	0.01	0.00
3.07	2.00	0.00	0.00	0.01	0.00	3.08	2.00	0.00	0.00	0.01	0.00
3.09	2.00	0.00	0.00	0.01	0.00	3.10	2.00	0.00	0.00	0.01	0.00
3.11	2.00	0.00	0.00	0.01	0.00	3.12	2.00	0.00	0.00	0.01	0.00
3.13	2.00	0.00	0.00	0.01	0.00	3.14	2.00	0.00	0.00	0.01	0.00
3.15	2.00	0.00	0.00	0.01	0.00	3.16	2.00	0.00	0.00	0.01	0.00
3.17	2.00	0.00	0.00	0.01	0.00	3.18	2.00	0.00	0.00	0.01	0.00
3.19	2.00	0.00	0.00	0.01	0.00	3.20	2.00	0.00	0.00	0.01	0.00
3.21	2.00	0.00	0.00	0.01	0.00	3.22	2.00	0.00	0.00	0.01	0.00
3.23	2.00	0.00	0.00	0.01	0.00	3.24	2.00	0.00	0.00	0.01	0.00
3.25	2.00	0.00	0.00	0.01	0.00	3.26	2.00	0.00	0.00	0.01	0.00
3.27	2.00	0.00	0.00	0.01	0.00	3.28	2.00	0.00	0.00	0.01	0.00
3.29	2.00	0.00	0.00	0.01	0.00	3.30	2.00	0.00	0.00	0.01	0.00
3.31	2.00	0.00	0.00	0.01	0.00	3.32	2.00	0.00	0.00	0.01	0.00
3.33	2.00	0.00	0.00	0.01	0.00	3.34	2.00	0.00	0.00	0.01	0.00
3.35	2.00	0.00	0.00	0.01	0.00	3.36	2.00	0.00	0.00	0.01	0.00
3.37	2.00	0.00	0.00	0.01	0.00	3.38	2.00	0.00	0.00	0.01	0.00
3.39	2.00	0.00	0.00	0.01	0.00	3.40	2.00	0.00	0.00	0.01	0.00
3.41	2.00	0.00	0.00	0.01	0.00	3.42	2.00	0.00	0.00	0.01	0.00
3.43	2.00	0.00	0.00	0.01	0.00	3.44	2.00	0.00	0.00	0.01	0.00
3.45	2.00	0.00	0.00	0.01	0.00	3.46	2.00	0.00	0.00	0.01	0.00
3.47	2.00	0.00	0.00	0.01	0.00	3.48	2.00	0.00	0.00	0.01	0.00
3.49	2.00	0.00	0.00	0.01	0.00	3.50	2.00	0.00	0.00	0.01	0.00
3.51	2.00	0.00	0.00	0.01	0.00	3.52	2.00	0.00	0.00	0.01	0.00
3.53	1.75	0.00	0.00	0.01	0.00	3.54	1.84	0.00	0.00	0.01	0.00
3.55	1.89	0.00	0.00	0.01	0.00	3.56	1.94	0.00	0.00	0.01	0.00
3.57	2.00	0.00	0.00	0.01	0.00	3.58	1.57	0.00	0.00	0.01	0.00
3.59	2.00	0.00	0.00	0.01	0.00	3.60	1.96	0.00	0.00	0.01	0.00
3.61	1.94	0.00	0.00	0.01	0.00	3.62	1.95	0.00	0.00	0.01	0.00
3.63	1.88	0.00	0.00	0.01	0.00	3.64	1.80	0.00	0.00	0.01	0.00
3.65	1.76	0.00	0.00	0.01	0.00	3.66	1.73	0.00	0.00	0.01	0.00
3.67	1.68	0.00	0.00	0.01	0.00	3.68	1.66	0.00	0.00	0.01	0.00
3.69	1.68	0.00	0.00	0.01	0.00	3.70	1.71	0.00	0.00	0.01	0.00
3.71	1.75	0.00	0.00	0.01	0.00	3.72	1.80	0.00	0.00	0.01	0.00
3.73	1.82	0.00	0.00	0.01	0.00	3.74	1.85	0.00	0.00	0.01	0.00
3.75	1.86	0.00	0.00	0.01	0.00	3.76	1.87	0.00	0.00	0.01	0.00
3.77	1.86	0.00	0.00	0.01	0.00	3.78	1.83	0.00	0.00	0.01	0.00
3.79	1.81	0.00	0.00	0.01	0.00	3.80	1.79	0.00	0.00	0.01	0.00
3.81	1.73	0.00	0.00	0.01	0.00	3.82	1.70	0.00	0.00	0.01	0.00
3.83	1.69	0.00	0.00	0.01	0.00	3.84	1.63	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
3.85	1.61	0.00	0.00	0.01	0.00	3.86	1.57	0.00	0.00	0.01	0.00
3.87	1.51	0.00	0.00	0.01	0.00	3.88	1.50	0.00	0.00	0.01	0.00
3.89	1.49	0.00	0.00	0.01	0.00	3.90	1.50	0.00	0.00	0.01	0.00
3.91	1.51	0.00	0.00	0.01	0.00	3.92	1.57	0.00	0.00	0.01	0.00
3.93	1.61	0.00	0.00	0.01	0.00	3.94	1.66	0.00	0.00	0.01	0.00
3.95	1.75	0.00	0.00	0.01	0.00	3.96	1.76	0.00	0.00	0.01	0.00
3.97	1.77	0.00	0.00	0.01	0.00	3.98	1.76	0.00	0.00	0.01	0.00
3.99	1.72	0.00	0.00	0.01	0.00	4.00	1.64	0.00	0.00	0.01	0.00
4.01	1.59	0.00	0.00	0.01	0.00	4.02	1.55	0.00	0.00	0.01	0.00
4.03	1.51	0.00	0.00	0.01	0.00	4.04	1.45	0.00	0.00	0.01	0.00
4.05	1.43	0.00	0.00	0.01	0.00	4.06	1.41	0.00	0.00	0.01	0.00
4.07	1.45	0.00	0.00	0.01	0.00	4.08	1.52	0.00	0.00	0.01	0.00
4.09	1.61	0.00	0.00	0.01	0.00	4.10	1.62	0.00	0.00	0.01	0.00
4.11	1.60	0.00	0.00	0.01	0.00	4.12	1.57	0.00	0.00	0.01	0.00
4.13	1.58	0.00	0.00	0.01	0.00	4.14	1.63	0.00	0.00	0.01	0.00
4.15	1.65	0.00	0.00	0.01	0.00	4.16	1.67	0.00	0.00	0.01	0.00
4.17	1.60	0.00	0.00	0.01	0.00	4.18	1.57	0.00	0.00	0.01	0.00
4.19	1.51	0.00	0.00	0.01	0.00	4.20	1.46	0.00	0.00	0.01	0.00
4.21	1.36	0.00	0.00	0.01	0.00	4.22	2.00	0.00	0.00	0.01	0.00
4.23	2.00	0.00	0.00	0.01	0.00	4.24	2.00	0.00	0.00	0.01	0.00
4.25	2.00	0.00	0.00	0.01	0.00	4.26	2.00	0.00	0.00	0.01	0.00
4.27	2.00	0.00	0.00	0.01	0.00	4.28	2.00	0.00	0.00	0.01	0.00
4.29	2.00	0.00	0.00	0.01	0.00	4.30	2.00	0.00	0.00	0.01	0.00
4.31	2.00	0.00	0.00	0.01	0.00	4.32	2.00	0.00	0.00	0.01	0.00
4.33	2.00	0.00	0.00	0.01	0.00	4.34	2.00	0.00	0.00	0.01	0.00
4.35	2.00	0.00	0.00	0.01	0.00	4.36	2.00	0.00	0.00	0.01	0.00
4.37	2.00	0.00	0.00	0.01	0.00	4.38	2.00	0.00	0.00	0.01	0.00
4.39	2.00	0.00	0.00	0.01	0.00	4.40	2.00	0.00	0.00	0.01	0.00
4.41	2.00	0.00	0.00	0.01	0.00	4.42	2.00	0.00	0.00	0.01	0.00
4.43	2.00	0.00	0.00	0.01	0.00	4.44	2.00	0.00	0.00	0.01	0.00
4.45	2.00	0.00	0.00	0.01	0.00	4.46	2.00	0.00	0.00	0.01	0.00
4.47	2.00	0.00	0.00	0.01	0.00	4.48	2.00	0.00	0.00	0.01	0.00
4.49	2.00	0.00	0.00	0.01	0.00	4.50	2.00	0.00	0.00	0.01	0.00
4.51	2.00	0.00	0.00	0.01	0.00	4.52	2.00	0.00	0.00	0.01	0.00
4.53	2.00	0.00	0.00	0.01	0.00	4.54	2.00	0.00	0.00	0.01	0.00
4.55	2.00	0.00	0.00	0.01	0.00	4.56	2.00	0.00	0.00	0.01	0.00
4.57	2.00	0.00	0.00	0.01	0.00	4.58	2.00	0.00	0.00	0.01	0.00
4.59	2.00	0.00	0.00	0.01	0.00	4.60	2.00	0.00	0.00	0.01	0.00
4.61	2.00	0.00	0.00	0.01	0.00	4.62	2.00	0.00	0.00	0.01	0.00
4.63	2.00	0.00	0.00	0.01	0.00	4.64	2.00	0.00	0.00	0.01	0.00
4.65	2.00	0.00	0.00	0.01	0.00	4.66	2.00	0.00	0.00	0.01	0.00
4.67	2.00	0.00	0.00	0.01	0.00	4.68	2.00	0.00	0.00	0.01	0.00
4.69	2.00	0.00	0.00	0.01	0.00	4.70	2.00	0.00	0.00	0.01	0.00
4.71	2.00	0.00	0.00	0.01	0.00	4.72	2.00	0.00	0.00	0.01	0.00
4.73	2.00	0.00	0.00	0.01	0.00	4.74	2.00	0.00	0.00	0.01	0.00
4.75	2.00	0.00	0.00	0.01	0.00	4.76	2.00	0.00	0.00	0.01	0.00
4.77	2.00	0.00	0.00	0.01	0.00	4.78	2.00	0.00	0.00	0.01	0.00
4.79	2.00	0.00	0.00	0.01	0.00	4.80	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
4.81	2.00	0.00	0.00	0.01	0.00	4.82	2.00	0.00	0.00	0.01	0.00
4.83	2.00	0.00	0.00	0.01	0.00	4.84	2.00	0.00	0.00	0.01	0.00
4.85	2.00	0.00	0.00	0.01	0.00	4.86	2.00	0.00	0.00	0.01	0.00
4.87	2.00	0.00	0.00	0.01	0.00	4.88	2.00	0.00	0.00	0.01	0.00
4.89	2.00	0.00	0.00	0.01	0.00	4.90	2.00	0.00	0.00	0.01	0.00
4.91	2.00	0.00	0.00	0.01	0.00	4.92	2.00	0.00	0.00	0.01	0.00
4.93	2.00	0.00	0.00	0.01	0.00	4.94	2.00	0.00	0.00	0.01	0.00
4.95	2.00	0.00	0.00	0.01	0.00	4.96	2.00	0.00	0.00	0.01	0.00
4.97	2.00	0.00	0.00	0.01	0.00	4.98	2.00	0.00	0.00	0.01	0.00
4.99	2.00	0.00	0.00	0.01	0.00	5.00	2.00	0.00	0.00	0.01	0.00
5.01	2.00	0.00	0.00	0.01	0.00	5.02	2.00	0.00	0.00	0.01	0.00
5.03	2.00	0.00	0.00	0.01	0.00	5.04	2.00	0.00	0.00	0.01	0.00
5.05	2.00	0.00	0.00	0.01	0.00	5.06	2.00	0.00	0.00	0.01	0.00
5.07	2.00	0.00	0.00	0.01	0.00	5.08	2.00	0.00	0.00	0.01	0.00
5.09	2.00	0.00	0.00	0.01	0.00	5.10	2.00	0.00	0.00	0.01	0.00
5.11	2.00	0.00	0.00	0.01	0.00	5.12	2.00	0.00	0.00	0.01	0.00
5.13	2.00	0.00	0.00	0.01	0.00	5.14	2.00	0.00	0.00	0.01	0.00
5.15	2.00	0.00	0.00	0.01	0.00	5.16	2.00	0.00	0.00	0.01	0.00
5.17	2.00	0.00	0.00	0.01	0.00	5.18	2.00	0.00	0.00	0.01	0.00
5.19	2.00	0.00	0.00	0.01	0.00	5.20	2.00	0.00	0.00	0.01	0.00
5.21	2.00	0.00	0.00	0.01	0.00	5.22	2.00	0.00	0.00	0.01	0.00
5.23	2.00	0.00	0.00	0.01	0.00	5.24	2.00	0.00	0.00	0.01	0.00
5.25	2.00	0.00	0.00	0.01	0.00	5.26	2.00	0.00	0.00	0.01	0.00
5.27	2.00	0.00	0.00	0.01	0.00	5.28	2.00	0.00	0.00	0.01	0.00
5.29	2.00	0.00	0.00	0.01	0.00	5.30	2.00	0.00	0.00	0.01	0.00
5.31	2.00	0.00	0.00	0.01	0.00	5.32	2.00	0.00	0.00	0.01	0.00
5.33	2.00	0.00	0.00	0.01	0.00	5.34	2.00	0.00	0.00	0.01	0.00
5.35	2.00	0.00	0.00	0.01	0.00	5.36	2.00	0.00	0.00	0.01	0.00
5.37	2.00	0.00	0.00	0.01	0.00	5.38	2.00	0.00	0.00	0.01	0.00
5.39	2.00	0.00	0.00	0.01	0.00	5.40	2.00	0.00	0.00	0.01	0.00
5.41	2.00	0.00	0.00	0.01	0.00	5.42	2.00	0.00	0.00	0.01	0.00
5.43	2.00	0.00	0.00	0.01	0.00	5.44	2.00	0.00	0.00	0.01	0.00
5.45	2.00	0.00	0.00	0.01	0.00	5.46	2.00	0.00	0.00	0.01	0.00
5.47	2.00	0.00	0.00	0.01	0.00	5.48	2.00	0.00	0.00	0.01	0.00
5.49	2.00	0.00	0.00	0.01	0.00	5.50	2.00	0.00	0.00	0.01	0.00
5.51	2.00	0.00	0.00	0.01	0.00	5.52	2.00	0.00	0.00	0.01	0.00
5.53	2.00	0.00	0.00	0.01	0.00	5.54	2.00	0.00	0.00	0.01	0.00
5.55	2.00	0.00	0.00	0.01	0.00	5.56	2.00	0.00	0.00	0.01	0.00
5.57	2.00	0.00	0.00	0.01	0.00	5.58	2.00	0.00	0.00	0.01	0.00
5.59	2.00	0.00	0.00	0.01	0.00	5.60	2.00	0.00	0.00	0.01	0.00
5.61	2.00	0.00	0.00	0.01	0.00	5.62	2.00	0.00	0.00	0.01	0.00
5.63	2.00	0.00	0.00	0.01	0.00	5.64	2.00	0.00	0.00	0.01	0.00
5.65	2.00	0.00	0.00	0.01	0.00	5.66	2.00	0.00	0.00	0.01	0.00
5.67	2.00	0.00	0.00	0.01	0.00	5.68	2.00	0.00	0.00	0.01	0.00
5.69	2.00	0.00	0.00	0.01	0.00	5.70	2.00	0.00	0.00	0.01	0.00
5.71	2.00	0.00	0.00	0.01	0.00	5.72	2.00	0.00	0.00	0.01	0.00
5.73	2.00	0.00	0.00	0.01	0.00	5.74	2.00	0.00	0.00	0.01	0.00
5.75	2.00	0.00	0.00	0.01	0.00	5.76	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
5.77	2.00	0.00	0.00	0.01	0.00	5.78	2.00	0.00	0.00	0.01	0.00
5.79	2.00	0.00	0.00	0.01	0.00	5.80	2.00	0.00	0.00	0.01	0.00
5.81	2.00	0.00	0.00	0.01	0.00	5.82	2.00	0.00	0.00	0.01	0.00
5.83	2.00	0.00	0.00	0.01	0.00	5.84	2.00	0.00	0.00	0.01	0.00
5.85	2.00	0.00	0.00	0.01	0.00	5.86	2.00	0.00	0.00	0.01	0.00
5.87	2.00	0.00	0.00	0.01	0.00	5.88	2.00	0.00	0.00	0.01	0.00
5.89	2.00	0.00	0.00	0.01	0.00	5.90	2.00	0.00	0.00	0.01	0.00
5.91	2.00	0.00	0.00	0.01	0.00	5.92	2.00	0.00	0.00	0.01	0.00
5.93	2.00	0.00	0.00	0.01	0.00	5.94	2.00	0.00	0.00	0.01	0.00
5.95	2.00	0.00	0.00	0.01	0.00	5.96	2.00	0.00	0.00	0.01	0.00
5.97	2.00	0.00	0.00	0.01	0.00	5.98	2.00	0.00	0.00	0.01	0.00
5.99	2.00	0.00	0.00	0.01	0.00	6.00	2.00	0.00	0.00	0.01	0.00
6.01	2.00	0.00	0.00	0.01	0.00	6.02	2.00	0.00	0.00	0.01	0.00
6.03	2.00	0.00	0.00	0.01	0.00	6.04	2.00	0.00	0.00	0.01	0.00
6.05	2.00	0.00	0.00	0.01	0.00	6.06	2.00	0.00	0.00	0.01	0.00
6.07	2.00	0.00	0.00	0.01	0.00	6.08	2.00	0.00	0.00	0.01	0.00
6.09	2.00	0.00	0.00	0.01	0.00	6.10	2.00	0.00	0.00	0.01	0.00
6.11	2.00	0.00	0.00	0.01	0.00	6.12	2.00	0.00	0.00	0.01	0.00
6.13	2.00	0.00	0.00	0.01	0.00	6.14	2.00	0.00	0.00	0.01	0.00
6.15	2.00	0.00	0.00	0.01	0.00	6.16	2.00	0.00	0.00	0.01	0.00
6.17	2.00	0.00	0.00	0.01	0.00	6.18	2.00	0.00	0.00	0.01	0.00
6.19	2.00	0.00	0.00	0.01	0.00	6.20	2.00	0.00	0.00	0.01	0.00
6.21	2.00	0.00	0.00	0.01	0.00	6.22	2.00	0.00	0.00	0.01	0.00
6.23	2.00	0.00	0.00	0.01	0.00	6.24	2.00	0.00	0.00	0.01	0.00
6.25	2.00	0.00	0.00	0.01	0.00	6.26	2.00	0.00	0.00	0.01	0.00
6.27	2.00	0.00	0.00	0.01	0.00	6.28	2.00	0.00	0.00	0.01	0.00
6.29	2.00	0.00	0.00	0.01	0.00	6.30	2.00	0.00	0.00	0.01	0.00
6.31	2.00	0.00	0.00	0.01	0.00	6.32	2.00	0.00	0.00	0.01	0.00
6.33	2.00	0.00	0.00	0.01	0.00	6.34	2.00	0.00	0.00	0.01	0.00
6.35	2.00	0.00	0.00	0.01	0.00	6.36	2.00	0.00	0.00	0.01	0.00
6.37	2.00	0.00	0.00	0.01	0.00	6.38	2.00	0.00	0.00	0.01	0.00
6.39	2.00	0.00	0.00	0.01	0.00	6.40	2.00	0.00	0.00	0.01	0.00
6.41	2.00	0.00	0.00	0.01	0.00	6.42	2.00	0.00	0.00	0.01	0.00
6.43	2.00	0.00	0.00	0.01	0.00	6.44	2.00	0.00	0.00	0.01	0.00
6.45	2.00	0.00	0.00	0.01	0.00	6.46	2.00	0.00	0.00	0.01	0.00
6.47	2.00	0.00	0.00	0.01	0.00	6.48	2.00	0.00	0.00	0.01	0.00
6.49	2.00	0.00	0.00	0.01	0.00	6.50	2.00	0.00	0.00	0.01	0.00
6.51	2.00	0.00	0.00	0.01	0.00	6.52	2.00	0.00	0.00	0.01	0.00
6.53	2.00	0.00	0.00	0.01	0.00	6.54	2.00	0.00	0.00	0.01	0.00
6.55	2.00	0.00	0.00	0.01	0.00	6.56	2.00	0.00	0.00	0.01	0.00
6.57	2.00	0.00	0.00	0.01	0.00	6.58	2.00	0.00	0.00	0.01	0.00
6.59	2.00	0.00	0.00	0.01	0.00	6.60	2.00	0.00	0.00	0.01	0.00
6.61	2.00	0.00	0.00	0.01	0.00	6.62	2.00	0.00	0.00	0.01	0.00
6.63	2.00	0.00	0.00	0.01	0.00	6.64	2.00	0.00	0.00	0.01	0.00
6.65	2.00	0.00	0.00	0.01	0.00	6.66	1.19	0.00	0.00	0.01	0.00
6.67	1.22	0.00	0.00	0.01	0.00	6.68	1.27	0.00	0.00	0.01	0.00
6.69	1.28	0.00	0.00	0.01	0.00	6.70	1.28	0.00	0.00	0.01	0.00
6.71	1.27	0.00	0.00	0.01	0.00	6.72	1.26	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
6.73	1.22	0.00	0.00	0.01	0.00	6.74	2.00	0.00	0.00	0.01	0.00
6.75	2.00	0.00	0.00	0.01	0.00	6.76	2.00	0.00	0.00	0.01	0.00
6.77	2.00	0.00	0.00	0.01	0.00	6.78	2.00	0.00	0.00	0.01	0.00
6.79	2.00	0.00	0.00	0.01	0.00	6.80	2.00	0.00	0.00	0.01	0.00
6.81	2.00	0.00	0.00	0.01	0.00	6.82	2.00	0.00	0.00	0.01	0.00
6.83	2.00	0.00	0.00	0.01	0.00	6.84	2.00	0.00	0.00	0.01	0.00
6.85	2.00	0.00	0.00	0.01	0.00	6.86	2.00	0.00	0.00	0.01	0.00
6.87	2.00	0.00	0.00	0.01	0.00	6.88	2.00	0.00	0.00	0.01	0.00
6.89	2.00	0.00	0.00	0.01	0.00	6.90	2.00	0.00	0.00	0.01	0.00
6.91	2.00	0.00	0.00	0.01	0.00	6.92	2.00	0.00	0.00	0.01	0.00
6.93	2.00	0.00	0.00	0.01	0.00	6.94	2.00	0.00	0.00	0.01	0.00
6.95	2.00	0.00	0.00	0.01	0.00	6.96	2.00	0.00	0.00	0.01	0.00
6.97	2.00	0.00	0.00	0.01	0.00	6.98	2.00	0.00	0.00	0.01	0.00
6.99	2.00	0.00	0.00	0.01	0.00	7.00	2.00	0.00	0.00	0.01	0.00
7.01	2.00	0.00	0.00	0.01	0.00	7.02	2.00	0.00	0.00	0.01	0.00
7.03	2.00	0.00	0.00	0.01	0.00	7.04	2.00	0.00	0.00	0.01	0.00
7.05	1.12	0.00	0.00	0.01	0.00	7.06	1.16	0.00	0.00	0.01	0.00
7.07	1.16	0.00	0.00	0.01	0.00	7.08	1.15	0.00	0.00	0.01	0.00
7.09	1.14	0.00	0.00	0.01	0.00	7.10	1.17	0.00	0.00	0.01	0.00
7.11	1.43	0.00	0.00	0.01	0.00	7.12	1.45	0.00	0.00	0.01	0.00
7.13	1.85	0.00	0.00	0.01	0.00	7.14	1.97	0.00	0.00	0.01	0.00
7.15	2.00	0.00	0.00	0.01	0.00	7.16	2.00	0.00	0.00	0.01	0.00
7.17	2.00	0.00	0.00	0.01	0.00	7.18	2.00	0.00	0.00	0.01	0.00
7.19	2.00	0.00	0.00	0.01	0.00	7.20	2.00	0.00	0.00	0.01	0.00
7.21	2.00	0.00	0.00	0.01	0.00	7.22	2.00	0.00	0.00	0.01	0.00
7.23	2.00	0.00	0.00	0.01	0.00	7.24	2.00	0.00	0.00	0.01	0.00
7.25	2.00	0.00	0.00	0.01	0.00	7.26	2.00	0.00	0.00	0.01	0.00
7.27	2.00	0.00	0.00	0.01	0.00	7.28	2.00	0.00	0.00	0.01	0.00
7.29	2.00	0.00	0.00	0.01	0.00	7.30	2.00	0.00	0.00	0.01	0.00
7.31	2.00	0.00	0.00	0.01	0.00	7.32	2.00	0.00	0.00	0.01	0.00
7.33	2.00	0.00	0.00	0.01	0.00	7.34	2.00	0.00	0.00	0.01	0.00
7.35	2.00	0.00	0.00	0.01	0.00	7.36	2.00	0.00	0.00	0.01	0.00
7.37	2.00	0.00	0.00	0.01	0.00	7.38	2.00	0.00	0.00	0.01	0.00
7.39	2.00	0.00	0.00	0.01	0.00	7.40	2.00	0.00	0.00	0.01	0.00
7.41	2.00	0.00	0.00	0.01	0.00	7.42	2.00	0.00	0.00	0.01	0.00
7.43	2.00	0.00	0.00	0.01	0.00	7.44	2.00	0.00	0.00	0.01	0.00
7.45	2.00	0.00	0.00	0.01	0.00	7.46	2.00	0.00	0.00	0.01	0.00
7.47	2.00	0.00	0.00	0.01	0.00	7.48	2.00	0.00	0.00	0.01	0.00
7.49	2.00	0.00	0.00	0.01	0.00	7.50	2.00	0.00	0.00	0.01	0.00
7.51	2.00	0.00	0.00	0.01	0.00	7.52	2.00	0.00	0.00	0.01	0.00
7.53	2.00	0.00	0.00	0.01	0.00	7.54	2.00	0.00	0.00	0.01	0.00
7.55	2.00	0.00	0.00	0.01	0.00	7.56	2.00	0.00	0.00	0.01	0.00
7.57	2.00	0.00	0.00	0.01	0.00	7.58	2.00	0.00	0.00	0.01	0.00
7.59	2.00	0.00	0.00	0.01	0.00	7.60	2.00	0.00	0.00	0.01	0.00
7.61	1.95	0.00	0.00	0.01	0.00	7.62	1.89	0.00	0.00	0.01	0.00
7.63	1.87	0.00	0.00	0.01	0.00	7.64	1.83	0.00	0.00	0.01	0.00
7.65	1.82	0.00	0.00	0.01	0.00	7.66	1.81	0.00	0.00	0.01	0.00
7.67	1.77	0.00	0.00	0.01	0.00	7.68	1.77	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
7.69	1.72	0.00	0.00	0.01	0.00	7.70	1.71	0.00	0.00	0.01	0.00
7.71	1.69	0.00	0.00	0.01	0.00	7.72	1.69	0.00	0.00	0.01	0.00
7.73	1.64	0.00	0.00	0.01	0.00	7.74	1.62	0.00	0.00	0.01	0.00
7.75	1.61	0.00	0.00	0.01	0.00	7.76	1.50	0.00	0.00	0.01	0.00
7.77	1.39	0.00	0.00	0.01	0.00	7.78	1.35	0.00	0.00	0.01	0.00
7.79	1.28	0.00	0.00	0.01	0.00	7.80	1.24	0.00	0.00	0.01	0.00
7.81	2.00	0.00	0.00	0.01	0.00	7.82	2.00	0.00	0.00	0.01	0.00
7.83	2.00	0.00	0.00	0.01	0.00	7.84	2.00	0.00	0.00	0.01	0.00
7.85	2.00	0.00	0.00	0.01	0.00	7.86	2.00	0.00	0.00	0.01	0.00
7.87	2.00	0.00	0.00	0.01	0.00	7.88	2.00	0.00	0.00	0.01	0.00
7.89	2.00	0.00	0.00	0.01	0.00	7.90	2.00	0.00	0.00	0.01	0.00
7.91	2.00	0.00	0.00	0.01	0.00	7.92	2.00	0.00	0.00	0.01	0.00
7.93	2.00	0.00	0.00	0.01	0.00	7.94	2.00	0.00	0.00	0.01	0.00
7.95	2.00	0.00	0.00	0.01	0.00	7.96	2.00	0.00	0.00	0.01	0.00
7.97	2.00	0.00	0.00	0.01	0.00	7.98	2.00	0.00	0.00	0.01	0.00
7.99	2.00	0.00	0.00	0.01	0.00	8.00	2.00	0.00	0.00	0.01	0.00
8.01	2.00	0.00	0.00	0.01	0.00	8.02	2.00	0.00	0.00	0.01	0.00
8.03	2.00	0.00	0.00	0.01	0.00	8.04	2.00	0.00	0.00	0.01	0.00
8.05	2.00	0.00	0.00	0.01	0.00	8.06	1.07	0.00	0.00	0.01	0.00
8.07	1.09	0.00	0.00	0.01	0.00	8.08	1.09	0.00	0.00	0.01	0.00
8.09	2.00	0.00	0.00	0.01	0.00	8.10	2.00	0.00	0.00	0.01	0.00
8.11	2.00	0.00	0.00	0.01	0.00	8.12	2.00	0.00	0.00	0.01	0.00
8.13	2.00	0.00	0.00	0.01	0.00	8.14	2.00	0.00	0.00	0.01	0.00
8.15	2.00	0.00	0.00	0.01	0.00	8.16	2.00	0.00	0.00	0.01	0.00
8.17	2.00	0.00	0.00	0.01	0.00	8.18	2.00	0.00	0.00	0.01	0.00
8.19	2.00	0.00	0.00	0.01	0.00	8.20	2.00	0.00	0.00	0.01	0.00
8.21	2.00	0.00	0.00	0.01	0.00	8.22	2.00	0.00	0.00	0.01	0.00
8.23	2.00	0.00	0.00	0.01	0.00	8.24	2.00	0.00	0.00	0.01	0.00
8.25	2.00	0.00	0.00	0.01	0.00	8.26	2.00	0.00	0.00	0.01	0.00
8.27	2.00	0.00	0.00	0.01	0.00	8.28	2.00	0.00	0.00	0.01	0.00
8.29	2.00	0.00	0.00	0.01	0.00	8.30	2.00	0.00	0.00	0.01	0.00
8.31	2.00	0.00	0.00	0.01	0.00	8.32	2.00	0.00	0.00	0.01	0.00
8.33	2.00	0.00	0.00	0.01	0.00	8.34	2.00	0.00	0.00	0.01	0.00
8.35	2.00	0.00	0.00	0.01	0.00	8.36	2.00	0.00	0.00	0.01	0.00
8.37	2.00	0.00	0.00	0.01	0.00	8.38	2.00	0.00	0.00	0.01	0.00
8.39	2.00	0.00	0.00	0.01	0.00	8.40	2.00	0.00	0.00	0.01	0.00
8.41	2.00	0.00	0.00	0.01	0.00	8.42	2.00	0.00	0.00	0.01	0.00
8.43	2.00	0.00	0.00	0.01	0.00	8.44	2.00	0.00	0.00	0.01	0.00
8.45	2.00	0.00	0.00	0.01	0.00	8.46	1.27	0.00	0.00	0.01	0.00
8.47	1.32	0.00	0.00	0.01	0.00	8.48	1.41	0.00	0.00	0.01	0.00
8.49	1.43	0.00	0.00	0.01	0.00	8.50	1.45	0.00	0.00	0.01	0.00
8.51	1.46	0.00	0.00	0.01	0.00	8.52	1.46	0.00	0.00	0.01	0.00
8.53	1.46	0.00	0.00	0.01	0.00	8.54	1.43	0.00	0.00	0.01	0.00
8.55	1.41	0.00	0.00	0.01	0.00	8.56	1.39	0.00	0.00	0.01	0.00
8.57	1.37	0.00	0.00	0.01	0.00	8.58	1.34	0.00	0.00	0.01	0.00
8.59	1.35	0.00	0.00	0.01	0.00	8.60	1.39	0.00	0.00	0.01	0.00
8.61	1.31	0.00	0.00	0.01	0.00	8.62	1.32	0.00	0.00	0.01	0.00
8.63	1.26	0.00	0.00	0.01	0.00	8.64	1.24	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
8.65	2.00	0.00	0.00	0.01	0.00	8.66	2.00	0.00	0.00	0.01	0.00
8.67	2.00	0.00	0.00	0.01	0.00	8.68	2.00	0.00	0.00	0.01	0.00
8.69	2.00	0.00	0.00	0.01	0.00	8.70	2.00	0.00	0.00	0.01	0.00
8.71	2.00	0.00	0.00	0.01	0.00	8.72	2.00	0.00	0.00	0.01	0.00
8.73	1.26	0.00	0.00	0.01	0.00	8.74	1.33	0.00	0.00	0.01	0.00
8.75	1.34	0.00	0.00	0.01	0.00	8.76	1.35	0.00	0.00	0.01	0.00
8.77	1.33	0.00	0.00	0.01	0.00	8.78	1.32	0.00	0.00	0.01	0.00
8.79	1.31	0.00	0.00	0.01	0.00	8.80	1.29	0.00	0.00	0.01	0.00
8.81	1.25	0.00	0.00	0.01	0.00	8.82	1.23	0.00	0.00	0.01	0.00
8.83	2.00	0.00	0.00	0.01	0.00	8.84	2.00	0.00	0.00	0.01	0.00
8.85	2.00	0.00	0.00	0.01	0.00	8.86	2.00	0.00	0.00	0.01	0.00
8.87	2.00	0.00	0.00	0.01	0.00	8.88	2.00	0.00	0.00	0.01	0.00
8.89	2.00	0.00	0.00	0.01	0.00	8.90	2.00	0.00	0.00	0.01	0.00
8.91	2.00	0.00	0.00	0.01	0.00	8.92	2.00	0.00	0.00	0.01	0.00
8.93	2.00	0.00	0.00	0.01	0.00	8.94	2.00	0.00	0.00	0.01	0.00
8.95	2.00	0.00	0.00	0.01	0.00	8.96	2.00	0.00	0.00	0.01	0.00
8.97	2.00	0.00	0.00	0.01	0.00	8.98	2.00	0.00	0.00	0.01	0.00
8.99	2.00	0.00	0.00	0.01	0.00	9.00	2.00	0.00	0.00	0.01	0.00
9.01	1.25	0.00	0.00	0.01	0.00	9.02	1.33	0.00	0.00	0.01	0.00
9.03	1.28	0.00	0.00	0.01	0.00	9.04	1.45	0.00	0.00	0.01	0.00
9.05	1.45	0.00	0.00	0.01	0.00	9.06	1.41	0.00	0.00	0.01	0.00
9.07	1.38	0.00	0.00	0.01	0.00	9.08	1.34	0.00	0.00	0.01	0.00
9.09	1.29	0.00	0.00	0.01	0.00	9.10	1.20	0.00	0.00	0.01	0.00
9.11	2.00	0.00	0.00	0.01	0.00	9.12	2.00	0.00	0.00	0.01	0.00
9.13	2.00	0.00	0.00	0.01	0.00	9.14	2.00	0.00	0.00	0.01	0.00
9.15	2.00	0.00	0.00	0.01	0.00	9.16	2.00	0.00	0.00	0.01	0.00
9.17	2.00	0.00	0.00	0.01	0.00	9.18	2.00	0.00	0.00	0.01	0.00
9.19	2.00	0.00	0.00	0.01	0.00	9.20	2.00	0.00	0.00	0.01	0.00
9.21	2.00	0.00	0.00	0.01	0.00	9.22	2.00	0.00	0.00	0.01	0.00
9.23	2.00	0.00	0.00	0.01	0.00	9.24	2.00	0.00	0.00	0.01	0.00
9.25	2.00	0.00	0.00	0.01	0.00	9.26	2.00	0.00	0.00	0.01	0.00
9.27	2.00	0.00	0.00	0.01	0.00	9.28	2.00	0.00	0.00	0.01	0.00
9.29	2.00	0.00	0.00	0.01	0.00	9.30	2.00	0.00	0.00	0.01	0.00
9.31	1.22	0.00	0.00	0.01	0.00	9.32	1.27	0.00	0.00	0.01	0.00
9.33	1.29	0.00	0.00	0.01	0.00	9.34	1.28	0.00	0.00	0.01	0.00
9.35	1.26	0.00	0.00	0.01	0.00	9.36	1.26	0.00	0.00	0.01	0.00
9.37	1.26	0.00	0.00	0.01	0.00	9.38	1.25	0.00	0.00	0.01	0.00
9.39	1.21	0.00	0.00	0.01	0.00	9.40	2.00	0.00	0.00	0.01	0.00
9.41	2.00	0.00	0.00	0.01	0.00	9.42	2.00	0.00	0.00	0.01	0.00
9.43	2.00	0.00	0.00	0.01	0.00	9.44	2.00	0.00	0.00	0.01	0.00
9.45	2.00	0.00	0.00	0.01	0.00	9.46	2.00	0.00	0.00	0.01	0.00
9.47	2.00	0.00	0.00	0.01	0.00	9.48	2.00	0.00	0.00	0.01	0.00
9.49	2.00	0.00	0.00	0.01	0.00	9.50	2.00	0.00	0.00	0.01	0.00
9.51	2.00	0.00	0.00	0.01	0.00	9.52	2.00	0.00	0.00	0.01	0.00
9.53	2.00	0.00	0.00	0.01	0.00	9.54	2.00	0.00	0.00	0.01	0.00
9.55	2.00	0.00	0.00	0.01	0.00	9.56	2.00	0.00	0.00	0.01	0.00
9.57	2.00	0.00	0.00	0.01	0.00	9.58	2.00	0.00	0.00	0.01	0.00
9.59	2.00	0.00	0.00	0.01	0.00	9.60	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
9.61	2.00	0.00	0.00	0.01	0.00	9.62	2.00	0.00	0.00	0.01	0.00
9.63	2.00	0.00	0.00	0.01	0.00	9.64	1.23	0.00	0.00	0.01	0.00
9.65	1.35	0.00	0.00	0.01	0.00	9.66	1.38	0.00	0.00	0.01	0.00
9.67	1.40	0.00	0.00	0.01	0.00	9.68	1.48	0.00	0.00	0.01	0.00
9.69	1.49	0.00	0.00	0.01	0.00	9.70	1.51	0.00	0.00	0.01	0.00
9.71	1.53	0.00	0.00	0.01	0.00	9.72	1.57	0.00	0.00	0.01	0.00
9.73	1.56	0.00	0.00	0.01	0.00	9.74	1.55	0.00	0.00	0.01	0.00
9.75	1.55	0.00	0.00	0.01	0.00	9.76	1.55	0.00	0.00	0.01	0.00
9.77	1.51	0.00	0.00	0.01	0.00	9.78	1.51	0.00	0.00	0.01	0.00
9.79	1.48	0.00	0.00	0.01	0.00	9.80	1.47	0.00	0.00	0.01	0.00
9.81	1.45	0.00	0.00	0.01	0.00	9.82	1.42	0.00	0.00	0.01	0.00
9.83	1.38	0.00	0.00	0.01	0.00	9.84	1.29	0.00	0.00	0.01	0.00
9.85	2.00	0.00	0.00	0.01	0.00	9.86	2.00	0.00	0.00	0.01	0.00
9.87	2.00	0.00	0.00	0.01	0.00	9.88	2.00	0.00	0.00	0.01	0.00
9.89	2.00	0.00	0.00	0.01	0.00	9.90	2.00	0.00	0.00	0.01	0.00
9.91	2.00	0.00	0.00	0.01	0.00	9.92	2.00	0.00	0.00	0.01	0.00
9.93	2.00	0.00	0.00	0.01	0.00	9.94	2.00	0.00	0.00	0.01	0.00
9.95	2.00	0.00	0.00	0.01	0.00	9.96	2.00	0.00	0.00	0.01	0.00
9.97	2.00	0.00	0.00	0.01	0.00	9.98	2.00	0.00	0.00	0.01	0.00
9.99	2.00	0.00	0.00	0.01	0.00	10.00	2.00	0.00	0.00	0.01	0.00
10.01	2.00	0.00	0.00	0.01	0.00	10.02	2.00	0.00	0.00	0.01	0.00
10.03	2.00	0.00	0.00	0.01	0.00	10.04	2.00	0.00	0.00	0.01	0.00
10.05	2.00	0.00	0.00	0.01	0.00	10.06	2.00	0.00	0.00	0.01	0.00
10.07	2.00	0.00	0.00	0.01	0.00	10.08	1.12	0.00	0.00	0.01	0.00
10.09	1.15	0.00	0.00	0.01	0.00	10.10	1.17	0.00	0.00	0.01	0.00
10.11	1.19	0.00	0.00	0.01	0.00	10.12	1.21	0.00	0.00	0.01	0.00
10.13	1.22	0.00	0.00	0.01	0.00	10.14	2.00	0.00	0.00	0.01	0.00
10.15	2.00	0.00	0.00	0.01	0.00	10.16	2.00	0.00	0.00	0.01	0.00
10.17	2.00	0.00	0.00	0.01	0.00	10.18	2.00	0.00	0.00	0.01	0.00
10.19	2.00	0.00	0.00	0.01	0.00	10.20	2.00	0.00	0.00	0.01	0.00
10.21	2.00	0.00	0.00	0.01	0.00	10.22	2.00	0.00	0.00	0.01	0.00
10.23	2.00	0.00	0.00	0.01	0.00	10.24	2.00	0.00	0.00	0.01	0.00
10.25	2.00	0.00	0.00	0.01	0.00	10.26	2.00	0.00	0.00	0.01	0.00
10.27	2.00	0.00	0.00	0.01	0.00	10.28	2.00	0.00	0.00	0.01	0.00
10.29	2.00	0.00	0.00	0.01	0.00	10.30	2.00	0.00	0.00	0.01	0.00
10.31	2.00	0.00	0.00	0.01	0.00	10.32	2.00	0.00	0.00	0.01	0.00
10.33	2.00	0.00	0.00	0.01	0.00	10.34	2.00	0.00	0.00	0.01	0.00
10.35	2.00	0.00	0.00	0.01	0.00	10.36	2.00	0.00	0.00	0.01	0.00
10.37	2.00	0.00	0.00	0.01	0.00	10.38	2.00	0.00	0.00	0.01	0.00
10.39	2.00	0.00	0.00	0.01	0.00	10.40	2.00	0.00	0.00	0.01	0.00
10.41	2.00	0.00	0.00	0.01	0.00	10.42	2.00	0.00	0.00	0.01	0.00
10.43	2.00	0.00	0.00	0.01	0.00	10.44	2.00	0.00	0.00	0.01	0.00
10.45	2.00	0.00	0.00	0.01	0.00	10.46	2.00	0.00	0.00	0.01	0.00
10.47	2.00	0.00	0.00	0.01	0.00	10.48	2.00	0.00	0.00	0.01	0.00
10.49	2.00	0.00	0.00	0.01	0.00	10.50	2.00	0.00	0.00	0.01	0.00
10.51	2.00	0.00	0.00	0.01	0.00	10.52	2.00	0.00	0.00	0.01	0.00
10.53	2.00	0.00	0.00	0.01	0.00	10.54	2.00	0.00	0.00	0.01	0.00
10.55	2.00	0.00	0.00	0.01	0.00	10.56	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
10.57	2.00	0.00	0.00	0.01	0.00	10.58	2.00	0.00	0.00	0.01	0.00
10.59	2.00	0.00	0.00	0.01	0.00	10.60	2.00	0.00	0.00	0.01	0.00
10.61	2.00	0.00	0.00	0.01	0.00	10.62	1.26	0.00	0.00	0.01	0.00
10.63	1.37	0.00	0.00	0.01	0.00	10.64	1.41	0.00	0.00	0.01	0.00
10.65	1.51	0.00	0.00	0.01	0.00	10.66	1.51	0.00	0.00	0.01	0.00
10.67	1.56	0.00	0.00	0.01	0.00	10.68	1.54	0.00	0.00	0.01	0.00
10.69	1.53	0.00	0.00	0.01	0.00	10.70	1.50	0.00	0.00	0.01	0.00
10.71	1.48	0.00	0.00	0.01	0.00	10.72	1.10	0.00	0.00	0.01	0.00
10.73	1.47	0.00	0.00	0.01	0.00	10.74	1.49	0.00	0.00	0.01	0.00
10.75	1.51	0.00	0.00	0.01	0.00	10.76	1.54	0.00	0.00	0.01	0.00
10.77	1.57	0.00	0.00	0.01	0.00	10.78	1.59	0.00	0.00	0.01	0.00
10.79	1.61	0.00	0.00	0.01	0.00	10.80	1.67	0.00	0.00	0.01	0.00
10.81	1.69	0.00	0.00	0.01	0.00	10.82	1.70	0.00	0.00	0.01	0.00
10.83	1.72	0.00	0.00	0.01	0.00	10.84	1.75	0.00	0.00	0.01	0.00
10.85	1.77	0.00	0.00	0.01	0.00	10.86	1.76	0.00	0.00	0.01	0.00
10.87	1.75	0.00	0.00	0.01	0.00	10.88	1.72	0.00	0.00	0.01	0.00
10.89	1.72	0.00	0.00	0.01	0.00	10.90	1.71	0.00	0.00	0.01	0.00
10.91	1.71	0.00	0.00	0.01	0.00	10.92	1.70	0.00	0.00	0.01	0.00
10.93	1.69	0.00	0.00	0.01	0.00	10.94	1.70	0.00	0.00	0.01	0.00
10.95	1.70	0.00	0.00	0.01	0.00	10.96	1.70	0.00	0.00	0.01	0.00
10.97	1.71	0.00	0.00	0.01	0.00	10.98	1.70	0.00	0.00	0.01	0.00
10.99	1.70	0.00	0.00	0.01	0.00	11.00	1.70	0.00	0.00	0.01	0.00
11.01	1.71	0.00	0.00	0.01	0.00	11.02	1.69	0.00	0.00	0.01	0.00
11.03	1.70	0.00	0.00	0.01	0.00	11.04	1.70	0.00	0.00	0.01	0.00
11.05	1.68	0.00	0.00	0.01	0.00	11.06	1.69	0.00	0.00	0.01	0.00
11.07	1.67	0.00	0.00	0.01	0.00	11.08	1.68	0.00	0.00	0.01	0.00
11.09	1.67	0.00	0.00	0.01	0.00	11.10	1.66	0.00	0.00	0.01	0.00
11.11	1.64	0.00	0.00	0.01	0.00	11.12	1.53	0.00	0.00	0.01	0.00
11.13	1.51	0.00	0.00	0.01	0.00	11.14	1.42	0.00	0.00	0.01	0.00
11.15	1.39	0.00	0.00	0.01	0.00	11.16	2.00	0.00	0.00	0.01	0.00
11.17	2.00	0.00	0.00	0.01	0.00	11.18	2.00	0.00	0.00	0.01	0.00
11.19	2.00	0.00	0.00	0.01	0.00	11.20	2.00	0.00	0.00	0.01	0.00
11.21	2.00	0.00	0.00	0.01	0.00	11.22	2.00	0.00	0.00	0.01	0.00
11.23	2.00	0.00	0.00	0.01	0.00	11.24	2.00	0.00	0.00	0.01	0.00
11.25	2.00	0.00	0.00	0.01	0.00	11.26	2.00	0.00	0.00	0.01	0.00
11.27	2.00	0.00	0.00	0.01	0.00	11.28	2.00	0.00	0.00	0.01	0.00
11.29	2.00	0.00	0.00	0.01	0.00	11.30	2.00	0.00	0.00	0.01	0.00
11.31	2.00	0.00	0.00	0.01	0.00	11.32	1.42	0.00	0.00	0.01	0.00
11.33	1.46	0.00	0.00	0.01	0.00	11.34	1.40	0.00	0.00	0.01	0.00
11.35	1.35	0.00	0.00	0.01	0.00	11.36	1.31	0.00	0.00	0.01	0.00
11.37	1.24	0.00	0.00	0.01	0.00	11.38	2.00	0.00	0.00	0.01	0.00
11.39	2.00	0.00	0.00	0.01	0.00	11.40	2.00	0.00	0.00	0.01	0.00
11.41	2.00	0.00	0.00	0.01	0.00	11.42	1.21	0.00	0.00	0.01	0.00
11.43	1.23	0.00	0.00	0.01	0.00	11.44	1.31	0.00	0.00	0.01	0.00
11.45	1.36	0.00	0.00	0.01	0.00	11.46	1.58	0.00	0.00	0.01	0.00
11.47	1.61	0.00	0.00	0.01	0.00	11.48	1.64	0.00	0.00	0.01	0.00
11.49	1.67	0.00	0.00	0.01	0.00	11.50	1.61	0.00	0.00	0.01	0.00
11.51	1.59	0.00	0.00	0.01	0.00	11.52	1.47	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
11.53	1.43	0.00	0.00	0.01	0.00	11.54	0.98	0.00	0.00	0.01	0.00
11.55	1.39	0.00	0.00	0.01	0.00	11.56	1.38	0.00	0.00	0.01	0.00
11.57	1.40	0.00	0.00	0.01	0.00	11.58	1.41	0.00	0.00	0.01	0.00
11.59	1.41	0.00	0.00	0.01	0.00	11.60	1.63	0.00	0.00	0.01	0.00
11.61	1.76	0.00	0.00	0.01	0.00	11.62	1.79	0.00	0.00	0.01	0.00
11.63	1.82	0.00	0.00	0.01	0.00	11.64	1.81	0.00	0.00	0.01	0.00
11.65	1.79	0.00	0.00	0.01	0.00	11.66	1.77	0.00	0.00	0.01	0.00
11.67	1.72	0.00	0.00	0.01	0.00	11.68	1.74	0.00	0.00	0.01	0.00
11.69	1.72	0.00	0.00	0.01	0.00	11.70	1.72	0.00	0.00	0.01	0.00
11.71	1.76	0.00	0.00	0.01	0.00	11.72	1.75	0.00	0.00	0.01	0.00
11.73	1.75	0.00	0.00	0.01	0.00	11.74	1.76	0.00	0.00	0.01	0.00
11.75	1.77	0.00	0.00	0.01	0.00	11.76	1.78	0.00	0.00	0.01	0.00
11.77	1.82	0.00	0.00	0.01	0.00	11.78	1.85	0.00	0.00	0.01	0.00
11.79	1.87	0.00	0.00	0.01	0.00	11.80	1.89	0.00	0.00	0.01	0.00
11.81	1.91	0.00	0.00	0.01	0.00	11.82	1.92	0.00	0.00	0.01	0.00
11.83	1.93	0.00	0.00	0.01	0.00	11.84	1.94	0.00	0.00	0.01	0.00
11.85	1.94	0.00	0.00	0.01	0.00	11.86	1.96	0.00	0.00	0.01	0.00
11.87	1.97	0.00	0.00	0.01	0.00	11.88	1.99	0.00	0.00	0.01	0.00
11.89	2.00	0.00	0.00	0.01	0.00	11.90	2.00	0.00	0.00	0.01	0.00
11.91	2.00	0.00	0.00	0.01	0.00	11.92	2.00	0.00	0.00	0.01	0.00
11.93	2.00	0.00	0.00	0.01	0.00	11.94	2.00	0.00	0.00	0.01	0.00
11.95	2.00	0.00	0.00	0.01	0.00	11.96	2.00	0.00	0.00	0.01	0.00
11.97	2.00	0.00	0.00	0.01	0.00	11.98	2.00	0.00	0.00	0.01	0.00
11.99	2.00	0.00	0.00	0.01	0.00	12.00	2.00	0.00	0.00	0.01	0.00
12.01	2.00	0.00	0.00	0.01	0.00	12.02	2.00	0.00	0.00	0.01	0.00
12.03	2.00	0.00	0.00	0.01	0.00	12.04	2.00	0.00	0.00	0.01	0.00
12.05	2.00	0.00	0.00	0.01	0.00	12.06	2.00	0.00	0.00	0.01	0.00
12.07	2.00	0.00	0.00	0.01	0.00	12.08	2.00	0.00	0.00	0.01	0.00
12.09	2.00	0.00	0.00	0.01	0.00	12.10	2.00	0.00	0.00	0.01	0.00
12.11	2.00	0.00	0.00	0.01	0.00	12.12	2.00	0.00	0.00	0.01	0.00
12.13	2.00	0.00	0.00	0.01	0.00	12.14	2.00	0.00	0.00	0.01	0.00
12.15	2.00	0.00	0.00	0.01	0.00	12.16	2.00	0.00	0.00	0.01	0.00
12.17	2.00	0.00	0.00	0.01	0.00	12.18	2.00	0.00	0.00	0.01	0.00
12.19	2.00	0.00	0.00	0.01	0.00	12.20	2.00	0.00	0.00	0.01	0.00
12.21	2.00	0.00	0.00	0.01	0.00	12.22	2.00	0.00	0.00	0.01	0.00
12.23	2.00	0.00	0.00	0.01	0.00	12.24	2.00	0.00	0.00	0.01	0.00
12.25	2.00	0.00	0.00	0.01	0.00	12.26	2.00	0.00	0.00	0.01	0.00
12.27	2.00	0.00	0.00	0.01	0.00	12.28	2.00	0.00	0.00	0.01	0.00
12.29	2.00	0.00	0.00	0.01	0.00	12.30	2.00	0.00	0.00	0.01	0.00
12.31	2.00	0.00	0.00	0.01	0.00	12.32	2.00	0.00	0.00	0.01	0.00
12.33	2.00	0.00	0.00	0.01	0.00	12.34	2.00	0.00	0.00	0.01	0.00
12.35	2.00	0.00	0.00	0.01	0.00	12.36	2.00	0.00	0.00	0.01	0.00
12.37	2.00	0.00	0.00	0.01	0.00	12.38	2.00	0.00	0.00	0.01	0.00
12.39	2.00	0.00	0.00	0.01	0.00	12.40	2.00	0.00	0.00	0.01	0.00
12.41	2.00	0.00	0.00	0.01	0.00	12.42	2.00	0.00	0.00	0.01	0.00
12.43	2.00	0.00	0.00	0.01	0.00	12.44	2.00	0.00	0.00	0.01	0.00
12.45	2.00	0.00	0.00	0.01	0.00	12.46	2.00	0.00	0.00	0.01	0.00
12.47	2.00	0.00	0.00	0.01	0.00	12.48	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
12.49	2.00	0.00	0.00	0.01	0.00	12.50	2.00	0.00	0.00	0.01	0.00
12.51	2.00	0.00	0.00	0.01	0.00	12.52	2.00	0.00	0.00	0.01	0.00
12.53	2.00	0.00	0.00	0.01	0.00	12.54	1.94	0.00	0.00	0.01	0.00
12.55	1.88	0.00	0.00	0.01	0.00	12.56	1.89	0.00	0.00	0.01	0.00
12.57	1.90	0.00	0.00	0.01	0.00	12.58	1.90	0.00	0.00	0.01	0.00
12.59	1.89	0.00	0.00	0.01	0.00	12.60	1.94	0.00	0.00	0.01	0.00
12.61	1.98	0.00	0.00	0.01	0.00	12.62	2.00	0.00	0.00	0.01	0.00
12.63	2.00	0.00	0.00	0.01	0.00	12.64	2.00	0.00	0.00	0.01	0.00
12.65	2.00	0.00	0.00	0.01	0.00	12.66	2.00	0.00	0.00	0.01	0.00
12.67	2.00	0.00	0.00	0.01	0.00	12.68	2.00	0.00	0.00	0.01	0.00
12.69	2.00	0.00	0.00	0.01	0.00	12.70	2.00	0.00	0.00	0.01	0.00
12.71	2.00	0.00	0.00	0.01	0.00	12.72	2.00	0.00	0.00	0.01	0.00
12.73	2.00	0.00	0.00	0.01	0.00	12.74	2.00	0.00	0.00	0.01	0.00
12.75	2.00	0.00	0.00	0.01	0.00	12.76	1.99	0.00	0.00	0.01	0.00
12.77	1.98	0.00	0.00	0.01	0.00	12.78	1.98	0.00	0.00	0.01	0.00
12.79	1.98	0.00	0.00	0.01	0.00	12.80	1.97	0.00	0.00	0.01	0.00
12.81	1.96	0.00	0.00	0.01	0.00	12.82	1.95	0.00	0.00	0.01	0.00
12.83	1.98	0.00	0.00	0.01	0.00	12.84	1.99	0.00	0.00	0.01	0.00
12.85	2.00	0.00	0.00	0.01	0.00	12.86	2.00	0.00	0.00	0.01	0.00
12.87	2.00	0.00	0.00	0.01	0.00	12.88	2.00	0.00	0.00	0.01	0.00
12.89	2.00	0.00	0.00	0.01	0.00	12.90	2.00	0.00	0.00	0.01	0.00
12.91	2.00	0.00	0.00	0.01	0.00	12.92	2.00	0.00	0.00	0.01	0.00
12.93	2.00	0.00	0.00	0.01	0.00	12.94	2.00	0.00	0.00	0.01	0.00
12.95	1.96	0.00	0.00	0.01	0.00	12.96	1.92	0.00	0.00	0.01	0.00
12.97	1.92	0.00	0.00	0.01	0.00	12.98	1.89	0.00	0.00	0.01	0.00
12.99	1.90	0.00	0.00	0.01	0.00	13.00	1.83	0.00	0.00	0.01	0.00
13.01	1.81	0.00	0.00	0.01	0.00	13.02	1.80	0.00	0.00	0.01	0.00
13.03	1.80	0.00	0.00	0.01	0.00	13.04	1.82	0.00	0.00	0.01	0.00
13.05	1.80	0.00	0.00	0.01	0.00	13.06	1.83	0.00	0.00	0.01	0.00
13.07	1.76	0.00	0.00	0.01	0.00	13.08	1.75	0.00	0.00	0.01	0.00
13.09	1.74	0.00	0.00	0.01	0.00	13.10	1.76	0.00	0.00	0.01	0.00
13.11	1.83	0.00	0.00	0.01	0.00	13.12	1.90	0.00	0.00	0.01	0.00
13.13	1.96	0.00	0.00	0.01	0.00	13.14	2.00	0.00	0.00	0.01	0.00
13.15	2.00	0.00	0.00	0.01	0.00	13.16	2.00	0.00	0.00	0.01	0.00
13.17	2.00	0.00	0.00	0.01	0.00	13.18	1.97	0.00	0.00	0.01	0.00
13.19	1.92	0.00	0.00	0.01	0.00	13.20	1.87	0.00	0.00	0.01	0.00
13.21	1.82	0.00	0.00	0.01	0.00	13.22	1.80	0.00	0.00	0.01	0.00
13.23	1.85	0.00	0.00	0.01	0.00	13.24	1.90	0.00	0.00	0.01	0.00
13.25	1.94	0.00	0.00	0.01	0.00	13.26	1.96	0.00	0.00	0.01	0.00
13.27	2.00	0.00	0.00	0.01	0.00	13.28	2.00	0.00	0.00	0.01	0.00
13.29	2.00	0.00	0.00	0.01	0.00	13.30	2.00	0.00	0.00	0.01	0.00
13.31	2.00	0.00	0.00	0.01	0.00	13.32	2.00	0.00	0.00	0.01	0.00
13.33	2.00	0.00	0.00	0.01	0.00	13.34	2.00	0.00	0.00	0.01	0.00
13.35	2.00	0.00	0.00	0.01	0.00	13.36	2.00	0.00	0.00	0.01	0.00
13.37	2.00	0.00	0.00	0.01	0.00	13.38	2.00	0.00	0.00	0.01	0.00
13.39	2.00	0.00	0.00	0.01	0.00	13.40	2.00	0.00	0.00	0.01	0.00
13.41	2.00	0.00	0.00	0.01	0.00	13.42	2.00	0.00	0.00	0.01	0.00
13.43	2.00	0.00	0.00	0.01	0.00	13.44	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
13.45	2.00	0.00	0.00	0.01	0.00	13.46	2.00	0.00	0.00	0.01	0.00
13.47	2.00	0.00	0.00	0.01	0.00	13.48	2.00	0.00	0.00	0.01	0.00
13.49	2.00	0.00	0.00	0.01	0.00	13.50	2.00	0.00	0.00	0.01	0.00
13.51	2.00	0.00	0.00	0.01	0.00	13.52	2.00	0.00	0.00	0.01	0.00
13.53	2.00	0.00	0.00	0.01	0.00	13.54	2.00	0.00	0.00	0.01	0.00
13.55	2.00	0.00	0.00	0.01	0.00	13.56	2.00	0.00	0.00	0.01	0.00
13.57	2.00	0.00	0.00	0.01	0.00	13.58	2.00	0.00	0.00	0.01	0.00
13.59	2.00	0.00	0.00	0.01	0.00	13.60	2.00	0.00	0.00	0.01	0.00
13.61	2.00	0.00	0.00	0.01	0.00	13.62	2.00	0.00	0.00	0.01	0.00
13.63	2.00	0.00	0.00	0.01	0.00	13.64	2.00	0.00	0.00	0.01	0.00
13.65	2.00	0.00	0.00	0.01	0.00	13.66	2.00	0.00	0.00	0.01	0.00
13.67	2.00	0.00	0.00	0.01	0.00	13.68	2.00	0.00	0.00	0.01	0.00
13.69	2.00	0.00	0.00	0.01	0.00	13.70	2.00	0.00	0.00	0.01	0.00
13.71	2.00	0.00	0.00	0.01	0.00	13.72	2.00	0.00	0.00	0.01	0.00
13.73	2.00	0.00	0.00	0.01	0.00	13.74	2.00	0.00	0.00	0.01	0.00
13.75	2.00	0.00	0.00	0.01	0.00	13.76	2.00	0.00	0.00	0.01	0.00
13.77	2.00	0.00	0.00	0.01	0.00	13.78	2.00	0.00	0.00	0.01	0.00
13.79	2.00	0.00	0.00	0.01	0.00	13.80	2.00	0.00	0.00	0.01	0.00
13.81	2.00	0.00	0.00	0.01	0.00	13.82	2.00	0.00	0.00	0.01	0.00
13.83	2.00	0.00	0.00	0.01	0.00	13.84	2.00	0.00	0.00	0.01	0.00
13.85	2.00	0.00	0.00	0.01	0.00	13.86	2.00	0.00	0.00	0.01	0.00
13.87	2.00	0.00	0.00	0.01	0.00	13.88	2.00	0.00	0.00	0.01	0.00
13.89	2.00	0.00	0.00	0.01	0.00	13.90	2.00	0.00	0.00	0.01	0.00
13.91	2.00	0.00	0.00	0.01	0.00	13.92	2.00	0.00	0.00	0.01	0.00
13.93	2.00	0.00	0.00	0.01	0.00	13.94	2.00	0.00	0.00	0.01	0.00
13.95	2.00	0.00	0.00	0.01	0.00	13.96	2.00	0.00	0.00	0.01	0.00
13.97	2.00	0.00	0.00	0.01	0.00	13.98	2.00	0.00	0.00	0.01	0.00
13.99	2.00	0.00	0.00	0.01	0.00	14.00	2.00	0.00	0.00	0.01	0.00
14.01	2.00	0.00	0.00	0.01	0.00	14.02	2.00	0.00	0.00	0.01	0.00
14.03	2.00	0.00	0.00	0.01	0.00	14.04	2.00	0.00	0.00	0.01	0.00
14.05	2.00	0.00	0.00	0.01	0.00	14.06	2.00	0.00	0.00	0.01	0.00
14.07	2.00	0.00	0.00	0.01	0.00	14.08	2.00	0.00	0.00	0.01	0.00
14.09	2.00	0.00	0.00	0.01	0.00	14.10	2.00	0.00	0.00	0.01	0.00
14.11	2.00	0.00	0.00	0.01	0.00	14.12	2.00	0.00	0.00	0.01	0.00
14.13	2.00	0.00	0.00	0.01	0.00	14.14	2.00	0.00	0.00	0.01	0.00
14.15	2.00	0.00	0.00	0.01	0.00	14.16	2.00	0.00	0.00	0.01	0.00
14.17	2.00	0.00	0.00	0.01	0.00	14.18	2.00	0.00	0.00	0.01	0.00
14.19	2.00	0.00	0.00	0.01	0.00	14.20	2.00	0.00	0.00	0.01	0.00
14.21	2.00	0.00	0.00	0.01	0.00	14.22	2.00	0.00	0.00	0.01	0.00
14.23	2.00	0.00	0.00	0.01	0.00	14.24	2.00	0.00	0.00	0.01	0.00
14.25	2.00	0.00	0.00	0.01	0.00	14.26	2.00	0.00	0.00	0.01	0.00
14.27	2.00	0.00	0.00	0.01	0.00	14.28	2.00	0.00	0.00	0.01	0.00
14.29	2.00	0.00	0.00	0.01	0.00	14.30	2.00	0.00	0.00	0.01	0.00
14.31	2.00	0.00	0.00	0.01	0.00	14.32	2.00	0.00	0.00	0.01	0.00
14.33	2.00	0.00	0.00	0.01	0.00	14.34	2.00	0.00	0.00	0.01	0.00
14.35	2.00	0.00	0.00	0.01	0.00	14.36	2.00	0.00	0.00	0.01	0.00
14.37	2.00	0.00	0.00	0.01	0.00	14.38	2.00	0.00	0.00	0.01	0.00
14.39	2.00	0.00	0.00	0.01	0.00	14.40	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
14.41	2.00	0.00	0.00	0.01	0.00	14.42	2.00	0.00	0.00	0.01	0.00
14.43	2.00	0.00	0.00	0.01	0.00	14.44	2.00	0.00	0.00	0.01	0.00
14.45	2.00	0.00	0.00	0.01	0.00	14.46	2.00	0.00	0.00	0.01	0.00
14.47	2.00	0.00	0.00	0.01	0.00	14.48	2.00	0.00	0.00	0.01	0.00
14.49	2.00	0.00	0.00	0.01	0.00	14.50	2.00	0.00	0.00	0.01	0.00
14.51	2.00	0.00	0.00	0.01	0.00	14.52	2.00	0.00	0.00	0.01	0.00
14.53	2.00	0.00	0.00	0.01	0.00	14.54	2.00	0.00	0.00	0.01	0.00
14.55	2.00	0.00	0.00	0.01	0.00	14.56	2.00	0.00	0.00	0.01	0.00
14.57	2.00	0.00	0.00	0.01	0.00	14.58	2.00	0.00	0.00	0.01	0.00
14.59	2.00	0.00	0.00	0.01	0.00	14.60	2.00	0.00	0.00	0.01	0.00
14.61	2.00	0.00	0.00	0.01	0.00	14.62	2.00	0.00	0.00	0.01	0.00
14.63	2.00	0.00	0.00	0.01	0.00	14.64	2.00	0.00	0.00	0.01	0.00
14.65	2.00	0.00	0.00	0.01	0.00	14.66	1.93	0.00	0.00	0.01	0.00
14.67	1.94	0.00	0.00	0.01	0.00	14.68	1.96	0.00	0.00	0.01	0.00
14.69	2.00	0.00	0.00	0.01	0.00	14.70	2.00	0.00	0.00	0.01	0.00
14.71	2.00	0.00	0.00	0.01	0.00	14.72	2.00	0.00	0.00	0.01	0.00
14.73	2.00	0.00	0.00	0.01	0.00	14.74	2.00	0.00	0.00	0.01	0.00
14.75	2.00	0.00	0.00	0.01	0.00	14.76	2.00	0.00	0.00	0.01	0.00
14.77	2.00	0.00	0.00	0.01	0.00	14.78	2.00	0.00	0.00	0.01	0.00
14.79	2.00	0.00	0.00	0.01	0.00	14.80	2.00	0.00	0.00	0.01	0.00
14.81	2.00	0.00	0.00	0.01	0.00	14.82	2.00	0.00	0.00	0.01	0.00
14.83	2.00	0.00	0.00	0.01	0.00	14.84	2.00	0.00	0.00	0.01	0.00
14.85	2.00	0.00	0.00	0.01	0.00	14.86	2.00	0.00	0.00	0.01	0.00
14.87	2.00	0.00	0.00	0.01	0.00	14.88	2.00	0.00	0.00	0.01	0.00
14.89	2.00	0.00	0.00	0.01	0.00	14.90	2.00	0.00	0.00	0.01	0.00
14.91	2.00	0.00	0.00	0.01	0.00	14.92	2.00	0.00	0.00	0.01	0.00
14.93	2.00	0.00	0.00	0.01	0.00	14.94	2.00	0.00	0.00	0.01	0.00
14.95	2.00	0.00	0.00	0.01	0.00	14.96	2.00	0.00	0.00	0.01	0.00
14.97	2.00	0.00	0.00	0.01	0.00	14.98	2.00	0.00	0.00	0.01	0.00
14.99	2.00	0.00	0.00	0.01	0.00	15.00	2.00	0.00	0.00	0.01	0.00
15.01	2.00	0.00	0.00	0.01	0.00	15.02	2.00	0.00	0.00	0.01	0.00
15.03	2.00	0.00	0.00	0.01	0.00	15.04	1.84	0.00	0.00	0.01	0.00
15.05	1.76	0.00	0.00	0.01	0.00	15.06	2.00	0.00	0.00	0.01	0.00
15.07	2.00	0.00	0.00	0.01	0.00	15.08	2.00	0.00	0.00	0.01	0.00
15.09	2.00	0.00	0.00	0.01	0.00	15.10	2.00	0.00	0.00	0.01	0.00
15.11	2.00	0.00	0.00	0.01	0.00	15.12	2.00	0.00	0.00	0.01	0.00
15.13	2.00	0.00	0.00	0.01	0.00	15.14	2.00	0.00	0.00	0.01	0.00
15.15	2.00	0.00	0.00	0.01	0.00	15.16	2.00	0.00	0.00	0.01	0.00
15.17	2.00	0.00	0.00	0.01	0.00	15.18	2.00	0.00	0.00	0.01	0.00
15.19	2.00	0.00	0.00	0.01	0.00	15.20	2.00	0.00	0.00	0.01	0.00
15.21	2.00	0.00	0.00	0.01	0.00	15.22	2.00	0.00	0.00	0.01	0.00
15.23	2.00	0.00	0.00	0.01	0.00	15.24	2.00	0.00	0.00	0.01	0.00
15.25	2.00	0.00	0.00	0.01	0.00	15.26	2.00	0.00	0.00	0.01	0.00
15.27	2.00	0.00	0.00	0.01	0.00	15.28	2.00	0.00	0.00	0.01	0.00
15.29	2.00	0.00	0.00	0.01	0.00	15.30	2.00	0.00	0.00	0.01	0.00
15.31	2.00	0.00	0.00	0.01	0.00	15.32	2.00	0.00	0.00	0.01	0.00
15.33	2.00	0.00	0.00	0.01	0.00	15.34	2.00	0.00	0.00	0.01	0.00
15.35	1.24	0.00	0.00	0.01	0.00	15.36	1.28	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
15.37	1.29	0.00	0.00	0.01	0.00	15.38	1.30	0.00	0.00	0.01	0.00
15.39	1.32	0.00	0.00	0.01	0.00	15.40	1.32	0.00	0.00	0.01	0.00
15.41	1.32	0.00	0.00	0.01	0.00	15.42	1.32	0.00	0.00	0.01	0.00
15.43	2.00	0.00	0.00	0.01	0.00	15.44	2.00	0.00	0.00	0.01	0.00
15.45	2.00	0.00	0.00	0.01	0.00	15.46	2.00	0.00	0.00	0.01	0.00
15.47	2.00	0.00	0.00	0.01	0.00	15.48	2.00	0.00	0.00	0.01	0.00
15.49	2.00	0.00	0.00	0.01	0.00	15.50	2.00	0.00	0.00	0.01	0.00
15.51	2.00	0.00	0.00	0.01	0.00	15.52	2.00	0.00	0.00	0.01	0.00
15.53	2.00	0.00	0.00	0.01	0.00	15.54	2.00	0.00	0.00	0.01	0.00
15.55	1.37	0.00	0.00	0.01	0.00	15.56	1.37	0.00	0.00	0.01	0.00
15.57	1.34	0.00	0.00	0.01	0.00	15.58	1.88	0.00	0.00	0.01	0.00
15.59	1.87	0.00	0.00	0.01	0.00	15.60	1.96	0.00	0.00	0.01	0.00
15.61	1.96	0.00	0.00	0.01	0.00	15.62	1.97	0.00	0.00	0.01	0.00
15.63	1.94	0.00	0.00	0.01	0.00	15.64	1.95	0.00	0.00	0.01	0.00
15.65	1.79	0.00	0.00	0.01	0.00	15.66	1.71	0.00	0.00	0.01	0.00
15.67	1.65	0.00	0.00	0.01	0.00	15.68	2.00	0.00	0.00	0.01	0.00
15.69	2.00	0.00	0.00	0.01	0.00	15.70	2.00	0.00	0.00	0.01	0.00
15.71	2.00	0.00	0.00	0.01	0.00	15.72	2.00	0.00	0.00	0.01	0.00
15.73	2.00	0.00	0.00	0.01	0.00	15.74	2.00	0.00	0.00	0.01	0.00
15.75	2.00	0.00	0.00	0.01	0.00	15.76	2.00	0.00	0.00	0.01	0.00
15.77	2.00	0.00	0.00	0.01	0.00	15.78	2.00	0.00	0.00	0.01	0.00
15.79	2.00	0.00	0.00	0.01	0.00	15.80	2.00	0.00	0.00	0.01	0.00
15.81	2.00	0.00	0.00	0.01	0.00	15.82	2.00	0.00	0.00	0.01	0.00
15.83	2.00	0.00	0.00	0.01	0.00	15.84	2.00	0.00	0.00	0.01	0.00
15.85	2.00	0.00	0.00	0.01	0.00	15.86	2.00	0.00	0.00	0.01	0.00
15.87	2.00	0.00	0.00	0.01	0.00	15.88	2.00	0.00	0.00	0.01	0.00
15.89	2.00	0.00	0.00	0.01	0.00	15.90	2.00	0.00	0.00	0.01	0.00
15.91	2.00	0.00	0.00	0.01	0.00	15.92	2.00	0.00	0.00	0.01	0.00
15.93	2.00	0.00	0.00	0.01	0.00	15.94	2.00	0.00	0.00	0.01	0.00
15.95	2.00	0.00	0.00	0.01	0.00	15.96	2.00	0.00	0.00	0.01	0.00
15.97	2.00	0.00	0.00	0.01	0.00	15.98	2.00	0.00	0.00	0.01	0.00
15.99	2.00	0.00	0.00	0.01	0.00	16.00	2.00	0.00	0.00	0.01	0.00
16.01	2.00	0.00	0.00	0.01	0.00	16.02	2.00	0.00	0.00	0.01	0.00
16.03	2.00	0.00	0.00	0.01	0.00	16.04	2.00	0.00	0.00	0.01	0.00
16.05	2.00	0.00	0.00	0.01	0.00	16.06	2.00	0.00	0.00	0.01	0.00
16.07	2.00	0.00	0.00	0.01	0.00	16.08	2.00	0.00	0.00	0.01	0.00
16.09	2.00	0.00	0.00	0.01	0.00	16.10	2.00	0.00	0.00	0.01	0.00
16.11	2.00	0.00	0.00	0.01	0.00	16.12	2.00	0.00	0.00	0.01	0.00
16.13	2.00	0.00	0.00	0.01	0.00	16.14	2.00	0.00	0.00	0.01	0.00
16.15	2.00	0.00	0.00	0.01	0.00	16.16	2.00	0.00	0.00	0.01	0.00
16.17	2.00	0.00	0.00	0.01	0.00	16.18	2.00	0.00	0.00	0.01	0.00
16.19	2.00	0.00	0.00	0.01	0.00	16.20	2.00	0.00	0.00	0.01	0.00
16.21	2.00	0.00	0.00	0.01	0.00	16.22	2.00	0.00	0.00	0.01	0.00
16.23	2.00	0.00	0.00	0.01	0.00	16.24	2.00	0.00	0.00	0.01	0.00
16.25	2.00	0.00	0.00	0.01	0.00	16.26	2.00	0.00	0.00	0.01	0.00
16.27	2.00	0.00	0.00	0.01	0.00	16.28	2.00	0.00	0.00	0.01	0.00
16.29	2.00	0.00	0.00	0.01	0.00	16.30	2.00	0.00	0.00	0.01	0.00
16.31	2.00	0.00	0.00	0.01	0.00	16.32	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
16.33	2.00	0.00	0.00	0.01	0.00	16.34	2.00	0.00	0.00	0.01	0.00
16.35	2.00	0.00	0.00	0.01	0.00	16.36	2.00	0.00	0.00	0.01	0.00
16.37	2.00	0.00	0.00	0.01	0.00	16.38	2.00	0.00	0.00	0.01	0.00
16.39	2.00	0.00	0.00	0.01	0.00	16.40	2.00	0.00	0.00	0.01	0.00
16.41	2.00	0.00	0.00	0.01	0.00	16.42	2.00	0.00	0.00	0.01	0.00
16.43	2.00	0.00	0.00	0.01	0.00	16.44	2.00	0.00	0.00	0.01	0.00
16.45	2.00	0.00	0.00	0.01	0.00	16.46	2.00	0.00	0.00	0.01	0.00
16.47	2.00	0.00	0.00	0.01	0.00	16.48	2.00	0.00	0.00	0.01	0.00
16.49	2.00	0.00	0.00	0.01	0.00	16.50	2.00	0.00	0.00	0.01	0.00
16.51	2.00	0.00	0.00	0.01	0.00	16.52	2.00	0.00	0.00	0.01	0.00
16.53	2.00	0.00	0.00	0.01	0.00	16.54	2.00	0.00	0.00	0.01	0.00
16.55	2.00	0.00	0.00	0.01	0.00	16.56	1.37	0.00	0.00	0.01	0.00
16.57	1.33	0.00	0.00	0.01	0.00	16.58	1.83	0.00	0.00	0.01	0.00
16.59	1.91	0.00	0.00	0.01	0.00	16.60	1.89	0.00	0.00	0.01	0.00
16.61	1.96	0.00	0.00	0.01	0.00	16.62	1.58	0.00	0.00	0.01	0.00
16.63	1.64	0.00	0.00	0.01	0.00	16.64	1.75	0.00	0.00	0.01	0.00
16.65	1.79	0.00	0.00	0.01	0.00	16.66	1.82	0.00	0.00	0.01	0.00
16.67	1.85	0.00	0.00	0.01	0.00	16.68	1.89	0.00	0.00	0.01	0.00
16.69	1.89	0.00	0.00	0.01	0.00	16.70	1.89	0.00	0.00	0.01	0.00
16.71	1.87	0.00	0.00	0.01	0.00	16.72	1.84	0.00	0.00	0.01	0.00
16.73	2.00	0.00	0.00	0.01	0.00	16.74	2.00	0.00	0.00	0.01	0.00
16.75	2.00	0.00	0.00	0.01	0.00	16.76	2.00	0.00	0.00	0.01	0.00
16.77	2.00	0.00	0.00	0.01	0.00	16.78	2.00	0.00	0.00	0.01	0.00
16.79	2.00	0.00	0.00	0.01	0.00	16.80	2.00	0.00	0.00	0.01	0.00
16.81	2.00	0.00	0.00	0.01	0.00	16.82	2.00	0.00	0.00	0.01	0.00
16.83	2.00	0.00	0.00	0.01	0.00	16.84	2.00	0.00	0.00	0.01	0.00
16.85	2.00	0.00	0.00	0.01	0.00	16.86	2.00	0.00	0.00	0.01	0.00
16.87	2.00	0.00	0.00	0.01	0.00	16.88	2.00	0.00	0.00	0.01	0.00
16.89	2.00	0.00	0.00	0.01	0.00	16.90	2.00	0.00	0.00	0.01	0.00
16.91	2.00	0.00	0.00	0.01	0.00	16.92	2.00	0.00	0.00	0.01	0.00
16.93	2.00	0.00	0.00	0.01	0.00	16.94	2.00	0.00	0.00	0.01	0.00
16.95	2.00	0.00	0.00	0.01	0.00	16.96	2.00	0.00	0.00	0.01	0.00
16.97	2.00	0.00	0.00	0.01	0.00	16.98	2.00	0.00	0.00	0.01	0.00
16.99	2.00	0.00	0.00	0.01	0.00	17.00	2.00	0.00	0.00	0.01	0.00
17.01	2.00	0.00	0.00	0.01	0.00	17.02	2.00	0.00	0.00	0.01	0.00
17.03	2.00	0.00	0.00	0.01	0.00	17.04	2.00	0.00	0.00	0.01	0.00
17.05	2.00	0.00	0.00	0.01	0.00	17.06	2.00	0.00	0.00	0.01	0.00
17.07	2.00	0.00	0.00	0.01	0.00	17.08	2.00	0.00	0.00	0.01	0.00
17.09	2.00	0.00	0.00	0.01	0.00	17.10	2.00	0.00	0.00	0.01	0.00
17.11	2.00	0.00	0.00	0.01	0.00	17.12	2.00	0.00	0.00	0.01	0.00
17.13	2.00	0.00	0.00	0.01	0.00	17.14	2.00	0.00	0.00	0.01	0.00
17.15	2.00	0.00	0.00	0.01	0.00	17.16	2.00	0.00	0.00	0.01	0.00
17.17	2.00	0.00	0.00	0.01	0.00	17.18	2.00	0.00	0.00	0.01	0.00
17.19	2.00	0.00	0.00	0.01	0.00	17.20	2.00	0.00	0.00	0.01	0.00
17.21	2.00	0.00	0.00	0.01	0.00	17.22	2.00	0.00	0.00	0.01	0.00
17.23	2.00	0.00	0.00	0.01	0.00	17.24	2.00	0.00	0.00	0.01	0.00
17.25	2.00	0.00	0.00	0.01	0.00	17.26	2.00	0.00	0.00	0.01	0.00
17.27	2.00	0.00	0.00	0.01	0.00	17.28	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
17.29	2.00	0.00	0.00	0.01	0.00	17.30	2.00	0.00	0.00	0.01	0.00
17.31	2.00	0.00	0.00	0.01	0.00	17.32	2.00	0.00	0.00	0.01	0.00
17.33	2.00	0.00	0.00	0.01	0.00	17.34	2.00	0.00	0.00	0.01	0.00
17.35	2.00	0.00	0.00	0.01	0.00	17.36	2.00	0.00	0.00	0.01	0.00
17.37	2.00	0.00	0.00	0.01	0.00	17.38	2.00	0.00	0.00	0.01	0.00
17.39	2.00	0.00	0.00	0.01	0.00	17.40	2.00	0.00	0.00	0.01	0.00
17.41	2.00	0.00	0.00	0.01	0.00	17.42	2.00	0.00	0.00	0.01	0.00
17.43	2.00	0.00	0.00	0.01	0.00	17.44	2.00	0.00	0.00	0.01	0.00
17.45	2.00	0.00	0.00	0.01	0.00	17.46	2.00	0.00	0.00	0.01	0.00
17.47	2.00	0.00	0.00	0.01	0.00	17.48	2.00	0.00	0.00	0.01	0.00
17.49	2.00	0.00	0.00	0.01	0.00	17.50	2.00	0.00	0.00	0.01	0.00
17.51	2.00	0.00	0.00	0.01	0.00	17.52	2.00	0.00	0.00	0.01	0.00
17.53	2.00	0.00	0.00	0.01	0.00	17.54	2.00	0.00	0.00	0.01	0.00
17.55	2.00	0.00	0.00	0.01	0.00	17.56	2.00	0.00	0.00	0.01	0.00
17.57	2.00	0.00	0.00	0.01	0.00	17.58	2.00	0.00	0.00	0.01	0.00
17.59	2.00	0.00	0.00	0.01	0.00	17.60	2.00	0.00	0.00	0.01	0.00
17.61	2.00	0.00	0.00	0.01	0.00	17.62	2.00	0.00	0.00	0.01	0.00
17.63	2.00	0.00	0.00	0.01	0.00	17.64	2.00	0.00	0.00	0.01	0.00
17.65	2.00	0.00	0.00	0.01	0.00	17.66	2.00	0.00	0.00	0.01	0.00
17.67	2.00	0.00	0.00	0.01	0.00	17.68	2.00	0.00	0.00	0.01	0.00
17.69	2.00	0.00	0.00	0.01	0.00	17.70	2.00	0.00	0.00	0.01	0.00
17.71	2.00	0.00	0.00	0.01	0.00	17.72	2.00	0.00	0.00	0.01	0.00
17.73	2.00	0.00	0.00	0.01	0.00	17.74	2.00	0.00	0.00	0.01	0.00
17.75	2.00	0.00	0.00	0.01	0.00	17.76	2.00	0.00	0.00	0.01	0.00
17.77	2.00	0.00	0.00	0.01	0.00	17.78	2.00	0.00	0.00	0.01	0.00
17.79	2.00	0.00	0.00	0.01	0.00	17.80	2.00	0.00	0.00	0.01	0.00
17.81	2.00	0.00	0.00	0.01	0.00	17.82	2.00	0.00	0.00	0.01	0.00
17.83	2.00	0.00	0.00	0.01	0.00	17.84	2.00	0.00	0.00	0.01	0.00
17.85	2.00	0.00	0.00	0.01	0.00	17.86	2.00	0.00	0.00	0.01	0.00
17.87	2.00	0.00	0.00	0.01	0.00	17.88	2.00	0.00	0.00	0.01	0.00
17.89	2.00	0.00	0.00	0.01	0.00	17.90	2.00	0.00	0.00	0.01	0.00
17.91	2.00	0.00	0.00	0.01	0.00	17.92	2.00	0.00	0.00	0.01	0.00
17.93	2.00	0.00	0.00	0.01	0.00	17.94	2.00	0.00	0.00	0.01	0.00
17.95	2.00	0.00	0.00	0.01	0.00	17.96	2.00	0.00	0.00	0.01	0.00
17.97	2.00	0.00	0.00	0.01	0.00	17.98	2.00	0.00	0.00	0.01	0.00
17.99	2.00	0.00	0.00	0.01	0.00	18.00	2.00	0.00	0.00	0.01	0.00
18.01	2.00	0.00	0.00	0.01	0.00	18.02	2.00	0.00	0.00	0.01	0.00
18.03	2.00	0.00	0.00	0.01	0.00	18.04	2.00	0.00	0.00	0.01	0.00
18.05	2.00	0.00	0.00	0.01	0.00	18.06	2.00	0.00	0.00	0.01	0.00
18.07	2.00	0.00	0.00	0.01	0.00	18.08	2.00	0.00	0.00	0.01	0.00
18.09	2.00	0.00	0.00	0.01	0.00	18.10	2.00	0.00	0.00	0.01	0.00
18.11	2.00	0.00	0.00	0.01	0.00	18.12	2.00	0.00	0.00	0.01	0.00
18.13	2.00	0.00	0.00	0.01	0.00	18.14	2.00	0.00	0.00	0.01	0.00
18.15	2.00	0.00	0.00	0.01	0.00	18.16	2.00	0.00	0.00	0.01	0.00
18.17	2.00	0.00	0.00	0.01	0.00	18.18	2.00	0.00	0.00	0.01	0.00
18.19	2.00	0.00	0.00	0.01	0.00	18.20	2.00	0.00	0.00	0.01	0.00
18.21	2.00	0.00	0.00	0.01	0.00	18.22	2.00	0.00	0.00	0.01	0.00
18.23	2.00	0.00	0.00	0.01	0.00	18.24	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
18.25	2.00	0.00	0.00	0.01	0.00	18.26	2.00	0.00	0.00	0.01	0.00
18.27	2.00	0.00	0.00	0.01	0.00	18.28	2.00	0.00	0.00	0.01	0.00
18.29	2.00	0.00	0.00	0.01	0.00	18.30	2.00	0.00	0.00	0.01	0.00
18.31	2.00	0.00	0.00	0.01	0.00	18.32	2.00	0.00	0.00	0.01	0.00
18.33	2.00	0.00	0.00	0.01	0.00	18.34	2.00	0.00	0.00	0.01	0.00
18.35	2.00	0.00	0.00	0.01	0.00	18.36	2.00	0.00	0.00	0.01	0.00
18.37	2.00	0.00	0.00	0.01	0.00	18.38	2.00	0.00	0.00	0.01	0.00
18.39	2.00	0.00	0.00	0.01	0.00	18.40	2.00	0.00	0.00	0.01	0.00
18.41	2.00	0.00	0.00	0.01	0.00	18.42	2.00	0.00	0.00	0.01	0.00
18.43	2.00	0.00	0.00	0.01	0.00	18.44	2.00	0.00	0.00	0.01	0.00
18.45	2.00	0.00	0.00	0.01	0.00	18.46	2.00	0.00	0.00	0.01	0.00
18.47	2.00	0.00	0.00	0.01	0.00	18.48	2.00	0.00	0.00	0.01	0.00
18.49	2.00	0.00	0.00	0.01	0.00	18.50	2.00	0.00	0.00	0.01	0.00
18.51	2.00	0.00	0.00	0.01	0.00	18.52	2.00	0.00	0.00	0.01	0.00
18.53	2.00	0.00	0.00	0.01	0.00	18.54	2.00	0.00	0.00	0.01	0.00
18.55	2.00	0.00	0.00	0.01	0.00	18.56	2.00	0.00	0.00	0.01	0.00
18.57	2.00	0.00	0.00	0.01	0.00	18.58	2.00	0.00	0.00	0.01	0.00
18.59	2.00	0.00	0.00	0.01	0.00	18.60	2.00	0.00	0.00	0.01	0.00
18.61	2.00	0.00	0.00	0.01	0.00	18.62	2.00	0.00	0.00	0.01	0.00
18.63	2.00	0.00	0.00	0.01	0.00	18.64	2.00	0.00	0.00	0.01	0.00
18.65	2.00	0.00	0.00	0.01	0.00	18.66	2.00	0.00	0.00	0.01	0.00
18.67	2.00	0.00	0.00	0.01	0.00	18.68	2.00	0.00	0.00	0.01	0.00
18.69	2.00	0.00	0.00	0.01	0.00	18.70	2.00	0.00	0.00	0.01	0.00
18.71	2.00	0.00	0.00	0.01	0.00	18.72	2.00	0.00	0.00	0.01	0.00
18.73	2.00	0.00	0.00	0.01	0.00	18.74	2.00	0.00	0.00	0.01	0.00
18.75	2.00	0.00	0.00	0.01	0.00	18.76	2.00	0.00	0.00	0.01	0.00
18.77	1.59	0.00	0.00	0.01	0.00	18.78	1.65	0.00	0.00	0.01	0.00
18.79	1.80	0.00	0.00	0.01	0.00	18.80	1.85	0.00	0.00	0.01	0.00
18.81	1.92	0.00	0.00	0.01	0.00	18.82	1.98	0.00	0.00	0.01	0.00
18.83	2.00	0.00	0.00	0.01	0.00	18.84	2.00	0.00	0.00	0.01	0.00
18.85	2.00	0.00	0.00	0.01	0.00	18.86	2.00	0.00	0.00	0.01	0.00
18.87	2.00	0.00	0.00	0.01	0.00	18.88	2.00	0.00	0.00	0.01	0.00
18.89	2.00	0.00	0.00	0.01	0.00	18.90	2.00	0.00	0.00	0.01	0.00
18.91	2.00	0.00	0.00	0.01	0.00	18.92	2.00	0.00	0.00	0.01	0.00
18.93	2.00	0.00	0.00	0.01	0.00	18.94	2.00	0.00	0.00	0.01	0.00
18.95	2.00	0.00	0.00	0.01	0.00	18.96	2.00	0.00	0.00	0.01	0.00
18.97	2.00	0.00	0.00	0.01	0.00	18.98	2.00	0.00	0.00	0.01	0.00
18.99	2.00	0.00	0.00	0.01	0.00	19.00	2.00	0.00	0.00	0.01	0.00
19.01	2.00	0.00	0.00	0.01	0.00	19.02	2.00	0.00	0.00	0.01	0.00
19.03	2.00	0.00	0.00	0.01	0.00	19.04	2.00	0.00	0.00	0.01	0.00
19.05	2.00	0.00	0.00	0.01	0.00	19.06	2.00	0.00	0.00	0.01	0.00
19.07	2.00	0.00	0.00	0.01	0.00	19.08	2.00	0.00	0.00	0.01	0.00
19.09	1.98	0.00	0.00	0.01	0.00	19.10	1.92	0.00	0.00	0.01	0.00
19.11	1.90	0.00	0.00	0.01	0.00	19.12	1.89	0.00	0.00	0.01	0.00
19.13	1.89	0.00	0.00	0.01	0.00	19.14	2.00	0.00	0.00	0.01	0.00
19.15	2.00	0.00	0.00	0.01	0.00	19.16	2.00	0.00	0.00	0.01	0.00
19.17	2.00	0.00	0.00	0.01	0.00	19.18	2.00	0.00	0.00	0.01	0.00
19.19	2.00	0.00	0.00	0.01	0.00	19.20	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}	Depth (m)	FS	m(FS)	H_i*m(FS)	d_z	LPI_{ISH}
19.21	2.00	0.00	0.00	0.01	0.00	19.22	2.00	0.00	0.00	0.01	0.00
19.23	2.00	0.00	0.00	0.01	0.00	19.24	2.00	0.00	0.00	0.01	0.00
19.25	2.00	0.00	0.00	0.01	0.00	19.26	2.00	0.00	0.00	0.01	0.00
19.27	2.00	0.00	0.00	0.01	0.00	19.28	2.00	0.00	0.00	0.01	0.00
19.29	2.00	0.00	0.00	0.01	0.00	19.30	2.00	0.00	0.00	0.01	0.00
19.31	2.00	0.00	0.00	0.01	0.00	19.32	2.00	0.00	0.00	0.01	0.00
19.33	2.00	0.00	0.00	0.01	0.00	19.34	2.00	0.00	0.00	0.01	0.00
19.35	2.00	0.00	0.00	0.01	0.00	19.36	2.00	0.00	0.00	0.01	0.00
19.37	2.00	0.00	0.00	0.01	0.00	19.38	2.00	0.00	0.00	0.01	0.00
19.39	2.00	0.00	0.00	0.01	0.00	19.40	2.00	0.00	0.00	0.01	0.00
19.41	2.00	0.00	0.00	0.01	0.00	19.42	2.00	0.00	0.00	0.01	0.00
19.43	2.00	0.00	0.00	0.01	0.00	19.44	2.00	0.00	0.00	0.01	0.00
19.45	2.00	0.00	0.00	0.01	0.00	19.46	2.00	0.00	0.00	0.01	0.00
19.47	2.00	0.00	0.00	0.01	0.00	19.48	2.00	0.00	0.00	0.01	0.00
19.49	2.00	0.00	0.00	0.01	0.00	19.50	2.00	0.00	0.00	0.01	0.00
19.51	2.00	0.00	0.00	0.01	0.00	19.52	2.00	0.00	0.00	0.01	0.00
19.53	2.00	0.00	0.00	0.01	0.00	19.54	2.00	0.00	0.00	0.01	0.00
19.55	2.00	0.00	0.00	0.01	0.00	19.56	2.00	0.00	0.00	0.01	0.00
19.57	2.00	0.00	0.00	0.01	0.00	19.58	2.00	0.00	0.00	0.01	0.00
19.59	2.00	0.00	0.00	0.01	0.00	19.60	2.00	0.00	0.00	0.01	0.00
19.61	2.00	0.00	0.00	0.01	0.00	19.62	2.00	0.00	0.00	0.01	0.00
19.63	2.00	0.00	0.00	0.01	0.00	19.64	2.00	0.00	0.00	0.01	0.00
19.65	2.00	0.00	0.00	0.01	0.00	19.66	2.00	0.00	0.00	0.01	0.00
19.67	2.00	0.00	0.00	0.01	0.00	19.68	2.00	0.00	0.00	0.01	0.00
19.69	2.00	0.00	0.00	0.01	0.00	19.70	2.00	0.00	0.00	0.01	0.00
19.71	2.00	0.00	0.00	0.01	0.00	19.72	2.00	0.00	0.00	0.01	0.00
19.73	2.00	0.00	0.00	0.01	0.00	19.74	2.00	0.00	0.00	0.01	0.00
19.75	2.00	0.00	0.00	0.01	0.00	19.76	2.00	0.00	0.00	0.01	0.00
19.77	2.00	0.00	0.00	0.01	0.00	19.78	2.00	0.00	0.00	0.01	0.00
19.79	2.00	0.00	0.00	0.01	0.00	19.80	2.00	0.00	0.00	0.01	0.00
19.81	2.00	0.00	0.00	0.01	0.00	19.82	2.00	0.00	0.00	0.01	0.00
19.83	2.00	0.00	0.00	0.01	0.00	19.84	2.00	0.00	0.00	0.01	0.00
19.85	2.00	0.00	0.00	0.01	0.00	19.86	2.00	0.00	0.00	0.01	0.00
19.87	2.00	0.00	0.00	0.01	0.00	19.88	2.00	0.00	0.00	0.01	0.00
19.89	2.00	0.00	0.00	0.01	0.00	19.90	2.00	0.00	0.00	0.01	0.00
19.91	2.00	0.00	0.00	0.01	0.00	19.92	2.00	0.00	0.00	0.01	0.00
19.93	2.00	0.00	0.00	0.01	0.00	19.94	2.00	0.00	0.00	0.01	0.00
19.95	2.00	0.00	0.00	0.01	0.00	19.96	2.00	0.00	0.00	0.01	0.00
19.97	2.00	0.00	0.00	0.01	0.00	19.98	2.00	0.00	0.00	0.01	0.00
19.99	2.00	0.00	0.00	0.01	0.00	20.00	2.00	0.00	0.00	0.01	0.00

Overall liquefaction potential: 0.00

LPI_{ISH} > 5.0 - Liquefaction manifestation is expected

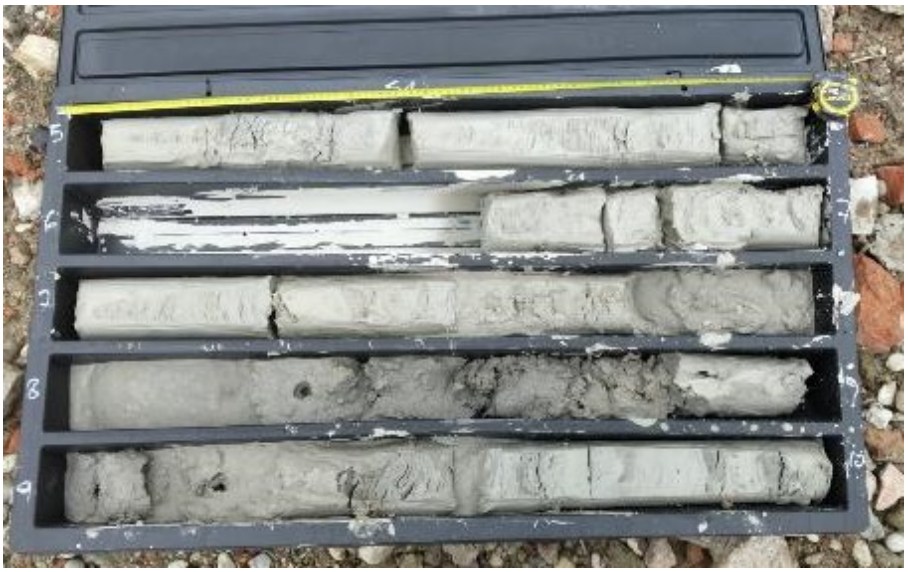
Abbreviations

FS: Calculated factor of safety for test point
d_z: Layer thickness (m)
LPI: Liquefaction potential index value for test point

ALLEGATO 3: SONDAGGIO A CAROTAGGIO CONTINUO – STRATIGRAFIA, FOTO CASSETTE E CAMPIONI GEOTECNICI



Sondaggio S1- CASSETTA 1 (0 – 5 m)



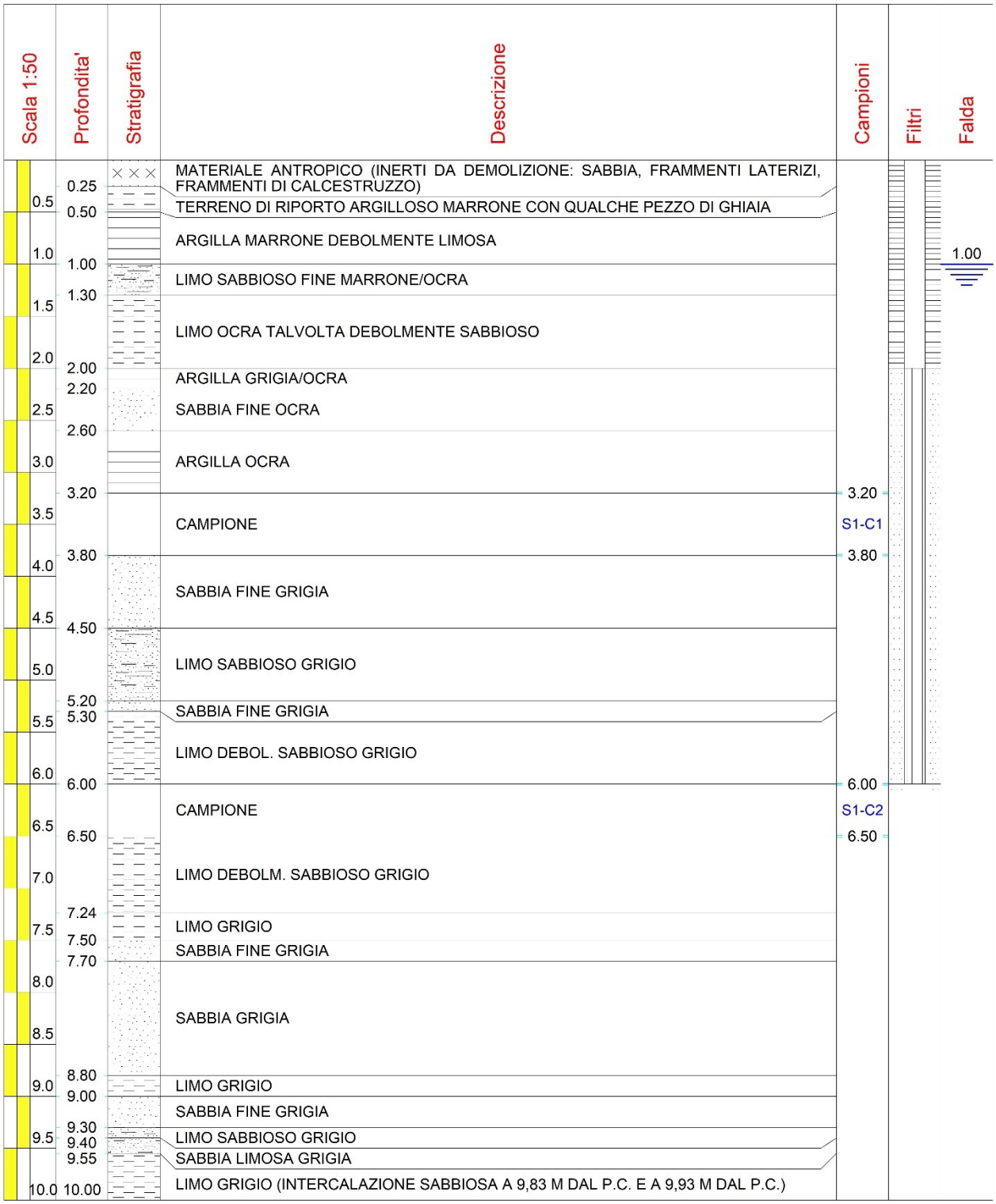
Sondaggio S1- CASSETTA 2 (5 – 10 m)





PIEZOMETRO S1-PZ (prof. 6 m dal p.c., filtri da -2 m a -6 m)

Cantiere EX-CONFIGLIACHI (Via Guido Reni, Padova)	N. sondaggio Provincia di Padova
Committente	Scala sondaggio
Perforatore Sondaggio a carotaggio continuo	Geologo S1/PZ
Coord. 1:50	Quota (p.c.) Segato E. - Lovison L.
Metodo perf.	Data ultimazione 26/02/2026



GEODATA S.r.l. Unipersonale
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PROVE GEOTECNICHE DI LABORATORIO
E CONTROLLI GEOTECNICI IN SITO

Laboratorio autorizzato dal Ministero delle Infrastrutture e dei Trasporti ai sensi dell'art. 59 del D.P.R. 380/2001

Verbale di accettazione n.	08326 del 06/03/26
Committente:	Provincia di Padova - AREA TECNICA SETTORE EDILIZIA E IMPIANTI Piazza Antenore 3 codice fiscale n. 80006510285 P.IVA 00700440282
Cantiere:	Area Ex Configliachi - Via Guido Reni Arcella – Padova CIG: B97548B6BE
Tipologia di prove richieste:	Analisi di laboratorio
Data ricevimento campioni:	**06/03/26**
Prove di laboratorio richieste da:	Dott.ssa Elisa Segato – Geodelta SRL STP

Data esecuzione prove	10-23/03/26	Data emissione documento	23/03/26

Per Vostro incarico, ricevuto tramite la Dott.ssa Elisa Segato della Geodelta SRL STP, abbiamo eseguito analisi di laboratorio su n. 2 campioni indisturbati provenienti dal cantiere in oggetto e consegnati presso il nostro laboratorio in data 06/03/26.

Come richiesto dalla Dott.ssa Elisa Segato, sui campioni consegnati sono state eseguite le seguenti prove:

- Classificazione geotecnica visiva con il rilievo della resistenza al penetrometro tascabile ed al Torvane
- Contenuto naturale d'acqua
- Massa volumica naturale
- Massa volumica dei granuli solidi
- Determinazione dei limiti di Atterberg (WL, WP, IP)
- Analisi granulometrica completa

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– Prova di consolidazione edometrica

I risultati delle prove eseguite sono riportati nei certificati di prova allegati.

CERTIFICATI DI PROVA EMESSI

Identificativo campione/prova	Tipo di prova	n. certificato
S1/CI1	Classificazione visiva	168001
	Contenuto d'acqua (UNI CEN ISO/TS 17892-1)	168002
	Massa volumica naturale (UNI CEN ISO/TS 17892-2)	168003
	Massa volumica granuli solidi (UNI CEN ISO/TS 17892-3)	168004
	Limiti di Atterberg (UNI CEN ISO/TS 17892-12)	168005
	Analisi granulometrica (UNI CEN ISO/TS 17892-4)	168006
	Prova edometrica (ASTM D 2435)	168007
S1/CI2	Classificazione visiva	168008
	Contenuto d'acqua (UNI CEN ISO/TS 17892-1)	168009
	Massa volumica naturale (UNI CEN ISO/TS 17892-2)	168010
	Massa volumica granuli solidi (UNI CEN ISO/TS 17892-3)	168011
	Limiti di Atterberg (UNI CEN ISO/TS 17892-12)	168012
	Analisi granulometrica (UNI CEN ISO/TS 17892-4)	168013
	Prova edometrica (ASTM D 2435)	168014

Ponte San Nicolò, 23 Marzo 2026

Dott. Geol. Pietro Daminato
Direttore Laboratorio

GEODATA
PROVE GEOTECNICHE DI LABORATORIO
E CONTROLLI GEOTECNICI IN SITO

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COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI

CANTIERE: Area Ex Configliachi - Via Guido Reni - Arcella - Padova

COMMESSA n. **08326** del **06/03/26**

RIASSUNTO DELLE PROVE ESEGUITE

Tipo di prova	sondaggio	S1					
	indisturbato	CI1	CI2				
	rimaneggiato						
	profondità	3,20-3,80	6,00-6,50				
Classificazione geotecnica		limo con argilla grigio	limo con argilla grigio				
Pocket Penetrometer	P.P. kPa	235-245	49-137				
Torvane	Torv. kPa	60	22-33				
Contenuto naturale d'acqua	W %	23,7	23,5				
Massa volumica naturale	γ kN/m^3	20,19	20,73				
Massa volumica dei granuli solidi	γ_s kN/m^3	27,15	27,04				
Limiti di Atterberg	WL %	38	39				
	WP %	22	21				
	IP %	16	18				
Analisi granulometrica	ciottoli %	0,00	0,00				
	ghiaia %	0,00	0,00				
	sabbia %	1,16	0,65				
	limo %	68,52	57,15				
	argilla %	30,32	42,20				
Classificazione UNI 11531-1	classe	A6	A6				
	Ig	10	11				
Prova di compressione edometrica	σ kPa	100	100				
	c_v m^2/sec	9,38E-08	3,93E-08				
	k_{ED} m/sec	2,36E-10	1,25E-10				
Prova di compressione edometrica	σ kPa	200	200				
	c_v m^2/sec	7,52E-08	6,86E-08				
	k_{ED} m/sec	1,10E-10	1,11E-10				

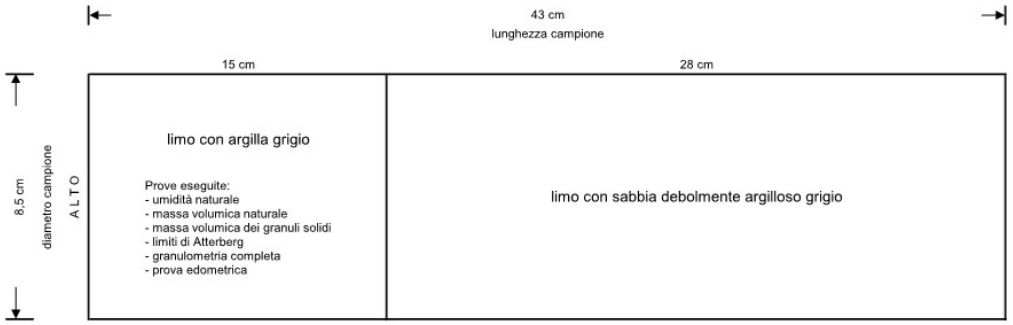
CERTIFICATO N° 168001 pag. 1/1 emesso il 23/03/26

Verbale di Accettazione n. 08326 data ricevimento campione 06/03/26 data prova 10/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI Sond.: **S1** Prof.: **3,20-3,80**

CANTIERE: Area Ex Configliachi - Via Guido Reni - Arcella - Padova Campione: **CI1**

CLASSIFICAZIONE GEOTECNICA VISIVA CAMPIONE INDISTURBATO



P.P.	kPa	235-245	216	177
TORV.	kPa	60	35	21

note:

QUALITA' CAMPIONE: [X] buona [ ] sufficiente [ ] scadente

Sperimentatore
Dott. L. Stimamiglio

Direttore Laboratorio
Dott. Pietro Daminato

Documento firmato digitalmente ai sensi della normativa vigente

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PROVE GEOTECNICHE DI LABORATORIO E CONTROLLI GEOTECNICI IN SITO

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CERTIFICATO N°	**168002**	pag.	1/1	emesso il	23/03/26
Verbale di Accettazione n.	08326	data ricevimento campione	06/03/26	data prova	10/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI

CANTIERE: Area Ex Configliachi - Via Guido Reni - Arcella - Padova

Sond.: **S1** Campione: **CI1** Prof.: **3,20-3,80**

CONTENUTO D'ACQUA

(norma: UNI CEN ISO/TS 17892-1)

Classificazione geotecnica: limo con argilla grigio

	prov. 1		prov. 2	
id.tara		117		116
massa umida lorda	g	86,69	g	78,81
massa secca lorda	g	76,79	g	70,31
tara	g	35,03	g	34,55
W%		**23,707**	W%	**23,770**

media

W % **23,7**

note:

Sperimentatore
Dott. L. Stimamiglio

Direttore Laboratorio
Dott. Pietro Daminato

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Laboratorio autorizzato dal Ministero delle Infrastrutture e dei Trasporti ai sensi dell'art. 59 del D.P.R. 380/2001

CERTIFICATO N°	**168003**	pag.	1/1	emesso il	23/03/26
Verbale di Accettazione n.	08326	data ricevimento campione	06/03/26	data prova	10/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI

CANTIERE: Area Ex Configliachi - Via Guido Reni - Arcella - Padova

Sond.: **S1** Camp.: **CI1** Prof.: **3,20-3,80**

MASSA VOLUMICA

(norma: UNI CEN ISO/TS 17892-2)

Classificazione geotecnica: limo con argilla grigio

		prov. 1		prov. 2
diametro	mm	71,4	mm	71,4
altezza	mm	20,0	mm	20,0
massa lorda	g	282,60	g	284,02
tara	g	118,47	g	118,47
massa netta	g	164,13	g	165,55
	ρ Mg/m3	**2,050**	ρ Mg/m3	**2,067**
	ρ kN/m3	**20,10**	ρ kN/m3	**20,27**

	media
ρ Mg/m^3	**2,060**
ρ kN/m^3	**20,19**

note:
eseguito con il metodo della fustella tarata su campione indisturbato

Sperimentatore
Dott. L. Stimamiglio

Direttore Laboratorio
Dott. Pietro Daminato

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CERTIFICATO N°	**168004**	pag.	1/1	emesso il	23/03/26
Verbale di Accettazione n.	08326	data ricevimento campione	06/03/26	data prova	16/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI

CANTIERE: Area Ex Configliachi - Via Guido Reni - Arcella - Padova

Sond.: **S1** Camp.: **CI1** Prof.: **3,20-3,80**

MASSA VOLUMICA DEI GRANULI SOLIDI

(norma: UNI CEN ISO/TS 17892-3)

Classificazione geotecnica: limo con argilla grigio

		prov. 1		prov. 2
n. picnometro		1		3
m2 - massa pic. + campione	g	70,401	g	72,159
m3 - massa pic.+acqua+terreno	g	163,880	g	165,204
temperatura prova	°C	25,0	°C	25,0
ρ_s Mg/m3		**2,768**	ρ_s Mg/m3	**2,769**
ρ_s kN/m3		**27,148**	ρ_s kN/m3	**27,152**

	media
ρ_s Mg/m^3	**2,770**
ρ_s kN/m^3	**27,15**

note:

Sperimentatore
Dott. L. Stimamiglio

Direttore Laboratorio
Dott. Pietro Daminato

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CERTIFICATO N° 168005 pag. 1/1 emesso il 23/03/26

Verbale di Accettazione n. 08326 data ricevimento campione 06/03/26 data prova 20/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI

CANTIERE: Area Ex Configliachi - Via Guido Reni - Arcella - Padova

Sond.: **S1** Campione: **CI1** Prof.: **3,20-3,80**

LIMITI DI ATTERBERG

(norma: UNI CEN ISO/TS 17892-12)

Classificazione geotecnica: limo con argilla grigio

Provino: terreno naturale

Medoto di prova WL: Cucchiaio di Casagrande

LIMITE DI LIQUIDITA'		prov. 1	prov. 2	prov. 3	
id. tara		30	34	52	
massa umida lorda	g	33,423	32,022	34,088	
massa secca lorda	g	27,636	26,789	28,482	
tara	g	12,895	12,730	13,171	
numero colpi		16	29	35	
	WL%	**39,26**	**37,22**	**36,61**	**WL % 38**

LIMITE DI PLASTICITA'		prov. 1	prov. 2	prov. 3	
id. tara		23	37	68	
massa umida lorda	g	12,628	13,395	14,180	
massa secca lorda	g	12,339	13,079	13,837	
tara	g	11,048	11,652	12,279	media
	WP%	**22,39**	**22,14**	**22,02**	**WP % 22**

INDICE DI PLASTICITA' **IP 16**

w%	Indice di consistenza (I_C)
23,7	0,9

cucchiaio Casagrande Controls n° 87121946

note:

Sperimentatore
Perito A. Fiore

Direttore Laboratorio
Dott. Pietro Daminato

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CERTIFICATO N° 168006	pag. 1/1	emesso il 23/03/26
Verbale di Accettazione n. 08326	data ricevimento campione 06/03/26	data prova 13/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI

CANTIERE: Area Ex Configliachi - Via Guido Reni - Arcella - Padova

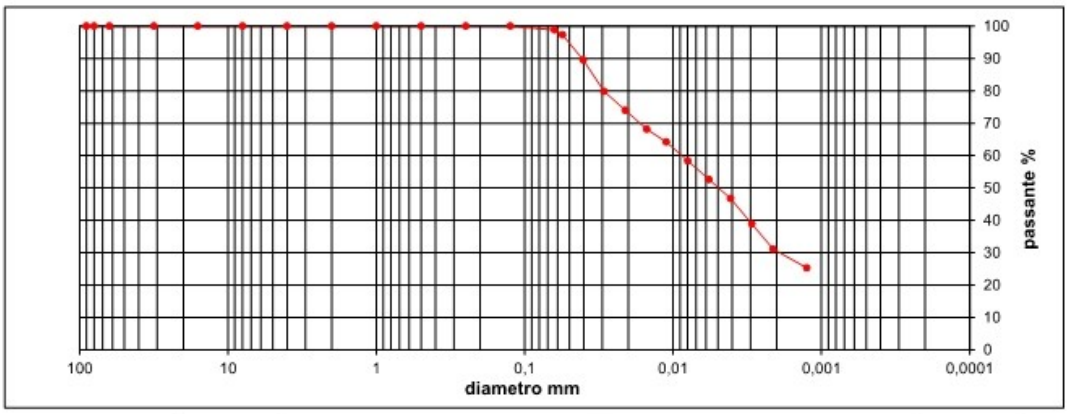
Sond.: **S1** Campione: **CI1** Prof.: **3,20-3,80**

ANALISI GRANULOMETRICA

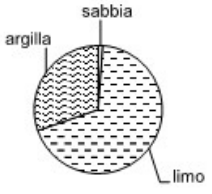
(norma: UNI EN ISO 17892-1)

setaccio	diametro mm	trattenuto %	passante %
125	125,000	0,00	100,00
90	90,000	0,00	100,00
80	80,000	0,00	100,00
63	63,000	0,00	100,00
31,5	31,500	0,00	100,00
16	16,000	0,00	100,00
8	8,000	0,00	100,00
4	4,000	0,00	100,00
2	2,000	0,00	100,00
1	1,000	0,00	100,00
0,5	0,500	0,00	100,00
0,25	0,250	0,00	100,00
0,125	0,125	0,00	100,00
0,063	0,063	1,16	98,84

setaccio	diametro mm	trattenuto %	passante %
	0,0557		97,31
	0,0403		89,53
	0,0292		79,79
	0,0210		73,96
	0,0151		68,12
	0,0111		64,22
	0,0080		58,39
	0,0057		52,55
	0,0041		46,71
	0,0029		38,92
	0,0021		31,14
	0,0013		25,30



ciottoli	ghiaia			sabbia			limo	argilla
	grossa	media	fine	grossa	media	fine		
> 60 mm	60 - 20 mm	20 - 6 mm	6 - 2 mm	2 - 0.6 mm	0.6 - 0.2 mm	0.2 - 0.063 mm	0.063-0.002 mm	< 0.002 mm
0,00	0,00	0,00	0,00	0,00	0,00	1,16	68,52	30,32



classificazione geotecnica: limo con argilla grigio

UNI 11531-1 A6 Ig 10 USCS - - -

Sperimentatore
Perito A. Fiore

Direttore Laboratorio
Dott. Pietro Daminato

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PROVE GEOTECNICHE DI LABORATORIO
E CONTROLLI GEOTECNICI IN SITO

Laboratorio autorizzato dal Ministero delle Infrastrutture e dei Trasporti ai sensi dell'art. 59 del D.P.R. 380/2001

CERTIFICATO N°	**168007**	pag. 1/5		emesso il	23/03/26
Verbale di Accettazione n.	08326	data ricevimento campione	06/03/26	data prova	10/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI

CANTIERE: Area Ex Configliachi - Via Guido Reni - Arcella - Padova

Sond.: **S1** Campione: **CI1** Prof.: **3,20-3,80**

PROVA DI CONSOLIDAZIONE EDOMETRICA

(norma: ASTM D 2435)

EDOMETRO N° **1** - comparatore n° CD 1

area =	4,0E+03	mm^2	γ in. =	20,12	kN/m^3	tara=	35,92	g
h iniziale=	20,0	mm	γs =	27,15	kN/m^3	wi =	23,7	%
volume=	8,0E+04	mm^3	m. umida I. =	195,48	g	wf =	20,2	%
m.umida n. =	164,13	g	m. secca I. =	168,65	g	hs =	1,199	

P kPa	cedimenti mm	e	def %	mv kPa^{-1}	E kPa
0,00	0,000	0,669	0,00		
25,0	0,602	0,618	3,01	1,24E-03	806
50,0	0,840	0,599	4,20	4,72E-04	2116
100,0	1,070	0,579	5,35	2,52E-04	3973
200,0	1,346	0,556	6,73	1,47E-04	6815
400,0	1,642	0,532	8,21	7,77E-05	12867
800,0	2,031	0,499	10,16	5,44E-05	18370
1600,0	2,418	0,467	12,09	2,70E-05	37075
800,0	2,336	0,474	11,68	5,95E-06	
100,0	1,984	0,503	9,92	2,78E-05	
12,5	1,618	0,534	8,09	2,33E-04	

classificazione geotecnica: limo con argilla grigio

note:

Sperimentatore
Dott. L. Stimamiglio

Direttore Laboratorio:
Dott. Pietro Daminato

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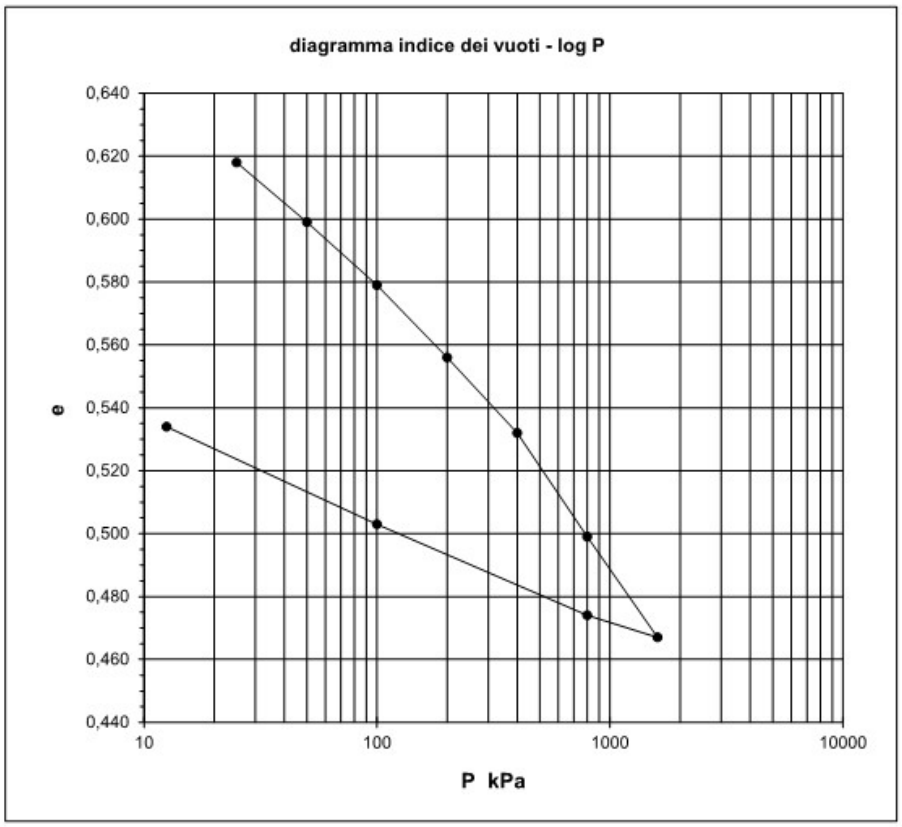
CERTIFICATO N°	**168007**	pag. 2/5		emesso il	23/03/26
Verbale di Accettazione n.	08326	data ricevimento campione	06/03/26	data prova	10/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI

CANTIERE: Area Ex Configliachi - Via Guido Reni - Arcella - Padova

Sond.: **S1** Campione: **CI1** Prof.: **3,20-3,80**

EDOMETRO N° **1** - comparatore n° CD 1



Cr = 0,0631 Cc = 0,1063 Cs = 0,0321

Note: il Cr è stato calcolato nell'intervallo 25-50 kPa
il Cc è stato calcolato nell'intervallo 800-1600 kPa
il Cs è stato calcolato nell'intervallo 800-100 kPa

Sperimentatore
Dott. L. Stimamiglio

Direttore Laboratorio:
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CERTIFICATO N° 168007		pag. 3/5		emesso il	23/03/26
Verbale di Accettazione n.	08326	data ricevimento campione	06/03/26	data prova	10/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI

CANTIERE: Area Ex Configliachi - Via Guido Reni - Arcella - Padova

Sond.: **S1** Campione: **CI1** Prof.: **3,20-3,80**

DATI CEDIMENTO-TEMPO

Tempo	25 kPa	50 kPa	100 kPa	200 kPa	400 kPa	800 kPa	1600 kPa	800 kPa	100 kPa	12,5 kPa
s	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm
5	0,240	0,642	0,816	1,086	1,427	1,757	2,158	2,394	2,315	1,953
15	0,258	0,646	0,832	1,103	1,432	1,773	2,175	2,351	2,162	1,924
29	0,272	0,649	0,843	1,117	1,436	1,784	2,189	2,348	2,135	1,909
60	0,291	0,651	0,856	1,136	1,441	1,797	2,208	2,345	2,105	1,885
135	0,319	0,654	0,870	1,159	1,447	1,811	2,231	2,343	2,067	1,849
240	0,343	0,658	0,881	1,175	1,453	1,822	2,247	2,342	2,042	1,815
540	0,374	0,661	0,896	1,199	1,461	1,837	2,271	2,341	2,015	1,757
960	0,397	0,664	0,905	1,217	1,467	1,846	2,289	2,340	2,006	1,719
1500	0,412	0,667	0,914	1,229	1,475	1,855	2,301	2,339	2,000	1,692
2160	0,424	0,670	0,921	1,239	1,481	1,862	2,311	2,339	1,998	1,675
3840	0,443	0,678	0,932	1,254	1,491	1,873	2,326	2,338	1,993	1,657
5430	0,454	0,684	0,940	1,262	1,498	1,881	2,334	2,338	1,991	1,649
7260	0,464	0,691	0,947	1,269	1,506	1,888	2,341	2,337	1,989	1,644
14400	0,488	0,712	0,968	1,286	1,529	1,909	2,358	2,336	1,984	1,634
29040	0,523	0,747	1,003	1,306	1,566	1,944	2,378			1,627
57600	0,574	0,803	1,045	1,329	1,610	2,001	2,401			1,623
86640	0,602	0,840	1,070	1,346	1,642	2,031	2,418			1,618

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CERTIFICATO N° 168007	pag. 4/5	emesso il 23/03/26
Verbale di Accettazione n. 08326	data ricevimento campione 06/03/26	data prova 10/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI

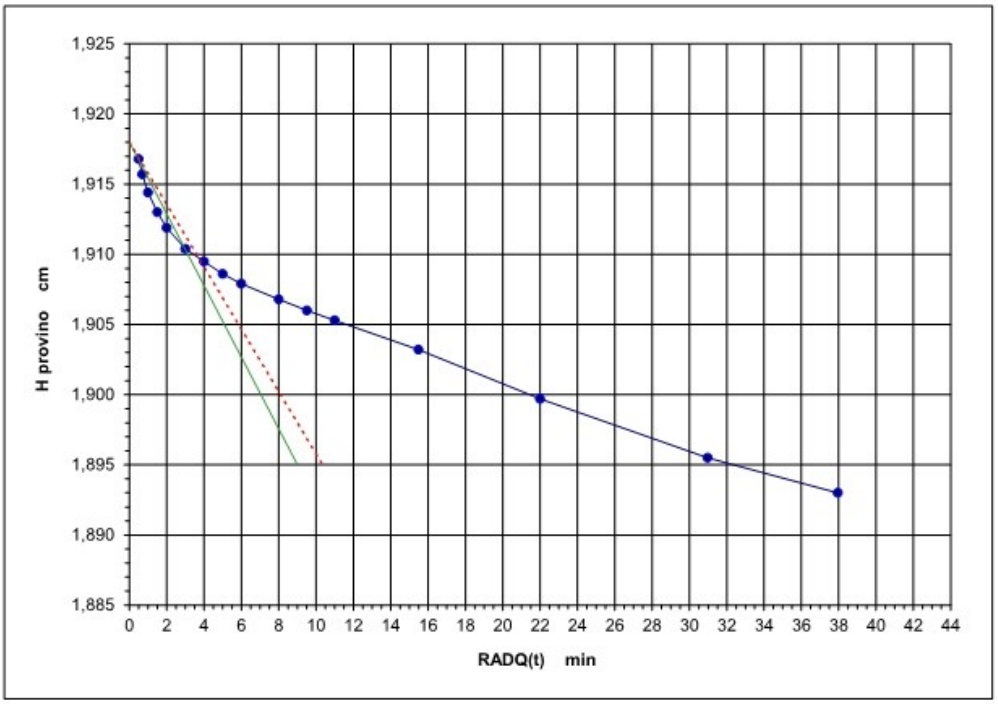
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Sond.: **S1** Campione: **CI1** Prof.: **3,20-3,80**

PROVA DI CONSOLIDAZIONE EDOMETRICA

Determinazione del coefficiente di consolidazione Cv con il metodo di Taylor

Pressione verticale	**100**	kPa



cv = 9,38E-08 m^2/s K_{ED} = 2,36E-10 m/s

Sperimentatore
Dott. L. Stimamiglio

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CERTIFICATO N° 168007	pag. 5/5	emesso il 23/03/26
Verbale di Accettazione n. 08326	data ricevimento campione 06/03/26	data prova 10/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI

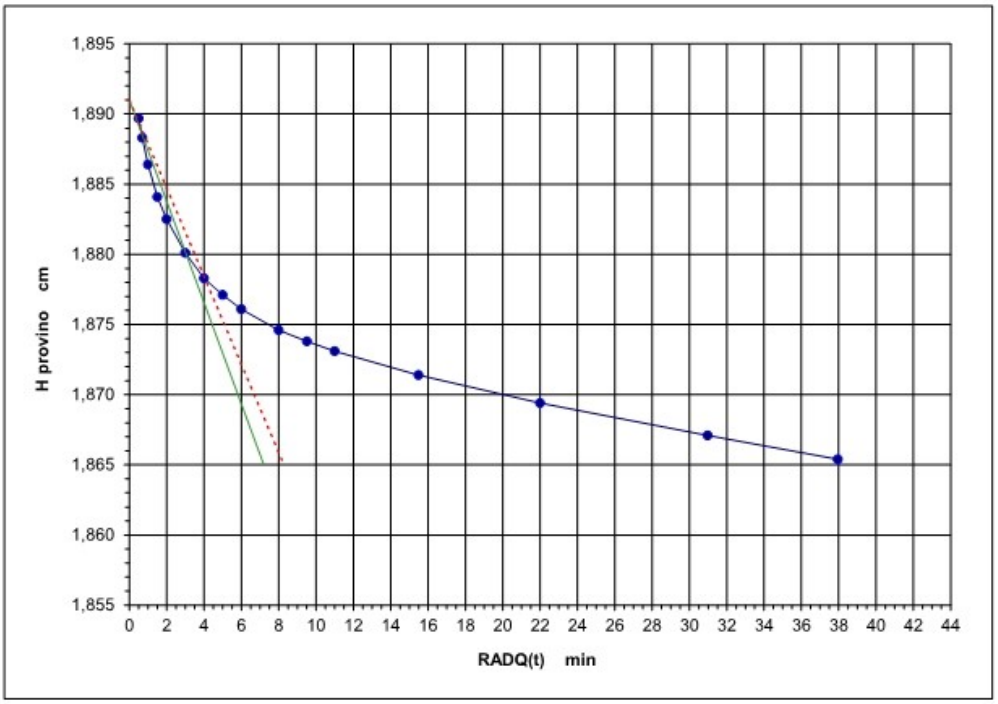
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Sond.: **S1** Campione: **CI1** Prof.: **3,20-3,80**

PROVA DI CONSOLIDAZIONE EDOMETRICA

Determinazione del coefficiente di consolidazione Cv con il metodo di Taylor

Pressione verticale	**200**	kPa



cv = 7,52E-08 m^2/s K_{ED} = 1,10E-10 m/s

Sperimentatore
Dott. L. Stimamiglio

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CERTIFICATO N°	168008	pag.	1/1	emesso il	23/03/26
Verbale di Accettazione n.	08326	data ricevimento campione	06/03/26	data prova	10/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI — Sond.: **S1** — Prof.: **6,00-6,50**

CANTIERE: Area Ex Configliachi - Via Guido Reni - Arcella - Padova — Campione: **CI2**

CLASSIFICAZIONE GEOTECNICA VISIVA CAMPIONE INDISTURBATO

49 cm
lunghezza campione

8,5 cm
diametro campione

ALTO

limo con argilla grigia

Prove eseguite:
- umidità naturale
- massa volumica naturale
- massa volumica dei granuli solidi
- limiti di Atterberg
- granulometria completa
- prova edometrica

BASSO

P.P.	kPa	49-59	137	69-88
TORV.	kPa	22	33	25

note:

QUALITA' CAMPIONE:
- [X] buona
- [ ] sufficiente
- [ ] scadente

Sperimentatore
Dott. L. Stimamiglio

Direttore Laboratorio
Dott. Pietro Daminato

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E CONTROLLI GEOTECNICI IN SITO

Laboratorio autorizzato dal Ministero delle Infrastrutture e dei Trasporti ai sensi dell'art. 59 del D.P.R. 380/2001

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CERTIFICATO N°	**168009**	pag.	1/1	emesso il	23/03/26
Verbale di Accettazione n.	08326	data ricevimento campione	06/03/26	data prova	10/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI

CANTIERE: Area Ex Configliachi - Via Guido Reni - Arcella - Padova

Sond.: **S1** Campione: **CI2** Prof.: **6,00-6,50**

CONTENUTO D'ACQUA

(norma: UNI CEN ISO/TS 17892-1)

Classificazione geotecnica: limo con argilla grigia

	prov. 1		prov. 2	
id.tara		111		131
massa umida lorda	g	98,17	g	76,45
massa secca lorda	g	86,30	g	68,43
tara	g	33,96	g	35,32
W%		**22,679**	W%	**24,222**

media

W % **23,5**

note:

Sperimentatore
Dott. L. Stimamiglio

Direttore Laboratorio
Dott. Pietro Daminato

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CERTIFICATO N°	**168010**	pag.	1/1	emesso il	23/03/26
Verbale di Accettazione n.	08326	data ricevimento campione	06/03/26	data prova	10/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI

CANTIERE: Area Ex Configliachi - Via Guido Reni - Arcella - Padova

Sond.: **S1** Camp.: **CI2** Prof.: **6,00-6,50**

MASSA VOLUMICA

(norma: UNI CEN ISO/TS 17892-2)

Classificazione geotecnica: limo con argilla grigia

		prov. 1		prov. 2
diametro	mm	71,4	mm	71,4
altezza	mm	20,0	mm	20,0
massa lorda	g	285,22	g	287,03
tara	g	116,85	g	116,85
massa netta	g	168,37	g	170,18
ρ Mg/m3		**2,103**	ρ Mg/m3	**2,125**
ρ kN/m3		**20,62**	ρ kN/m3	**20,84**

	media
ρ Mg/m^3	**2,110**
ρ kN/m^3	**20,73**

note:
eseguito con il metodo della fustella tarata su campione indisturbato

Sperimentatore
Dott. L. Stimamiglio

Direttore Laboratorio
Dott. Pietro Daminato

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CERTIFICATO N°	**168011**	pag.	1/1	emesso il	23/03/26
Verbale di Accettazione n.	08326	data ricevimento campione	06/03/26	data prova	16/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI

CANTIERE: Area Ex Configliachi - Via Guido Reni - Arcella - Padova

Sond.: **S1** Camp.: **CI2** Prof.: **6,00-6,50**

MASSA VOLUMICA DEI GRANULI SOLIDI

(norma: UNI CEN ISO/TS 17892-3)

Classificazione geotecnica: limo con argilla grigia

		prov. 1		prov. 2
n. picnometro		4		6
m2 - massa pic. + campione	g	72,583	g	74,289
m3 - massa pic.+acqua+terreno	g	164,001	g	167,035
temperatura prova	°C	25,0	°C	25,0
ρ_s Mg/m3		**2,756**	ρ_s Mg/m3	**2,758**
ρ_s kN/m3		**27,030**	ρ_s kN/m3	**27,047**

	media
ρ_s Mg/m^3	**2,760**
ρ_s kN/m^3	**27,04**

note:

Sperimentatore
Dott. L. Stimamiglio

Direttore Laboratorio
Dott. Pietro Daminato

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CERTIFICATO N°	**168012**	pag.	1/1	emesso il	23/03/26
Verbale di Accettazione n.	08326	data ricevimento campione	06/03/26	data prova	20/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI

CANTIERE: Area Ex Configliachi - Via Guido Reni - Arcella - Padova

Sond.: **S1** Campione: **CI2** Prof.: **6,00-6,50**

LIMITI DI ATTERBERG

(norma: UNI CEN ISO/TS 17892-12)

Classificazione geotecnica: limo con argilla grigia

Provino: terreno naturale

Medoto di prova WL: Cucchiaio di Casagrande

LIMITE DI LIQUIDITA'		prov. 1	prov. 2	prov. 3	
id. tara		31	79	28	
massa umida lorda	g	32,554	31,633	35,669	
massa secca lorda	g	26,769	26,106	30,190	
tara	g	12,975	11,998	15,370	
numero colpi		15	24	35	
	WL%	**41,94**	**39,18**	**36,97**	**WL % 39**

LIMITE DI PLASTICITA'		prov. 1	prov. 2	prov. 3	
id. tara		8	10	11	
massa umida lorda	g	14,396	14,754	14,403	
massa secca lorda	g	14,101	14,457	14,094	
tara	g	12,709	13,044	12,570	media
	WP%	**21,19**	**21,02**	**20,28**	**WP % 21**

INDICE DI PLASTICITA' **IP 18**

w%	Indice di consistenza (I_C)
23,5	0,9

cucchiaio Casagrande Controls n° 87121946

note:

Sperimentatore
Perito A. Fiore

Direttore Laboratorio
Dott. Pietro Daminato

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info@geodatapadova.it - PEC: geodatapadova@pec.it - www.geodatapadova.it

PROVE GEOTECNICHE DI LABORATORIO
E CONTROLLI GEOTECNICI IN SITO

Laboratorio autorizzato dal Ministero delle Infrastrutture e dei Trasporti ai sensi dell'art. 59 del D.P.R. 380/2001

CERTIFICATO N°	**168013**	pag.	1/1	emesso il	23/03/26
Verbale di Accettazione n.	08326	data ricevimento campione	06/03/26	data prova	13/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI

CANTIERE: Area Ex Configliachi - Via Guido Reni - Arcella - Padova

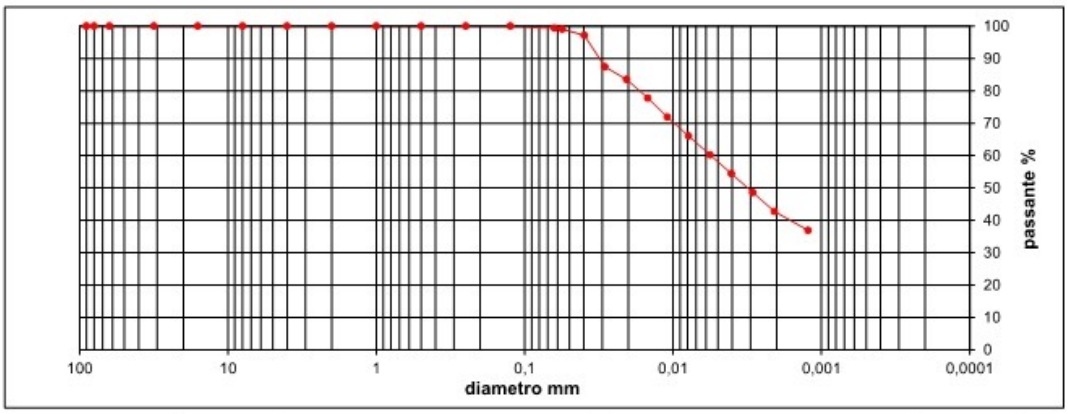
Sond.: **S1** Campione: **CI2** Prof.: **6,00-6,50**

ANALISI GRANULOMETRICA

(norma: UNI EN ISO 17892-1)

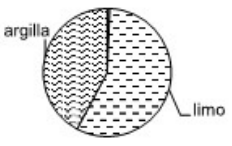
setaccio	diametro mm	trattenuto %	passante %
125	125,000	0,00	100,00
90	90,000	0,00	100,00
80	80,000	0,00	100,00
63	63,000	0,00	100,00
31,5	31,500	0,00	100,00
16	16,000	0,00	100,00
8	8,000	0,00	100,00
4	4,000	0,00	100,00
2	2,000	0,00	100,00
1	1,000	0,00	100,00
0,5	0,500	0,00	100,00
0,25	0,250	0,00	100,00
0,125	0,125	0,00	100,00
0,063	0,063	0,65	99,35

setaccio	diametro mm	trattenuto %	passante %
	0,0558		99,08
	0,0397		97,14
	0,0288		87,43
	0,0206		83,54
	0,0148		77,71
	0,0110		71,88
	0,0079		66,06
	0,0056		60,23
	0,0040		54,40
	0,0029		48,57
	0,0021		42,74
	0,0012		36,91



ciottoli	ghiaia			sabbia			limo	argilla
	grossa	media	fine	grossa	media	fine		
> 60 mm	60 - 20 mm	20 - 6 mm	6 - 2 mm	2 - 0.6 mm	0.6 - 0.2 mm	0.2 - 0.063 mm	0.063-0.002 mm	< 0.002 mm
0,00	0,00	0,00	0,00	0,00	0,00	0,65	57,15	42,20

classificazione geotecnica: limo con argilla grigia



UNI 11531-1 A6 Ig 11 USCS - - -

Sperimentatore
Perito A. Fiore

Direttore Laboratorio
Dott. Pietro Daminato

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Laboratorio autorizzato dal Ministero delle Infrastrutture e dei Trasporti ai sensi dell'art. 59 del D.P.R. 380/2001

CERTIFICATO N°	**168014**	pag. 1/5		emesso il	23/03/26
Verbale di Accettazione n.	08326	data ricevimento campione	06/03/26	data prova	10/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI

CANTIERE: Area Ex Configliachi - Via Guido Reni - Arcella - Padova

Sond.: **S1** Campione: **CI2** Prof.: **6,00-6,50**

PROVA DI CONSOLIDAZIONE EDOMETRICA

(norma: ASTM D 2435)

EDOMETRO N° **2** - comparatore n° CD 2

area =	4,0E+03	mm^2	γ in. =	20,64	kN/m^3	tara=	34,94	g
h iniziale=	20,0	mm	γs =	27,04	kN/m^3	wi =	22,1	%
volume=	8,0E+04	mm^3	m. umida l. =	195,91	g	wf =	16,7	%
m.umida n. =	168,37	g	m. secca l. =	172,86	g	hs =	1,250	

P kPa	cedimenti mm	e	def %	mv kPa^{-1}	E kPa
0,00	0,000	0,599	0,00		
25,0	0,675	0,545	3,38	1,37E-03	728
50,0	0,925	0,525	4,63	5,21E-04	1919
100,0	1,236	0,501	6,18	3,17E-04	3152
200,0	1,535	0,477	7,68	1,61E-04	6204
400,0	1,850	0,451	9,25	8,88E-05	11262
800,0	2,212	0,422	11,06	5,05E-05	19814
1600,0	2,615	0,390	13,08	2,84E-05	35150
800,0	2,607	0,391	13,04	8,99E-07	
100,0	2,377	0,409	11,89	1,84E-05	
12,5	2,082	0,433	10,41	1,93E-04	

classificazione geotecnica: limo con argilla grigia

note:

Sperimentatore
Dott. L. Stimamiglio

Direttore Laboratorio:
Dott. Pietro Daminato

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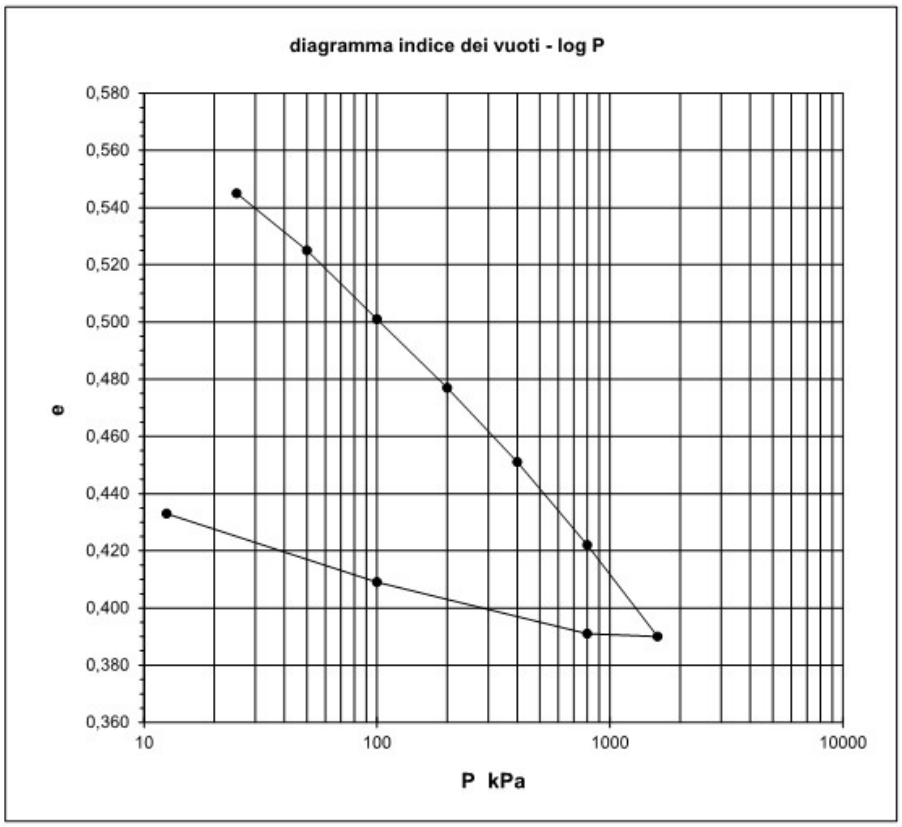
CERTIFICATO N°	**168014**	pag.	2/5	emesso il	23/03/26
Verbale di Accettazione n.	08326	data ricevimento campione	06/03/26	data prova	10/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI

CANTIERE: Area Ex Configliachi - Via Guido Reni - Arcella - Padova

Sond.: **S1** Campione: **CI2** Prof.: **6,00-6,50**

EDOMETRO N° **2** - comparatore n° CD 2



Cr = 0,0664 Cc = 0,1063 Cs = 0,0199

Note: il Cr è stato calcolato nell'intervallo 25-50 kPa
il Cc è stato calcolato nell'intervallo 800-1600 kPa
il Cs è stato calcolato nell'intervallo 800-100 kPa

Sperimentatore
Dott. L. Stimamiglio

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Dott. Pietro Daminato

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Laboratorio autorizzato dal Ministero delle Infrastrutture e dei Trasporti ai sensi dell'art. 59 del D.P.R. 380/2001

CERTIFICATO N° 168014	pag. 3/5	emesso il 23/03/26
Verbale di Accettazione n. 08326	data ricevimento campione 06/03/26	data prova 10/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI

CANTIERE: Area Ex Configliachi - Via Guido Reni - Arcella - Padova

Sond.: **S1** Campione: **CI2** Prof.: **6,00-6,50**

DATI CEDIMENTO-TEMPO

Tempo	25 kPa	50 kPa	100 kPa	200 kPa	400 kPa	800 kPa	1600 kPa	800 kPa	100 kPa	12,5 kPa
s	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm
5	0,116	0,723	1,029	1,264	1,643	1,941	2,331	2,647	2,591	2,353
15	0,138	0,728	1,039	1,284	1,650	1,961	2,367	2,617	2,487	2,324
29	0,159	0,731	1,046	1,299	1,655	1,976	2,395	2,615	2,466	2,310
60	0,193	0,734	1,055	1,319	1,662	1,996	2,435	2,613	2,444	2,293
135	0,254	0,738	1,065	1,346	1,670	2,023	2,481	2,613	2,422	2,264
240	0,315	0,741	1,077	1,366	1,676	2,043	2,509	2,612	2,409	2,239
540	0,432	0,747	1,097	1,393	1,688	2,070	2,541	2,611	2,398	2,198
960	0,518	0,751	1,114	1,410	1,696	2,087	2,559	2,611	2,394	2,169
1500	0,561	0,754	1,128	1,422	1,703	2,099	2,572	2,611	2,391	2,150
2160	0,581	0,758	1,142	1,432	1,709	2,109	2,581	2,610	2,389	2,138
3840	0,597	0,765	1,159	1,446	1,720	2,123	2,596	2,610	2,386	2,123
5430	0,604	0,770	1,173	1,453	1,727	2,130	2,603	2,609	2,384	2,116
7260	0,609	0,776	1,181	1,460	1,733	2,137	2,610	2,609	2,382	2,112
14400	0,620	0,795	1,193	1,475	1,751	2,152	2,623	2,607	2,377	2,102
29040	0,644	0,828	1,209	1,493	1,777	2,170	2,637			2,097
57600	0,662	0,880	1,224	1,516	1,818	2,193	2,653			2,090
86640	0,675	0,925	1,236	1,535	1,850	2,212	2,665			2,082

Sperimentatore Dott. L. Stimamiglio

Direttore Laboratorio: Dott. Pietro Daminato

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CERTIFICATO N° 168014	pag. 4/5	emesso il 23/03/26
Verbale di Accettazione n. 08326	data ricevimento campione 06/03/26	data prova 10/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI

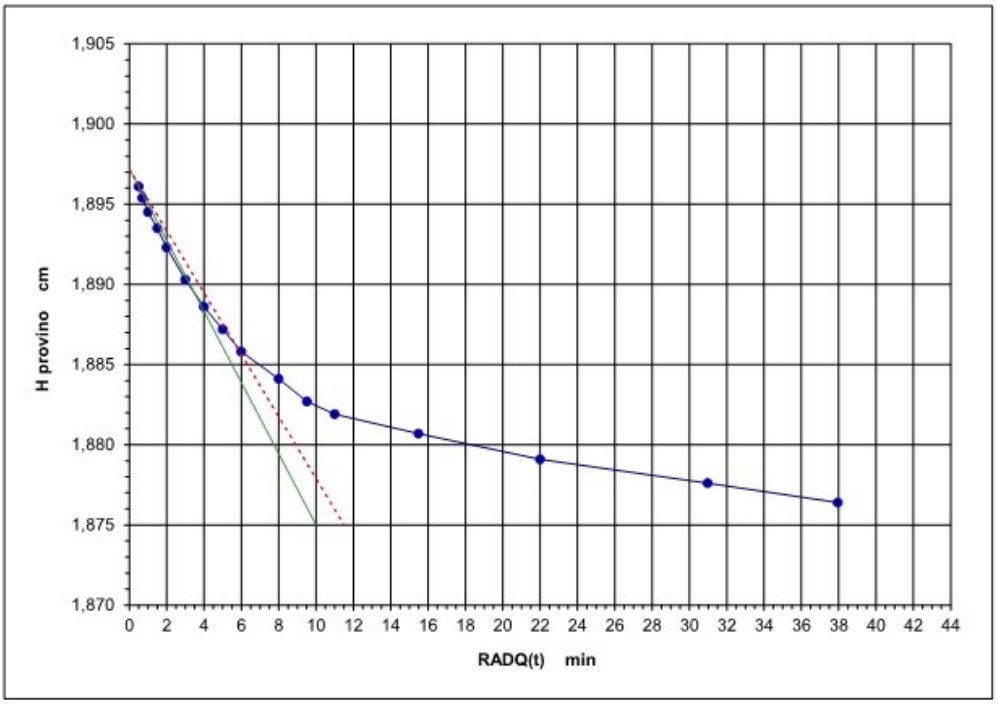
CANTIERE: Area Ex Configliachi - Via Guido Reni - Arcella - Padova

Sond.: **S1** Campione: **CI2** Prof.: **6,00-6,50**

PROVA DI CONSOLIDAZIONE EDOMETRICA

Determinazione del coefficiente di consolidazione Cv con il metodo di Taylor

Pressione verticale	**100**	kPa



cv = 3,93E-08 m^2/s K_{ED} = 1,25E-10 m/s

Sperimentatore
Dott. L. Stimamiglio

Direttore Laboratorio:
Dott. Pietro Daminato

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CERTIFICATO N° 168014	pag. 5/5	emesso il 23/03/26
Verbale di Accettazione n. 08326	data ricevimento campione 06/03/26	data prova 10/03/26

COMMITTENTE: Provincia di Padova - AREA TECNICA - SETTORE EDILIZIA E IMPIANTI

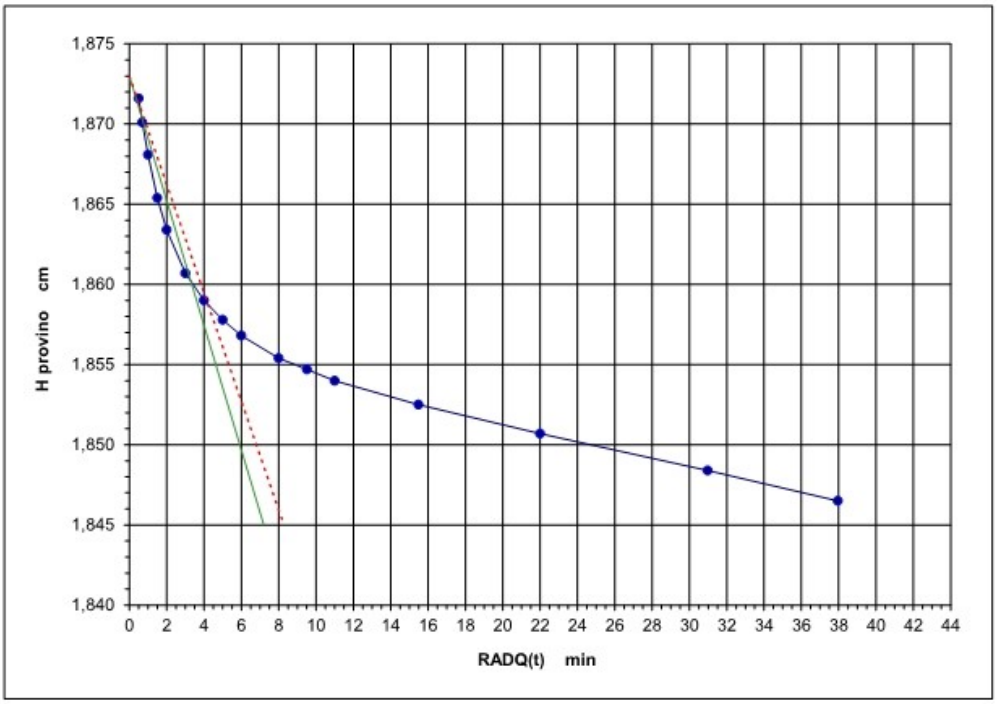
CANTIERE: Area Ex Configliachi - Via Guido Reni - Arcella - Padova

Sond.: **S1** Campione: **CI2** Prof.: **6,00-6,50**

PROVA DI CONSOLIDAZIONE EDOMETRICA

Determinazione del coefficiente di consolidazione Cv con il metodo di Taylor

Pressione verticale	**200**	kPa



cv = 6,86E-08 m^2/s K_{ED} = 1,11E-10 m/s

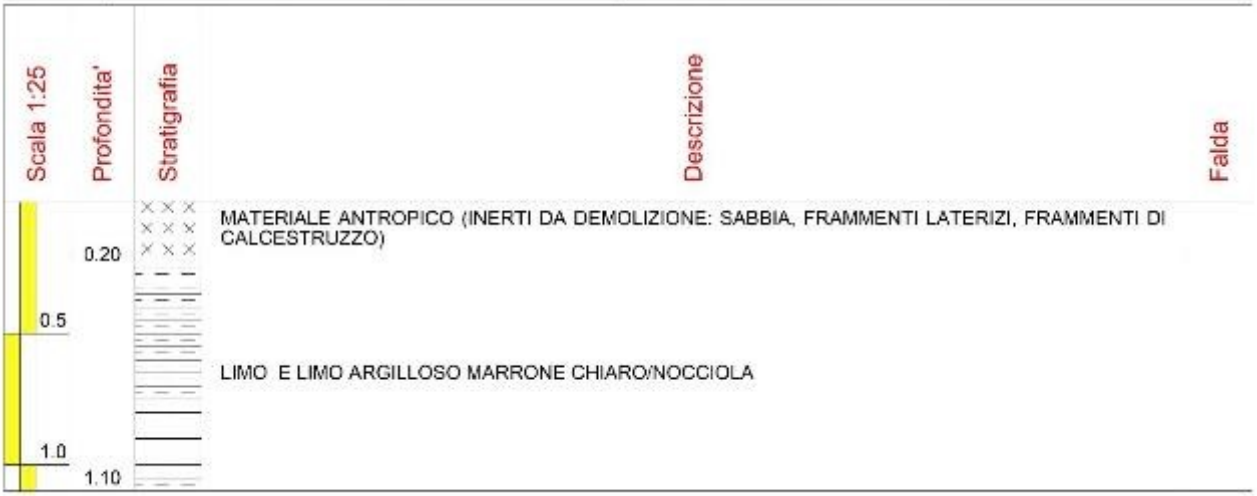
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ALLEGATO 4: TRINCEE ESPLORATIVE

Cantiere EX-CONFIGLIACHI (Via Guido Reni, Padova)	N. sondaggio T1
Committente Provincia di Padova	Scala sondaggio 1:25
Perforatore	Geologo Segato E. - Lovison L.
Coord.	Quota (p.c.)
Metodo perf. Escavatore meccanico	Data ultimazione 11/02/2026



Cantiere EX-CONFIGLIACHI (Via Guido Reni, Padova)	N. sondaggio T2
Committente Provincia di Padova	Scala sondaggio 1:25
Perforatore	Geologo Segato E. - Lovison L.
Coord.	Quota (p.c.)
Metodo perf. Escavatore meccanico	Data ultimazione 11/02/2026



Cantiere EX-CONFIGLIACHI (Via Guido Reni, Padova)	N. sondaggio T3
Committente Provincia di Padova	Scala sondaggio 1:25
Perforatore	Geologo Segato E. - Lovison L.
Coord.	Quota (p.c.)
Metodo perf. Escavatore meccanico	Data ultimazione 11/02/2026



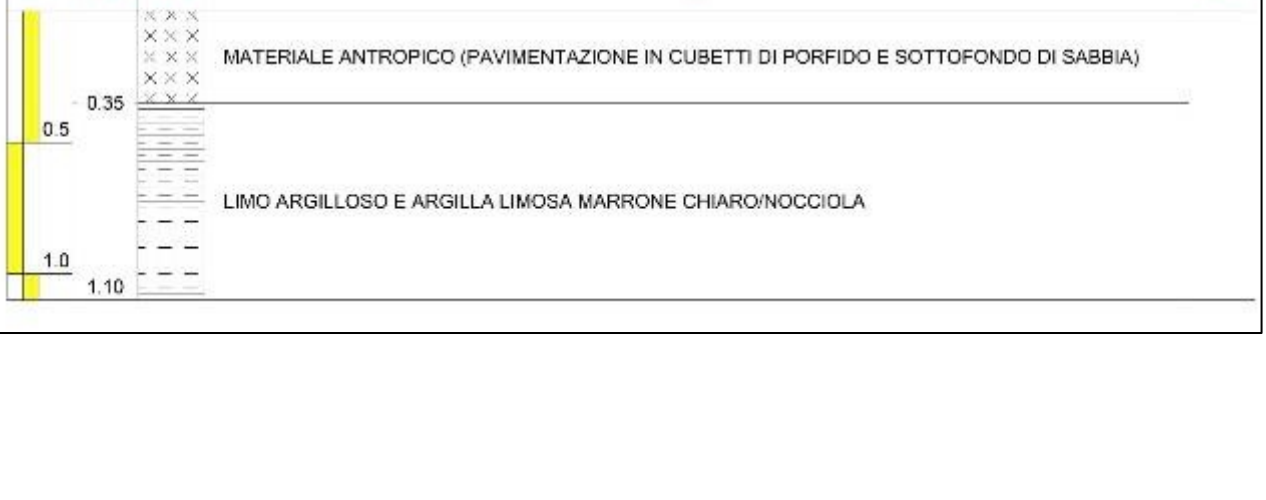
Cantiere EX-CONFIGLIACHI (Via Guido Reni, Padova)	N. sondaggio T4
Committente Provincia di Padova	Scala sondaggio 1:25
Perforatore	Geologo Segato E. - Lovison L.
Coord.	Quota (p.c.)
Metodo perf. Escavatore meccanico	Data ultimazione 11/02/2026



Cantiere EX-CONFIGLIACHI (Via Guido Reni, Padova)	N. sondaggio T5
Committente Provincia di Padova	Scala sondaggio 1:25
Perforatore	Geologo Segato E. - Lovison L.
Coord.	Quota (p.c.)
Metodo perf. Escavatore meccanico	Data ultimazione 11/02/2026



Cantiere EX-CONFIGLIACHI (Via Guido Reni, Padova)	N. sondaggio T6
Committente Provincia di Padova	Scala sondaggio 1:25
Perforatore	Geologo Segato E. - Lovison L.
Coord.	Quota (p.c.)
Metodo perf. Escavatore meccanico	Data ultimazione 11/02/2026



ALLEGATO 5: RISPOSTA SISMICA LOCALE

SOMMARIO

PREMESSA 2
INQUADRAMENTO DELL'AREA ..... **ERRORE. IL SEGNALIBRO NON È DEFINITO.**
INQUADRAMENTO STRUTTURALE E STRATIGRAFICO 3
SISMICITÀ DEL TERRITORIO 5
Sismicità storica *15*
RICOSTRUZIONE STRATIGRAFICA E SISMICA LOCALE 22
Velocità onde Vs *23*
Indagine sismica passiva a stazione singola *23*
Ricostruzione modello stratigrafico profondo *26*
FONDAMENTI DI RISPOSTA SISMICA LOCALE 29
Ricostruzione stratigrafica ai fini della Risposta Sismica Locale *30*
SISMICITÀ DI BASE DEL SITO 32
Pericolosità di base da NTC *33*
DEFINIZIONE DELLE AZIONI DI INPUT 36
ANALISI DI RISPOSTA SISMICA LOCALE 37
Analisi di risposta sismica locale - SLD *39*
Analisi allo stato limite SLV *41*
SINTESI E CONSIDERAZIONI 43

Allegati

Allegato 1: Report analisi RSL_SLD
Allegato 2: Report analisi RSL_SLV

PREMESSA

Per incarico del Committente è stata condotta l'elaborazione della Risposta Sismica Locale, nell'ambito del progetto di nuova costruzione all'interno dell'area Ex Configliachi, in Via Guido Reni, in Comune di Padova commissionata dalla Provincia di Padova (Determina Dirigenziale n.1592 del 22/12/2025).

Questo studio è stato preceduto da una serie di indagini che hanno permesso di caratterizzare il sottosuolo dal punto di vista litologico, geotecnico e sismico; i dati da esse derivati sono elaborati nel presente studio al fine di definire la Risposta Sismica Locale.

Il lavoro è stato svolto secondo quanto previsto dalle vigenti normative in materia:

- D.M. 17.01.18 – Aggiornamento NORME TECNICHE PER LE COSTRUZIONI.
- CIRCOLARE DEL MINISTERO DELLE INFRASTRUTTURE E DEI TRASPORTI DEL 21 GENNAIO 2019 N.7 "ISTRUZIONI PER L'APPLICAZIONE DELL'AGGIORNAMENTO DELLE NORME TECNICHE PER LE COSTRUZIONI DI CUI AL D.M. 17.01.2018" (PUBBLICATA NEL SUPPLEMENTO ORDINARIO N.5 DELLA G.U. N.35 DEL 11.02.2019)
- ORDINANZA n° 3274 del 20.03.03 – PRIMI ELEMENTI IN MATERIA DI CRITERI GENERALI PER LA CLASSIFICAZIONE SISMICA DEL TERRITORIO NAZIONALE E DI NORMATIVE TECNICHE PER LE COSTRUZIONI IN ZONA SISMICA.
- ORDINANZA DEL P.C.M. 28 APRILE 2006 N. 3519 – CRITERI GENERALI PER L'INDIVIDUAZIONE DELLE ZONE SISMICHE E PER LA FORMAZIONE E L'AGGIORNAMENTO DEGLI ELENCHI DELLE MEDESIME ZONE;
- DELIBERAZIONE DELLA GIUNTA REGIONALE N. 244 DEL 09 MARZO 2021 - AGGIORNAMENTO DELL'ELENCO DELLE ZONE SISMICHE DEL VENETO. D.P.R. 6 GIUGNO 2001, N. 380, ARTICOLO 83, COMMA 3; D. LGS 31 MARZO 1998, N. 112, ARTICOLI 93 E 94. D.G.R./CR N. 1 DEL 19/01/2021.

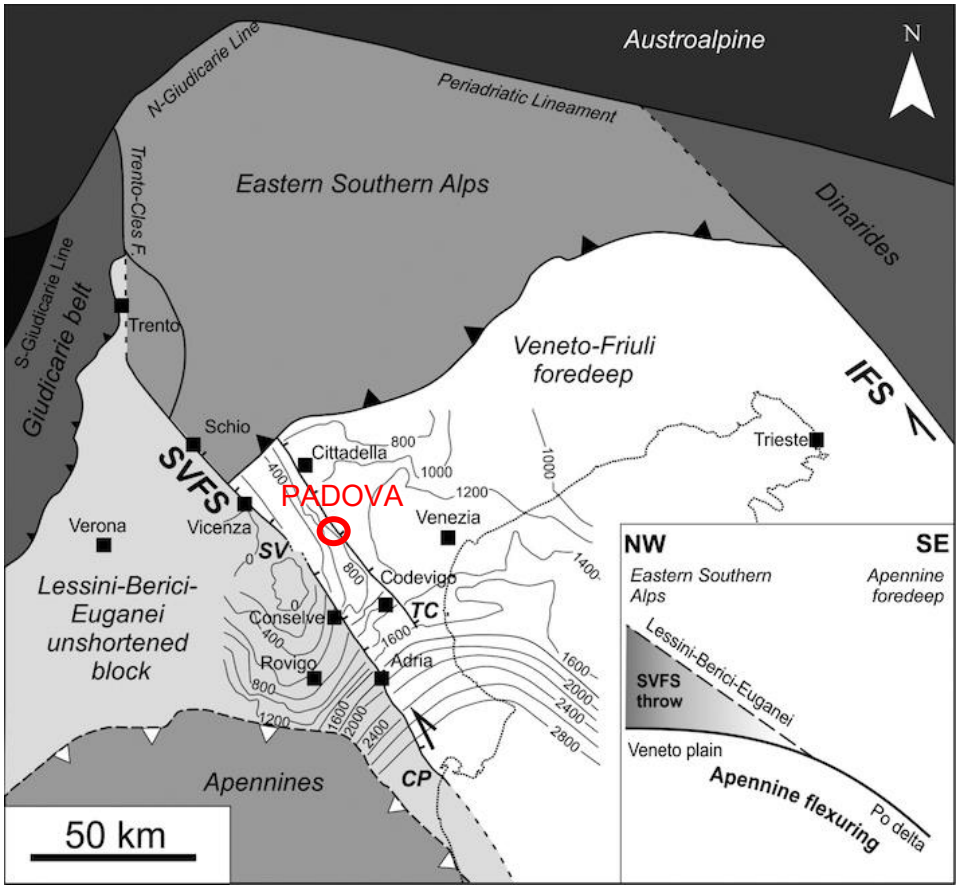
INQUADRAMENTO STRUTTURALE E STRATIGRAFICO

Al fine di inquadrare il modello generale strutturale del territorio della pianura veneta sono state prese in considerazione alcune fonti bibliografiche e immagini estraibili dal database DISS riguardante il catalogo delle sorgenti sismo-genetiche e disponibile online.

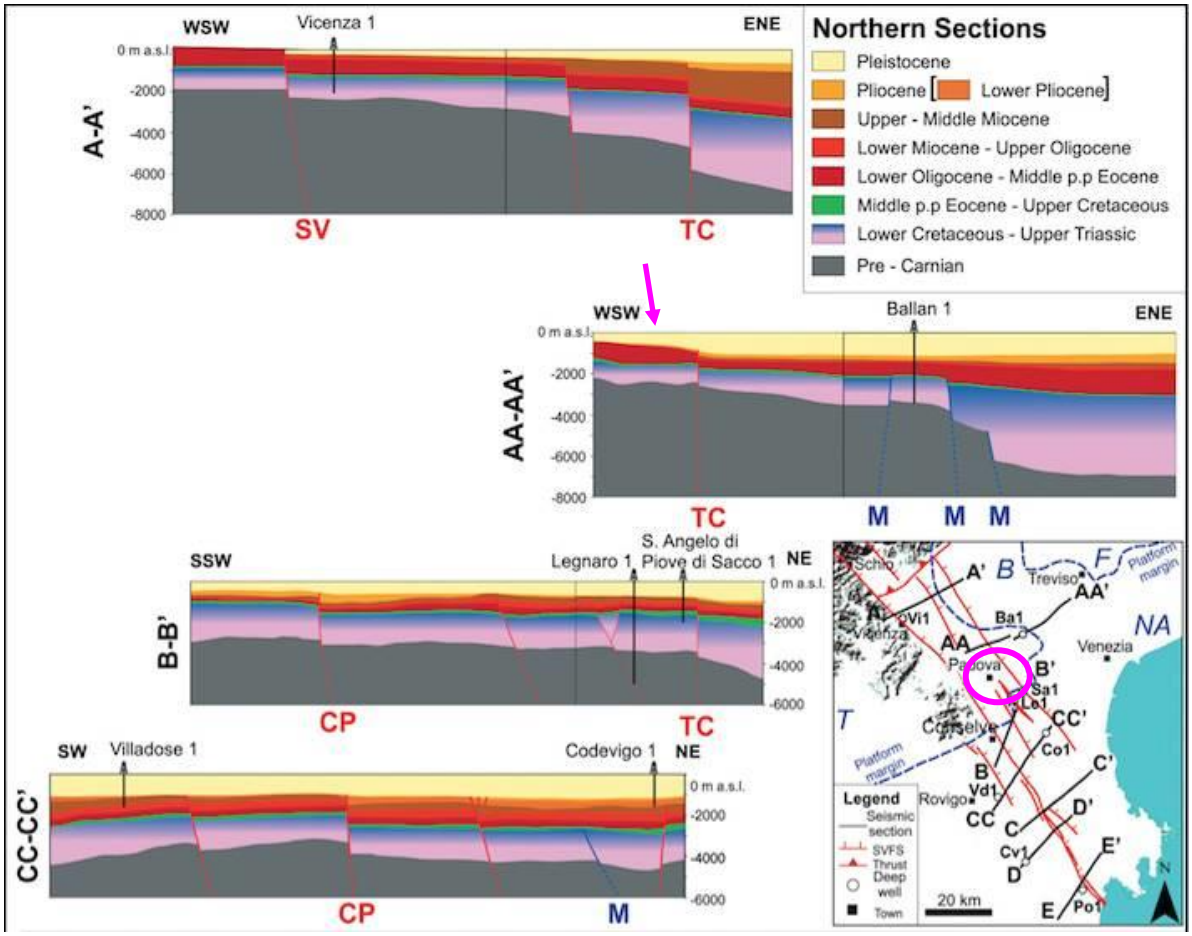
In particolare si riportano alcune immagini che rappresentano rispettivamente l'assetto schematico delle strutture sepolte del Veneto e le profondità della base del Pliocene al di sotto dei depositi alluvionali che caratterizzano la pianura, evidenziando complessivamente le differenze tra Est e Ovest della linea Schio-Vicenza.

Le sezioni che seguono evidenziano l'andamento dei diversi lito-strati: in particolare l'area in esame si colloca tra le sezioni AA-AA' e la B-B'; le sezioni mettono in risalto la variazione degli spessori delle diverse formazioni con aumento complessivamente dello spessore del Pleistocene da ovest verso est.

Map of the depth of the Pliocene base along the Schio-Vicenza Fault System (SVFS), Travettore-Codevigo fault (TC) and Conselve-Pomposa fault (CP). Notice the deepening toward southeast due to the Apennine Pliocene-Quaternary flexuring. IFS: Idrija Fault System (from Pola et al. [2014]).



Cross-sections sub-orthogonal to the Schio-Vicenza Line obtained through the interpretation of the seismic sections. Fault traces associated with the Schio-Vicenza Fault System are recognized. SV: Schio-Vicenza fault; CP: Conselve-Pomposa fault; TC: Travettore-Codevigo fault; M: Mesozoic extensional fault; A: Apennine reverse fault (from Pola et al. [2014]).

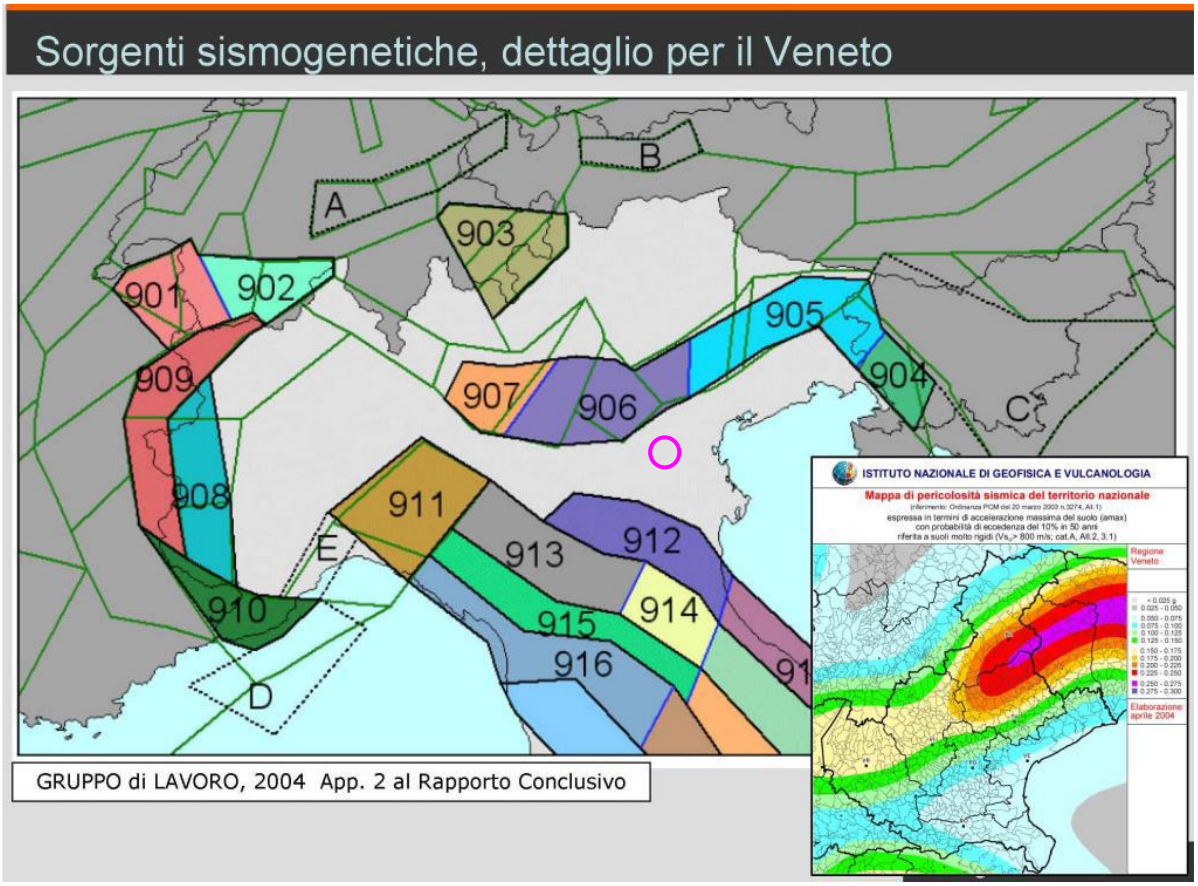


SISMICITÀ DEL TERRITORIO

La sismicità generale del territorio è strettamente connessa al suo contesto tettonico-strutturale e quindi alla presenza di strutture geologicamente "attive". Alla base di ogni stima della pericolosità sismica di un territorio vi è dunque l'indispensabile conoscenza della sua storia sismica, cioè di tutte le informazioni sui sismi avvenuti nel passato, e della geologia strutturale locale, entrambe strettamente connesse tra loro.

La "*Carta delle zone sismogenetiche ZS9"* suddivide il territorio italiano in 36 zone, in base a un modello cinematico che sfrutta una serie di relazioni di attenuazione stimate sulla base di simulazioni. Le zone sismogenetiche sono state definite in base a uniformità dello stile deformativo e della congruenza cinematica con il modello deformativo.
La zona in esame può essere associata alle zone sismogenetiche 905 e 906 le quali si sviluppano a nord, lungo l'arco di passaggio dalle Prealpi Venete alla pianura, e caratterizzate da strutture a pieghe sud-vergenti del Sudalpino orientale e faglie inverse associate.
La zona 905 include sorgenti sismogenetiche potenzialmente responsabili di terremoti con magnitudo M>6, e racchiude un'area in cui la frequenza di eventi sismici (anche di magnitudo medio-alte) è nettamente superiore a quella delle zone adiacenti.
La zona 905 comprende anche la sorgente del Montello (potenzialmente responsabile di terremoti con M>6), che, in base ai dati attualmente disponibili, è definita come "silente" (cioè mancano, nei cataloghi disponibili, terremoti storici con magnitudo prossima a quella massima attesa).
La zona 906 interessa l'area che va da Bassano del Grappa fino a Verona.
Per le aree 905 e 906 la magnitudo massima attesa è M_{wmax}= 6.60.

Tutte le zone sismogenetiche vengono considerate omogenee ai fini della probabilità di accadimento degli eventi sismici e in rapporto agli epicentri noti, ne consegue che non esiste l'effetto distanza. L'ICMS 2008 al paragrafo 2.8.2 stabilisce che può essere utilizzato, a favore della sicurezza, per alcune tipologie di verifiche (es. liquefazione), la magnitudo attesa massima della zona sismogenetica di appartenenza.



Faglie attive e capaci, e sorgenti sismogenetiche responsabili di terremoti

Verso la fine degli anni ’90 sono iniziate delle ricerche geologico-strutturali, sul fronte pliocenico (7-1.5 milioni di anni fa) - quaternario (1.5 milioni all’attuale) nell’Italia Nord Orientale e sul suo potenziale sismogenetico; con tale studio sono stati ridefiniti l’architettura del fronte sepolto della pianura friulano-veneta, lo schema dei rapporti fra i sovrascorrimenti paleocenici dinarici WSW-vergenti e quelli neoalpini SSE-vergenti e il quadro dell’evoluzione miocenica superiore-quaternaria dell’area.

Lo schema strutturale aggiornato del fronte pliocenico-quaternario evidenzia la segmentazione del fronte stesso in un sistema di “thrust” arcuati, in massima parte ciechi e spesso caratterizzati da rampe oblique, mediante le quali un “thrust” si accavalla lateralmente su un altro. Analisi morfotettoniche e neotettoniche applicate a tali strutture hanno permesso in vari casi di datarne l’attività e di definirne la cinematica quaternaria.

Nonostante le faglie capaci possono rappresentare l'emersione in superficie di strutture sismogeniche, il Catalogo ITHACA non va utilizzato per valutazioni di hazard sismico in termini di scuotimento.

Per tali scopi si rimanda alla banca dati DISS – Database of Individual Seismogenic Sources http://diss.rm.ingv.it/diss/: alla pagina seguente la mappa riportata risulta la sovrapposizione tra le informazioni del catalogo Ithaca e del Database DISS.

Di seguito si riportano i "credits" del nuovo DISS 3.3.0 (dicembre 2021):

Permission to use the Database is granted subject to full acknowledgement of the source in the following form.

When referring to concept & design of the database as a whole:

Basili R., G. Valensise, P. Vannoli, P. Burrato, U. Fracassi, S. Mariano, M.M. Tiberti, E. Boschi (2008). The Database of Individual Seismogenic Sources (DISS), version 3: summarizing 20 years of research on Italy's earthquake geology, Tectonophysics; https://doi.org/10.1016/j.tecto.2007.04.014

When referring to a specific dataset or subset of the current version:

DISS Working Group (2021). Database of Individual Seismogenic Sources (DISS), Version 3.3.0: A compilation of potential sources for earthquakes larger than M 5.5 in Italy and surrounding areas. Istituto Nazionale di Geofisica e Vulcanologia (INGV). https://doi.org/10.13127/diss3.3.0

When using additional datasets from external sources:

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License



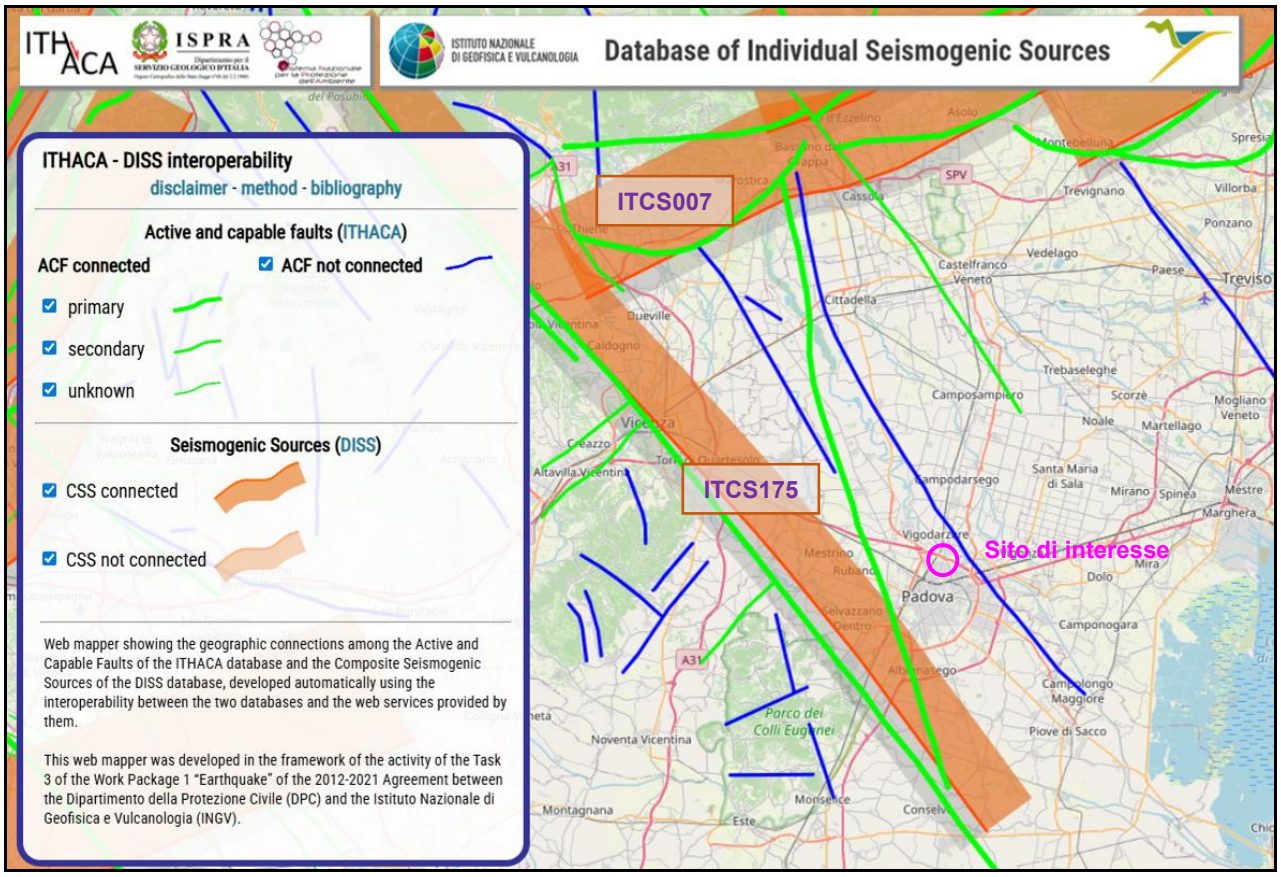
Except where otherwise noted, content on this site is licensed under a Creative Commons Attribution 4.0 International (CC BY 4.0) licence.

Il DISS 3.3.0 (Database of Individual Seismogenic Sources versione di dicembre 2021) dell'INGV (Istituto Nazionale di Geofisica e Vulcanologia) individua:

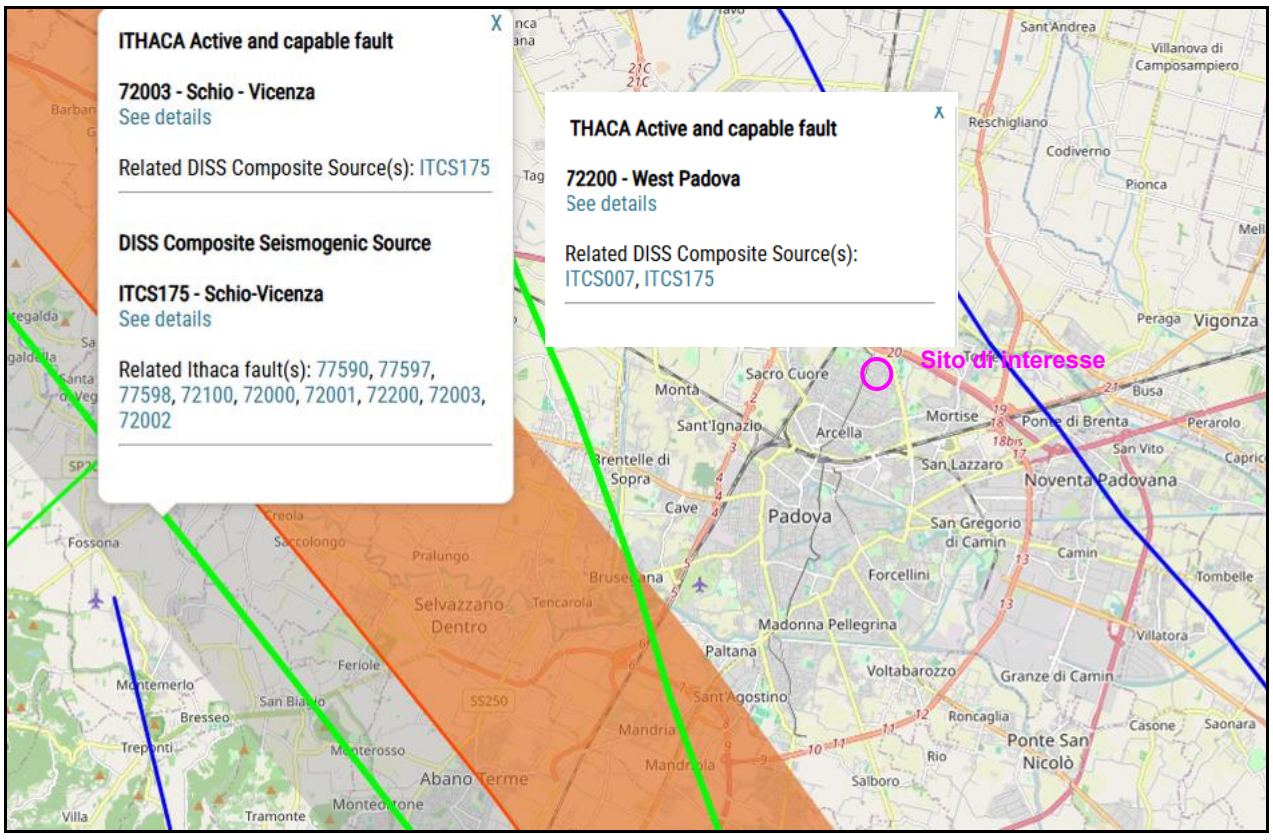
- Sorgenti sismogenetiche composite: sono zone molto estese, all'interno delle quali vi sono sorgenti sismogenetiche minori ancora non sufficientemente studiate. Queste aree non sono associate a specifici terremoti storici (individuate con un retino arancione o con una scala di profondità nell'immagine di seguito riportata della nuova versione).
- Sorgenti sismogenetiche individuali: aree a cui sono associati specifici terremoti storici.

ITHACA individua invece le faglie attive e capaci.

Faglie Attive e Capaci (ITHACA) e Sorgenti Sismogenetiche (DISS) nell'area di interesse



Faglie Attive e Capaci nell'area di interesse - DETTAGLIO



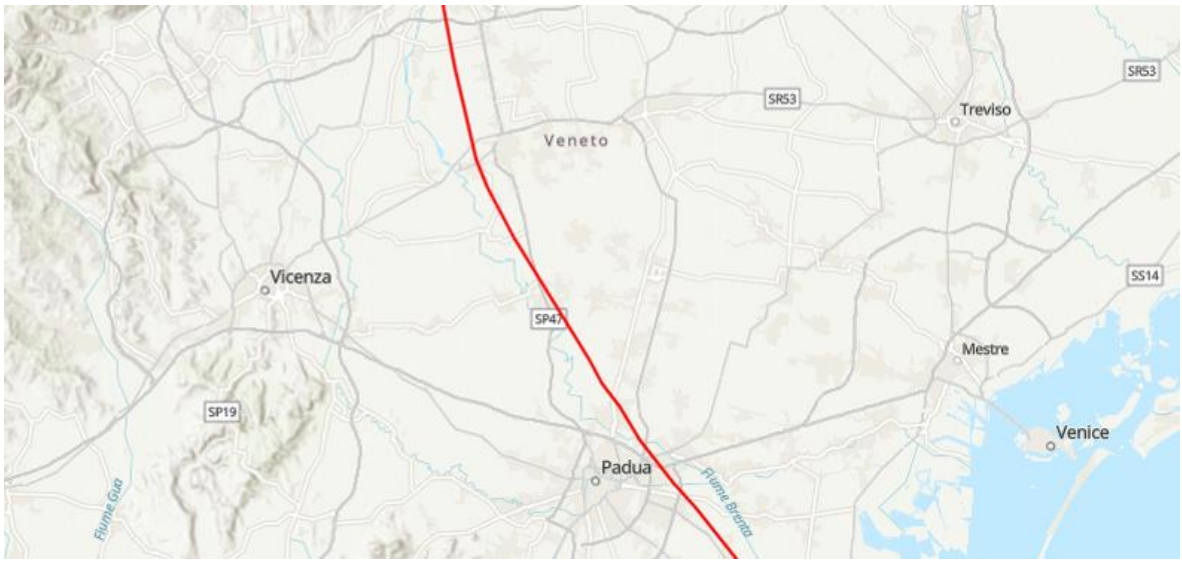
Le faglie attive e capaci individuate nel territorio in esame sono identificate come:

- 72300 : Est Padova – ACF Not Connected
- 72200 : West Padova – Related DISS Composite Source ITCS007
- 72003 : Schio – Vicenza – Related DISS Composite Source ITCS175

Di seguito viene riportata la traccia e la scheda tecnica di ciascuna faglia evidenziata per l'area in esame:

ITHACA - Catalogo delle faglie capaci
AREA GEODINAMICA, GEORISORSE, PERICOLOSITA' E IMPATTI EVENTI NATURALI E INDOTTI

72300



Fault description	
GENERAL IDENTIFICATION	
Fault Code	72300
Fault Name	East Padova
Region Name	Veneto
Tectonic Environment	ND
System Name	East Padova
Synopsis	
Rank	Primary
GEOMETRY AND KINEMATICS	
Segmentation	Single Segment
Average Strike (°)	140
Dip (°)	Undefined
Dip Direction	E
Fault Length (km)	54.9
Mapping Scale	1:
Fault Depth (m)	
Kinematics	Normal

ACTIVITY	
Surface Evidence	ND
Last Activity	Early Pleistocene
Evidence for Capability	Displacement of Quaternary deposits and/or land forms

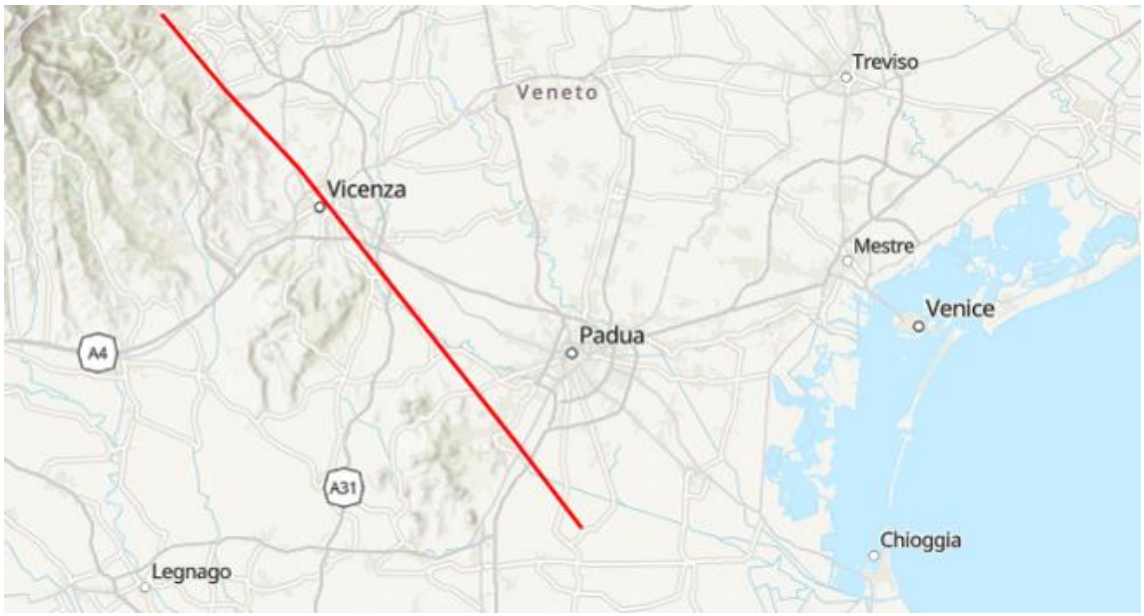
SLIP PARAMETERS	
Recurrence Interval (yr)	
Slip Rate (mm/yr)	
Max Credible Rupture Length (km)	
Max Credible Slip (m)	
Time Since Last Event (yr)	
Max Known Magnitude (Mw)	
Max Known Intensity (MCS)	
Known Seismic Events	

72200



Fault description	
GENERAL IDENTIFICATION	
Fault Code	72200
Fault Name	West Padova
Region Name	Veneto
Tectonic Environment	ND
System Name	West Padova
Synopsis	
Rank	Primary
GEOMETRY AND KINEMATICS	
Segmentation	Single Segment
Average Strike (°)	150
Dip (°)	Undefined
Dip Direction	E
Fault Length (km)	57.2
Mapping Scale	1:
Fault Depth (m)	
Kinematics	Normal
ACTIVITY	
Surface Evidence	ND
Last Activity	Early Pleistocene

72003



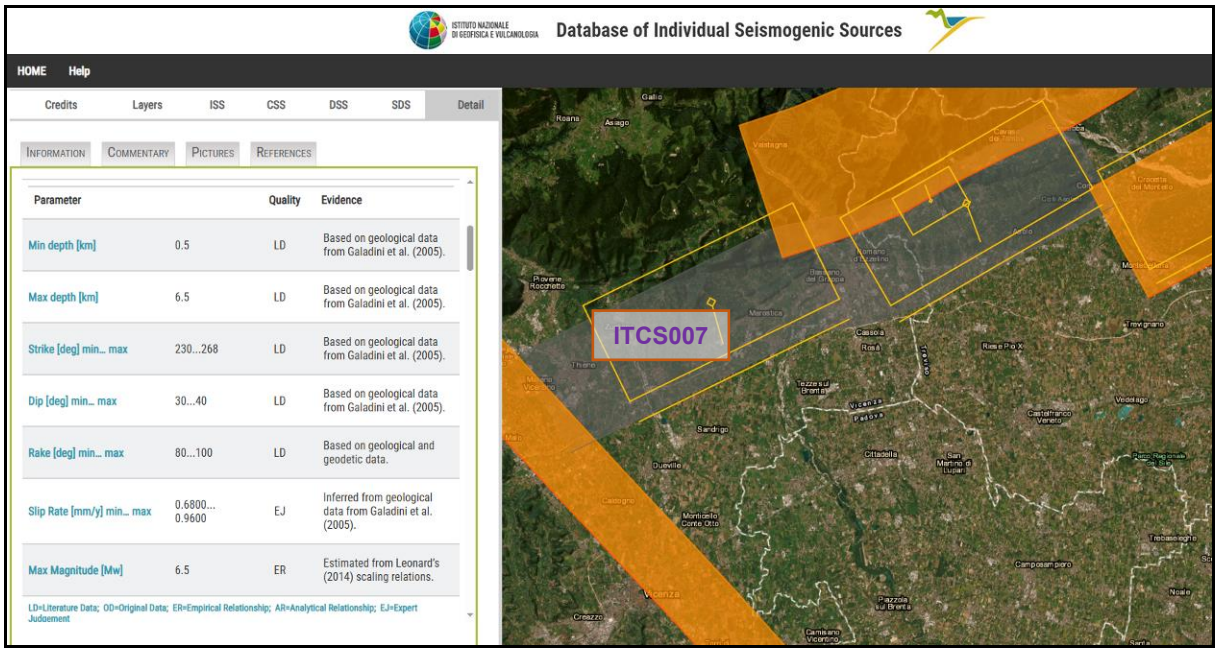
Fault description	
GENERAL IDENTIFICATION	
Fault Code	72003
Fault Name	Schio - Vicenza
Region Name	Veneto
Tectonic Environment	PLATE BOUNDARY
System Name	Schio - Vicenza
Synopsis	
Rank	Primary
GEOMETRY AND KINEMATICS	
Segmentation	Single Segment
Average Strike (°)	320
Dip (°)	Undefined
Dip Direction	NE
Fault Length (km)	69.2
Mapping Scale	1:500000
Fault Depth (m)	
Kinematics	Normal
ACTIVITY	
Surface Evidence	hidden (buried, blind fault)
Last Activity	Early Pleistocene

Le faglie attive individuate sono messe in relazione alle rispettive sorgenti sismogenetiche di seguito descritte:

- ITCS007 Thiene-Cornuda, sorgente sismogenetica composita; ad essa vengono associati il terremoto Asolano del 25 febbraio 1695 con M = 6.7 e quello di Bassano del 12 giugno 1836 con M = 5.5.
- ITCS175 Schio – Vicenza, sorgente sismogenetica composita che non sembra possa generare terremoti con M > 5 tuttavia il DISS riporta una M massima di 7.3; si attribuiscono a tale struttura i terremoti del 13 settembre 1989 a Nord si Schio e con M=4.7 e quello del 16 giugno 2000 che ha interessato Rovereto con M = 3.7.

A seguire si riportano le relative schede estratte dal database DISS.

ITCS007 THIENE-CORNUDA

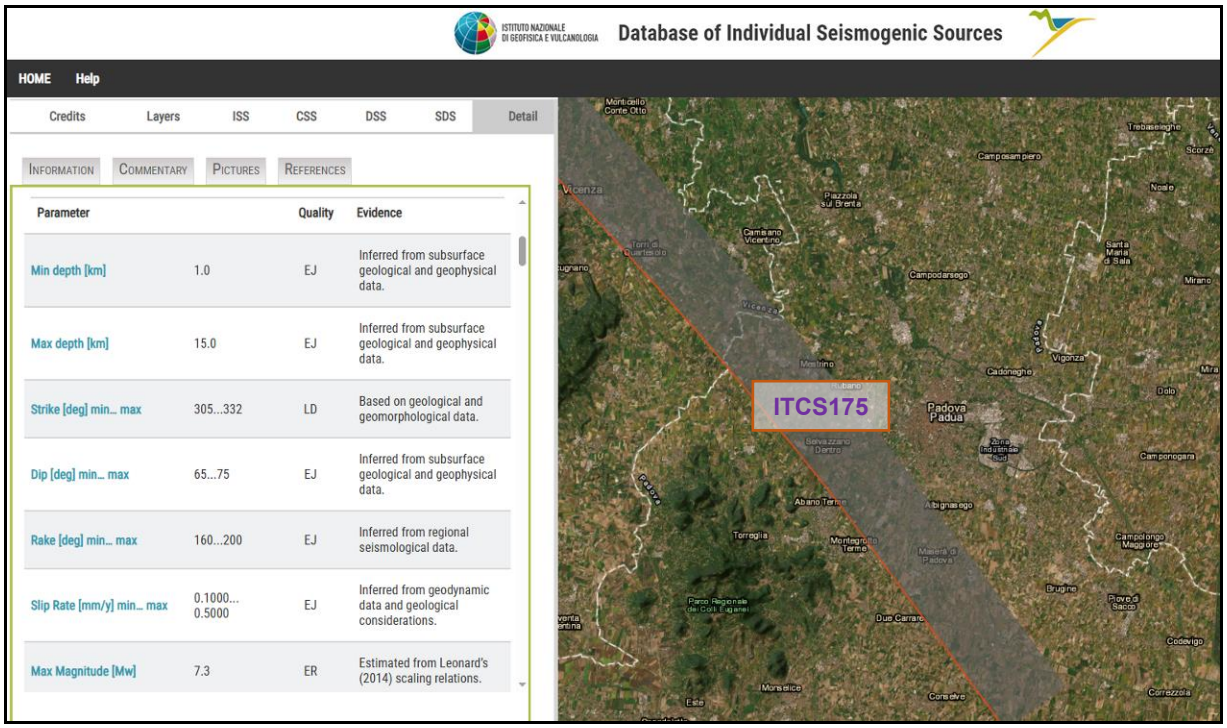


This Composite Source straddles the region across the Veneto southwestern foothills and belongs to the overall thrust system that borders the Veneto-Friuli plain in north-eastern Italy. This front is a S-to SE-verging fault system of the eastern Southalpine Chain and is thought to accommodate the ca. N-S convergence between Africa (the Adriatic microplate here) and Europe.

Historical and instrumental catalogues (Boschi et al., 2000; Gruppo di Lavoro CPTI, 2004; Pondrelli et al., 2006; Guidoboni et al., 2007) show scattered, intermediate seismicity (ca. Mw 4) just north of this region. A key, destructive earthquake has occurred in the eastern sector on 25 February 1695 (Mw 6.7) in the Asolano area, while another damaging event hit just west, on 12 June 1836 (Mw 5.5) in Bassano.

We believe that this sector of the north-eastern South Alpine chain is characterised by large magnitude earthquakes (Mw 6+, such as the 1695 event) that are generated by segments of the frontal, S-to SE-verging thrust, while smaller (Mw 5+), yet potentially destructive events, can be generated by secondary structures, such as the Monte Grappa back-thrust.

ITCS175 SCHIO-VICENZA



This Composite Source belongs to the Schio-Vicenza fault system, a NW-SE trending, NE-dipping, set of high angle faults that lower the sedimentary succession of the Veneto plain to the east (e.g. Pola et al., 2014), being a transverse structure with respect to the general trend of the Eastern Southern Alps thrust front. The main structure of this fault system is the Schio-Vicenza Line, a NW-SE, 120 km long, steep strike-slip fault (e.g. Pellegrini, 1988; Castaldini and Panizza, 1991; Zampieri et al., 2003, 2021). The Schio-Vicenza Line is a prominent geomorphological lineament across the Southern Alps and the Venetian Po Plain, bordering to the east the Lessini, Berici and Euganei Mts., fragments of the Alpine retro-foreland (Bigi et al., 1992). To the south-east, this prominent lineament continues in the subsurface of the Veneto plain, where it is known as the Conselve-Pomposa fault (Pola et al., 2014).

Historical and instrumental catalogues (e.g. Rovida et al., 2021) show only a scattered distribution of moderate seismicity along this structure. Moreover, the source of the 13 September 1989, Mw 4.9 earthquake, having a depth of 40 km and a dextral strike-slip kinematics (Pondrelli et al., 2006), is located north of Schio and falls within the Schio-Vicenza fault system, and is thus deemed responsible for the 1989 event (Vannoli et al., 2015). Other instrumental earthquakes occurred near the northern part of the structure and showed dextral strike-slip focal mechanisms (Viganò et al., 2008; Viganò et al., 2015). Among these, the 16 June 2000, Mw 3.7 earthquake occurred near Rovereto along the northernmost sector of this fault system (Braunmiller et al., 2002).

Sismicità storica

Si è consultato il Catalogo Parametrico dei Terremoti Italiani, CPTI15 nella versione più aggiornata v 4.0 di gennaio 2022.

I dati macrosismici a supporto di CPTI15 costituiscono il Database Macrosismico Italiano; si è consultato infatti in parallelo anche il Database Macrosismico Italiano DBMI15 v4.0 di gennaio 2022, che permette di osservare i parametri dei terremoti che hanno interessato una determinata area nell'intorno del sito in esame.

CPTI15 v4.0
Catalogo Parametrico dei Terremoti Italiani
DBMI15 v4.0
Database Macrosismico Italiano

Termini di utilizzo dei dati

CPTI15 è consultabile liberamente all'indirizzo http://emidius.mi.ingv.it/CPTI15-DBMI15 e attraverso il "web service" dell'Archivio Storico Macrosismico Italiano (ASMI) all'indirizzo https://emidius.mi.ingv.it/ASMI/services/.

CPTI15 è un prodotto scientifico dell'Istituto Nazionale di Geofisica e Vulcanologia (INGV) la cui realizzazione ha richiesto anni di lavoro e raccoglie il frutto della ricerca di diversi autori di diversi enti.

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Citazione

L'utilizzo, anche parziale, del catalogo è consentito a condizione che la fonte sia sempre citata come segue:

Rovida A., Locati M., Camassi R., Lolli B., Gasperini P., Antonucci A. (2022). Catalogo Parametrico dei Terremoti Italiani (CPTI15), versione 4.0 [Data set]. Istituto Nazionale di Geofisica e Vulcanologia (INGV). https://doi.org/10.13127/cpti/cpti15.4

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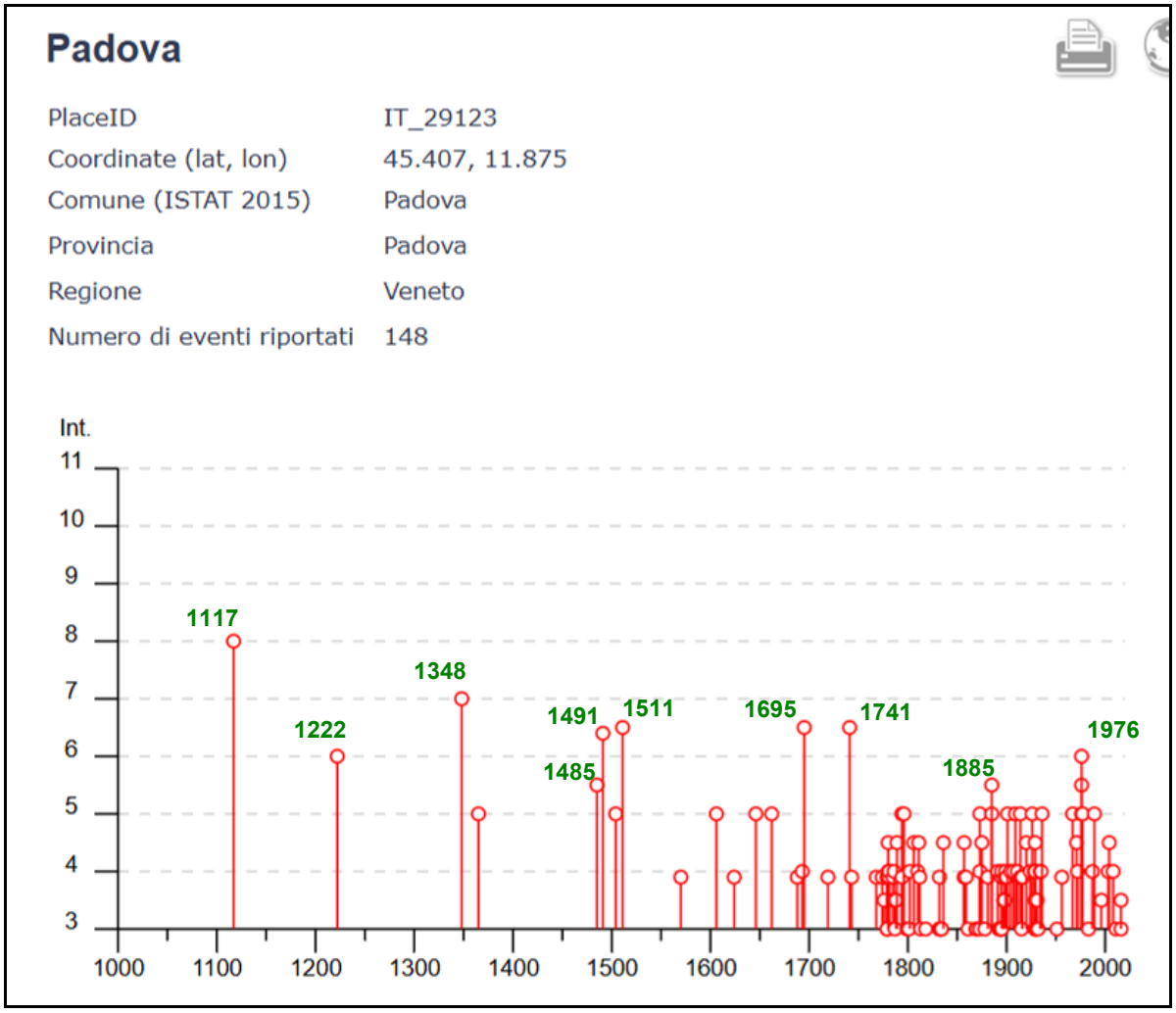
Limitazioni di responsabilità

CPTI15 fornisce dati sulla sismicità italiana utilizzando le migliori conoscenze scientifiche disponibili; tuttavia, in conseguenza della complessità dei fenomeni naturali in oggetto, nulla può essere imputato all'all'Istituto Nazionale di Geofisica e Vulcanologia circa l'eventuale incompletezza ed incertezza dei

dati riportati nel catalogo e circa accadimenti futuri che possano essere dedotti dagli utenti sulla base di tali dati.
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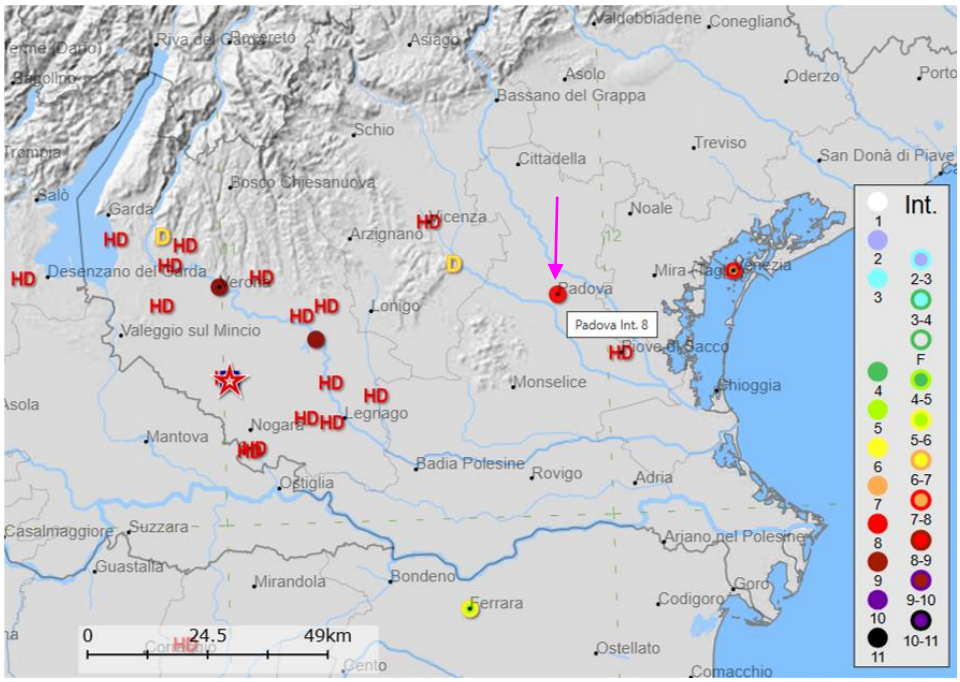
CPTI15 v4.0 è stato realizzato nell'ambito delle attività dell'Allegato A dell'Accordo quadro tra il Dipartimento di Protezione Civile e l'Istituto Nazionale di Geofisica e Vulcanologia 2012-2021.
Fornisce dati parametrici omogenei, sia macrosismici, sia strumentali, relativi ai terremoti con intensità massima ≥ 5 o magnitudo ≥ 4.0 d'interesse per l'Italia nella finestra temporale 1000-2020.

Si rilevano terremoti storici anche molto forti, che hanno determinato particolari intensità registrate a Padova e nell'immediato intorno.

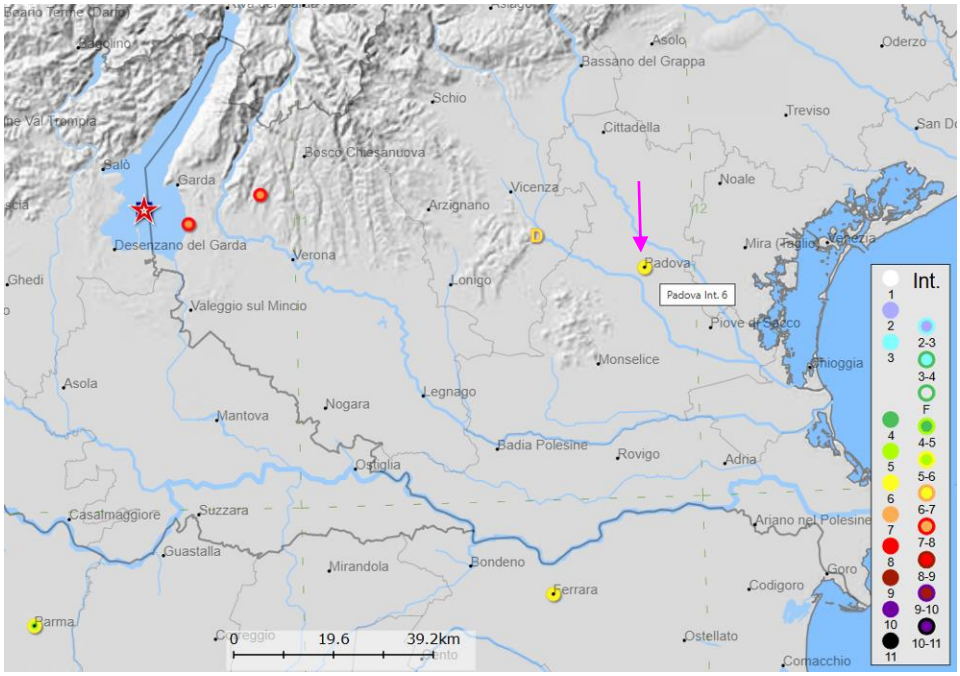


Di seguito si prendono in considerazione con maggiore dettaglio gli eventi sismici per i quali sono state registrate mediamente le Intensità maggiori presso Padova, come evidenziato dal grafico sopra riportato.

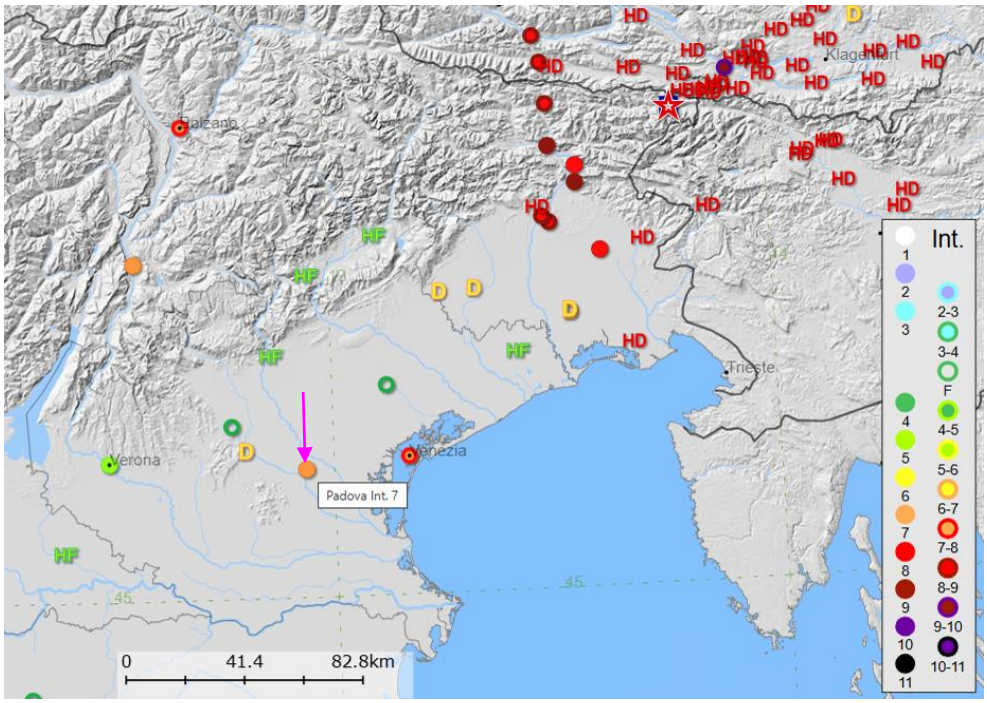
3 gennaio 1118 Veronese Mw = 6.52



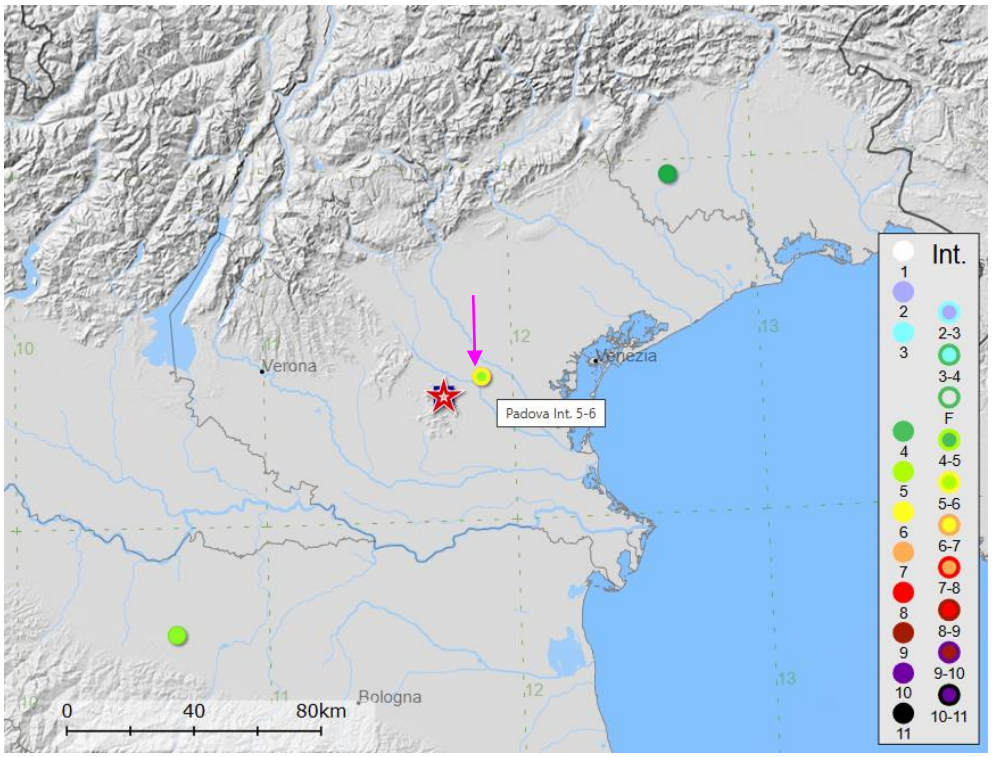
25 dicembre 1222 Bresciano-Veronese Mw = 5.68



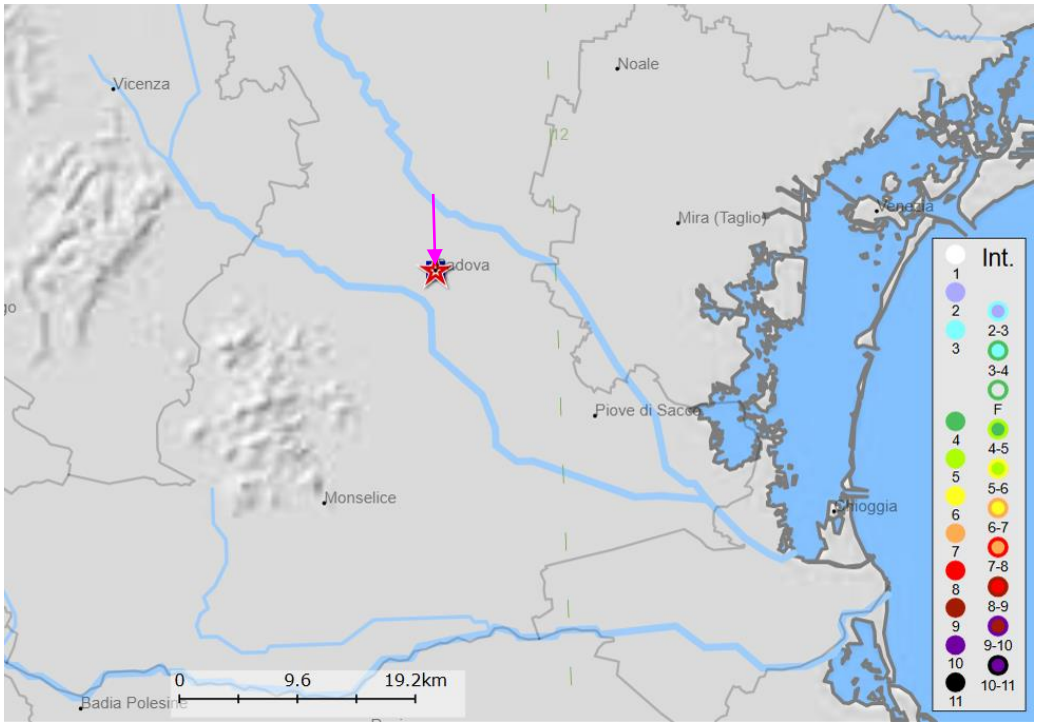
25 gennaio 1348 Alpi Giulie Mw = 6.63



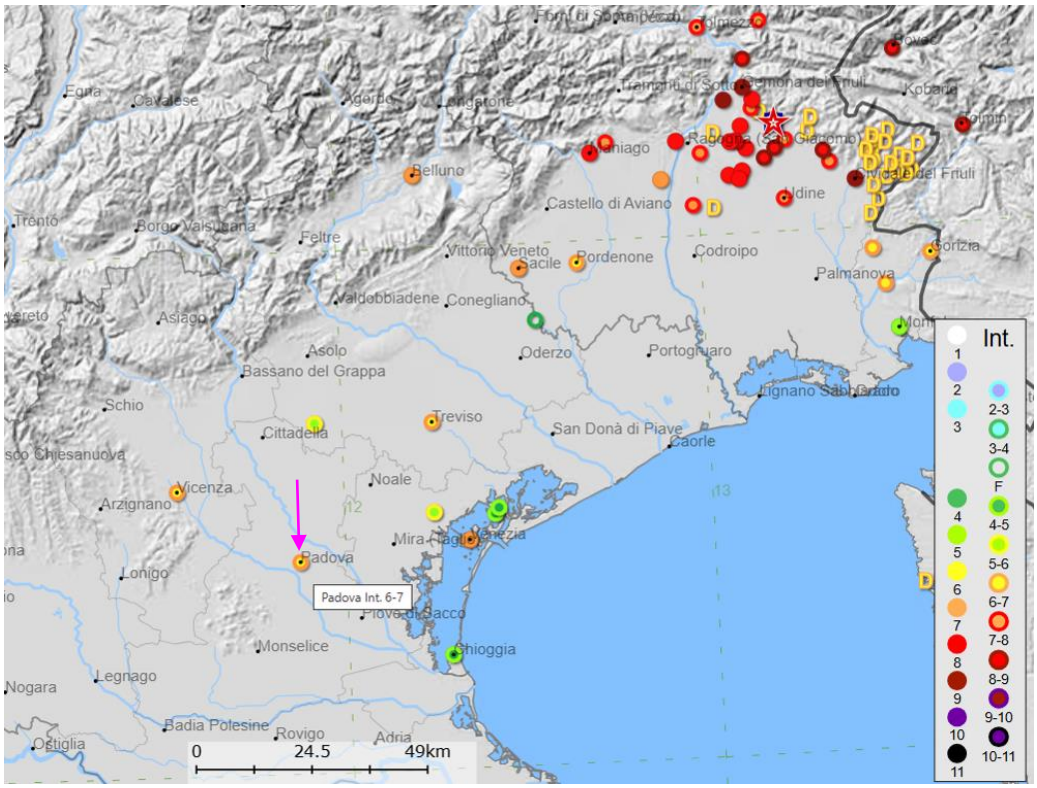
01 settembre 1485 Pianura padano-veneta Mw = 4.16



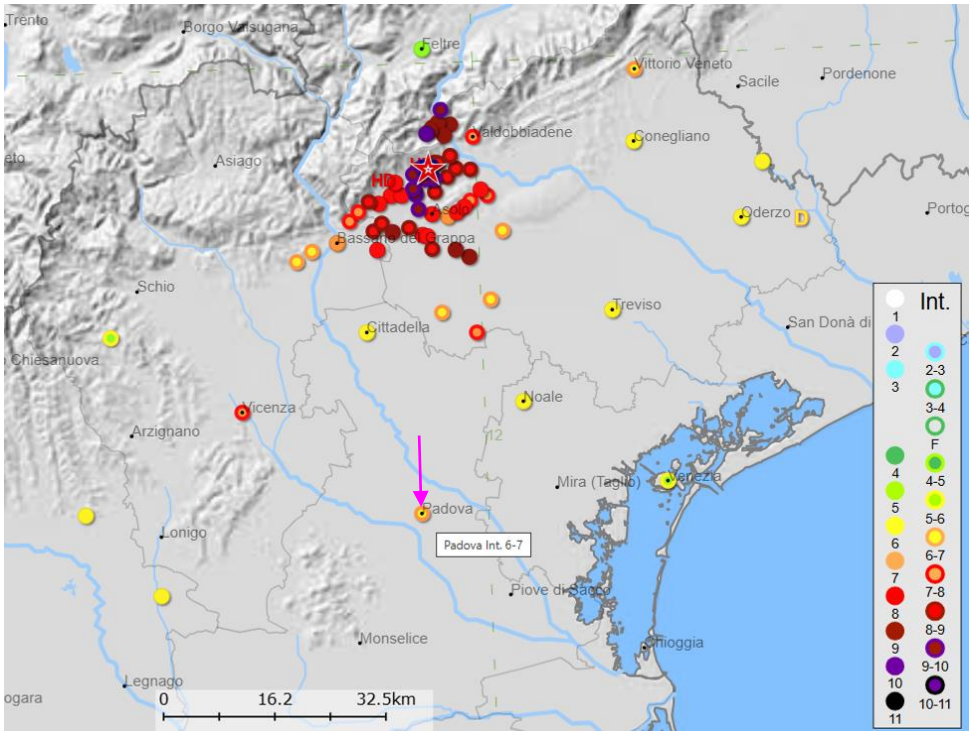
24 gennaio 1491 Padova Mw = 4.86



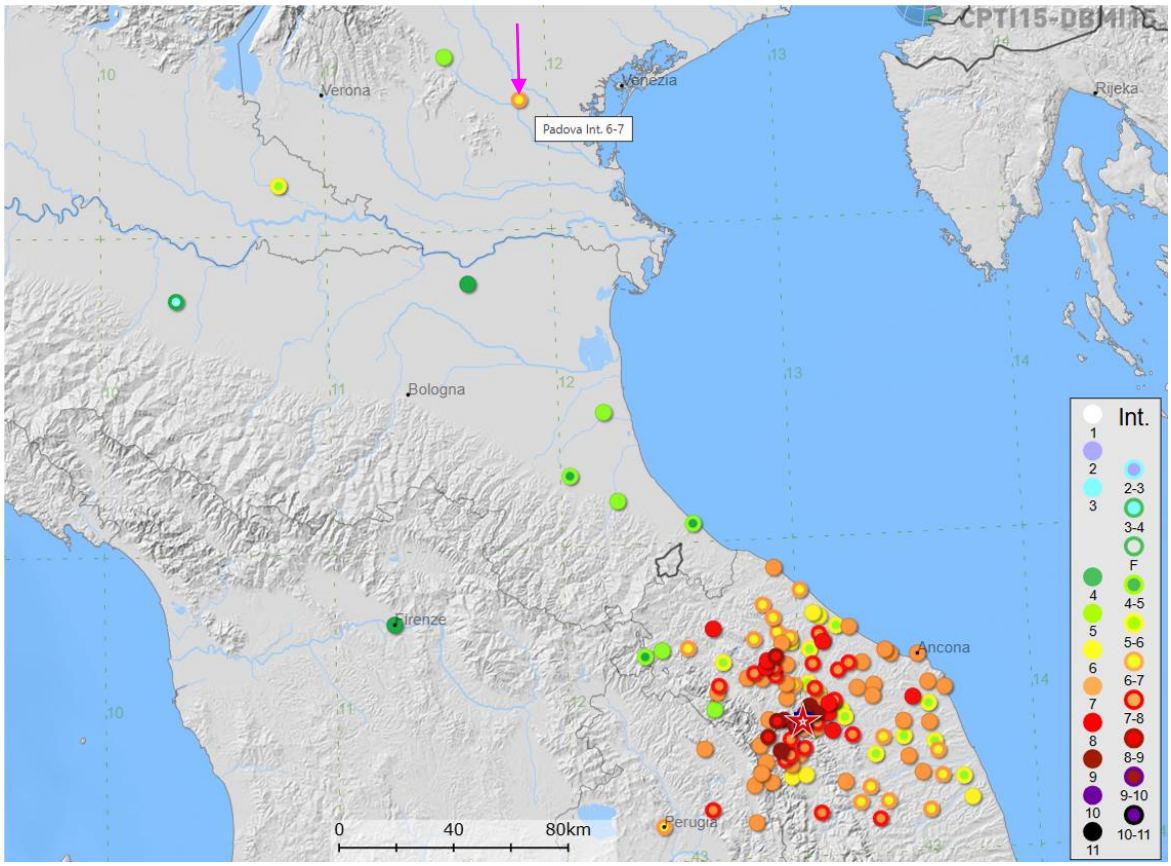
26 marzo 1511 Friuli-Slovenia Mw = 6.32



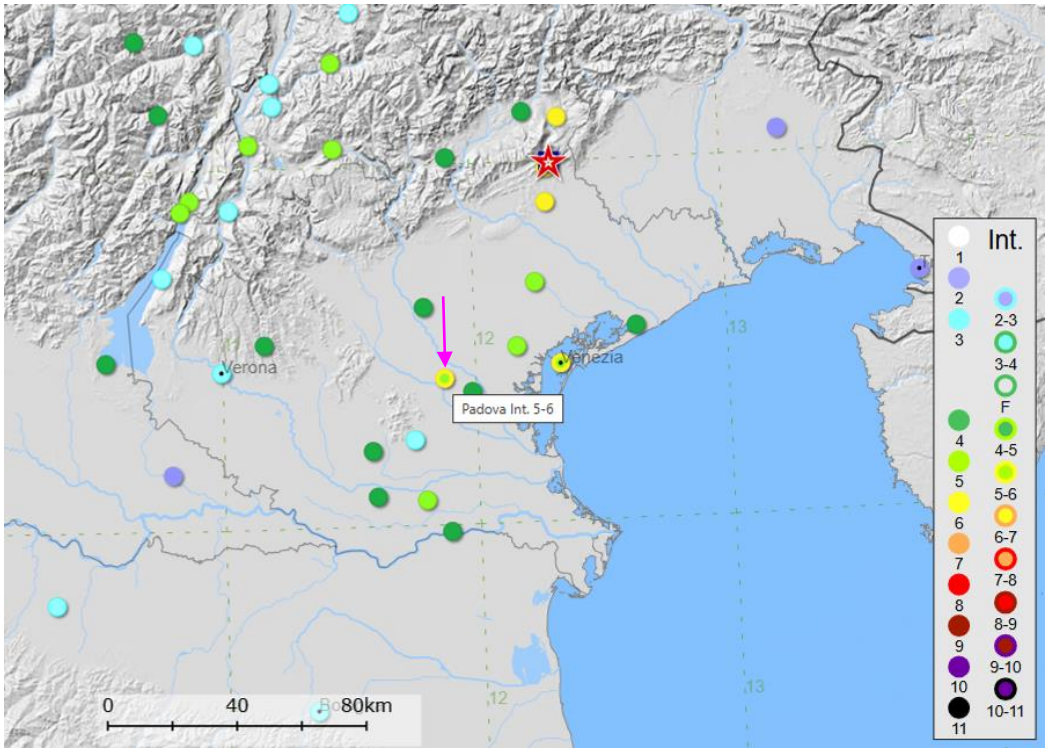
25 febbraio 1695 Asolano Mw = 6.40



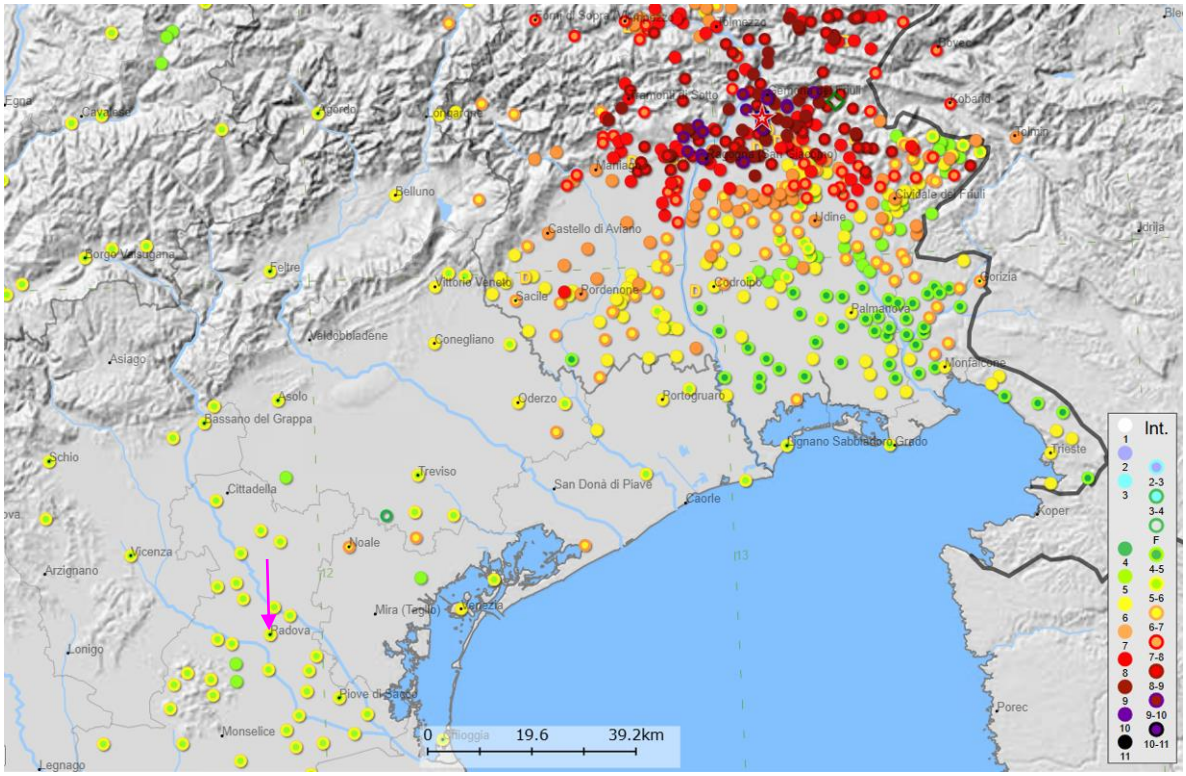
24 aprile 1741 Fabrianese Mw = 6.17



29 dicembre 1885 Alpago-Cansiglio Mw = 4.96



6 maggio 1976 Friuli Mw = 6.45



Osservando le mappe riportate si riscontra che complessivamente nel territorio di Padova sono state registrate negli anni intensità comprese prevalentemente tra 6 e 7.

RICOSTRUZIONE STRATIGRAFICA E SISMICA LOCALE

Al fine di ricostruire con maggior dettaglio le litologie che interessano il sottosuolo più superficiale si fa riferimento in primo luogo qui di seguito alle indagini geognostiche e sismiche condotte in sito nell'ambito del progetto in esame.



Ubicazione delle indagini

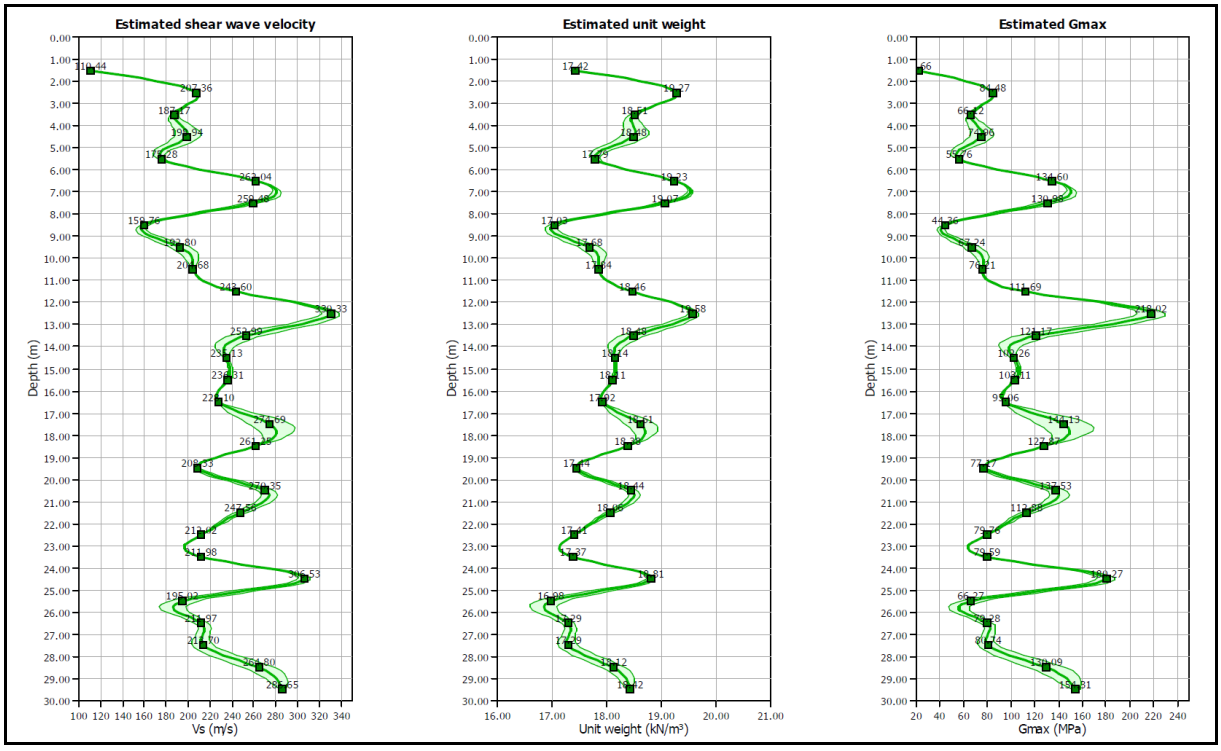
Al netto di piccole variazioni in senso laterale e in senso verticale, cosa comunque normale nell'ambiente deposizionale nel quale si inserisce il sito, si rileva lungo tutta la verticale delle indagini una buona omogeneità stratigrafica con netta prevalenza di terreni sabbiosi fino alla massima profondità d'indagine.

Falda

Al termine delle prove penetrometriche è stata rilevata la presenza di acqua all'interno dei fori d'indagine, tramite l'utilizzo di una sonda freatimetrica, la quale è stata rinvenuta a profondità compresa tra -0,35 m e -0,80 m dai punti di prova.

Velocità onde Vs

Nel corso dell'indagine denominata SCPTU1, sono state eseguite le registrazioni dei tempi di arrivo delle onde Vs a determinate profondità. Tramite il software SPAS della ditta Geologismiki, si elabora il segnale ed i tempi di arrivo delle onde S in modo da ottenere il valore di Vs alle varie profondità per le singole battute (destra e sinistra) dalle quali poi ottenere i valori medi di Vs.



Il valore di Vs calcolato sulla SCPTU3 restituisce un valore pari a **Vs,eq = 226,91 m/s**.

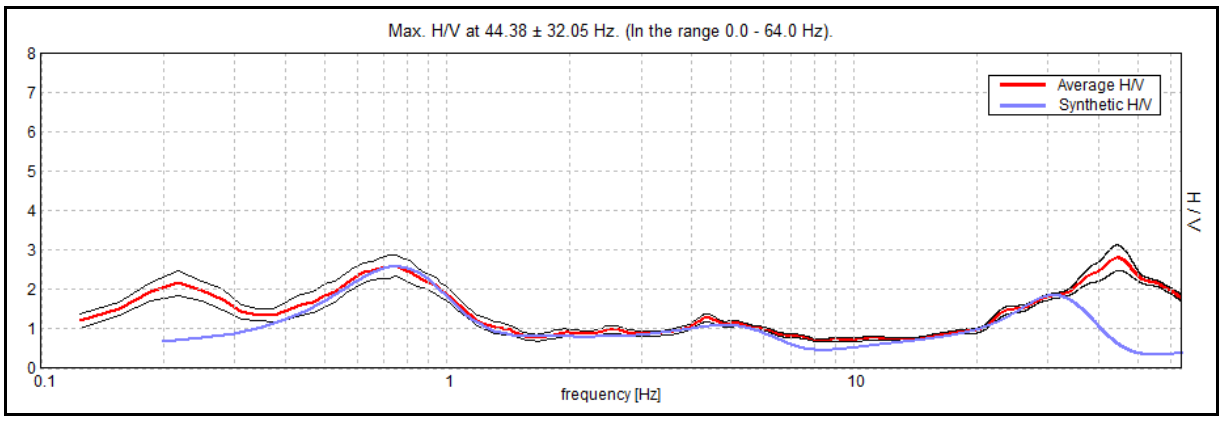
Indagine sismica passiva a stazione singola

È stata eseguita n. 1 misura ubicata come da planimetria alle pagine precedenti (HVSR1).

Di seguito si riporta l'elaborazione del grafico sperimentale della misura, partendo dalle misure di Vs che si estraggono dalla precedente indagine SCPTU1, per quanto riguarda i primi 30 m circa di sottosuolo; i sismo-strati più profondi vengono quindi ricostruiti interpolando il grafico nel miglior modo possibile anche sulla base di informazioni stratigrafiche e sismiche derivate da bibliografia o da indagini d'archivio, in particolare da stratigrafie profonde di perforazioni che sono registrate nel geoportale di ISPRA.

HVSR1

H/V SPERIMENTALE vs. H/V SINTETICO

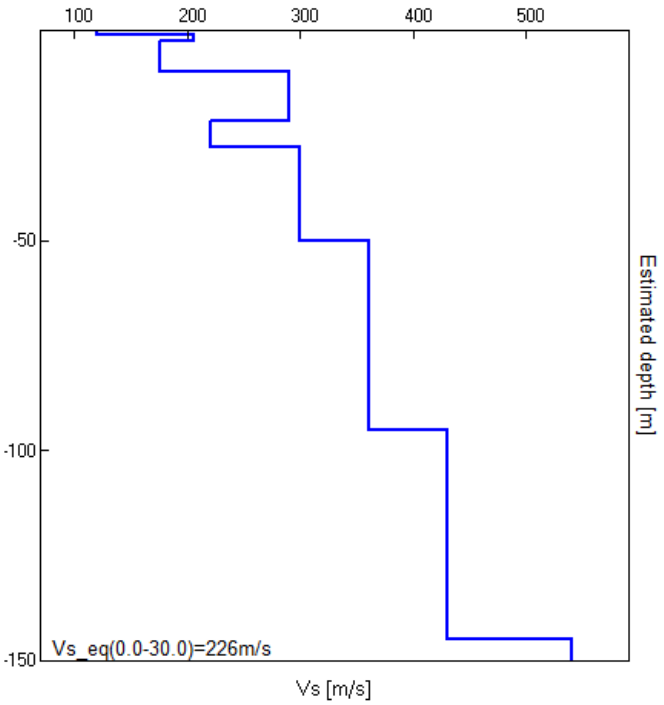


Depth at the bottom of the layer [m]	Thickness [m]	Vs [m/s]	Poisson ratio
1.00	1.00	120	0.48
2.60	1.60	205	0.48
9.60	7.00	175	0.48
21.50	11.90	290	0.47
27.60	6.10	220	0.48
50.00	22.40	300	0.47
95.00	45.00	360	0.48
145.00	50.00	430	0.46
inf.	inf.	540	0.46

Vs_eq(0.0-30.0) = 226 m/s

Non è evidente un vero e proprio picco che indichi il passaggio al bedrock sismico, si ha piuttosto un graduale aumento delle Vs.
L'elaborazione del grafico sperimentale ha permesso di determinare il seguente profilo sismico del terreno più possibile profondo, senza tuttavia raggiungere una Vs di 800 m/s.

Di seguito il profilo ricostruito delle Vs con la profondità; l'elaborazione evidenzia che l'incremento delle Vs con la profondità, in questo contesto, è piuttosto regolare, senza contrasti di impedenza significativi e bruschi.
Ci si aspetta dunque che il raggiungimento del bedrock sismico avvenga in modo graduale e ad elevate profondità.



Categoria sismica di sottosuolo

Ai fini della definizione dell'azione sismica di progetto (come riportato nel vigente D.M. 17 gennaio 2018), si rende necessario valutare l'effetto della risposta sismica locale mediante specifiche analisi. In mancanza di tali analisi, si può fare riferimento ad un approccio semplificato che si basa sull'individuazione di categorie di sottosuolo di riferimento.

Ai fini della identificazione della categoria di sottosuolo, viene valutato il parametro denominato "Velocità Equivalente", calcolata in modo analogo alla precedente Vs,30, che invece di estendere la media pesata fino ai 30 m di profondità, viene valutata entro una profondità H (pari a 30 m o inferiore). La discriminante della profondità H è il raggiungimento del "substrato" caratterizzato da velocità superiori agli 800 m/s.

I valori di Vs sono quindi ottenuti mediante specifiche prove oppure, con giustificata motivazione e limitatamente all'approccio semplificato, sono stati valutati tramite relazioni empiriche di comprovata affidabilità con i risultati di altre prove in sito.

Per velocità equivalente di propagazione delle onde di taglio si intende la media pesata delle velocità delle onde S negli strati nei primi metri di profondità dal piano di posa della fondazione, secondo la relazione:

$$Vs,eq = \frac{H}{\sum_{strato=1}^{N} \frac{h(strato)}{Vs(strato)}}$$

Dove N è il numero di strati individuabili nei primi metri di suolo, ciascuno caratterizzato dallo spessore h (strato) e dalla velocità delle onde S Vs (strato).
Per H si intende la profondità del substrato, definito come quella formazione costituita da roccia o terreno molto rigido, caratterizzato da Vs non inferiore a 800 m/s.
Per depositi con profondità H del substrato superiore a 30 m, la velocità equivalente delle onde di taglio Vs,eq è definita dal parametro Vs,30 ottenuto ponendo H = 30 m nella precedente espressione e considerando le proprietà degli strati di terreno fino a tale profondità.

Dall'analisi dei risultati ottenuti con la prova SCPTU1 e dall'indagine sismica HVSR, ai fini delle prescrizioni della vigente normativa in materia (O.P.C.M 3274/2003 e successive modifiche ed integrazioni e D.M. 17.01.2018) e alla luce di quanto sopra è possibile verificare come il suolo di fondazione del sito, oggetto di studio, vada a ricadere in **categoria sismica C.**
A tale categoria appartengono *depositi di terreni a grana grossa mediamente addensati o terreni a grana fina mediamente consistenti*, con profondità del substrato superiori a 30 m, caratterizzati da un miglioramento delle proprietà meccaniche con la profondità e da valori di velocità equivalente compresi tra 180 m/s e 360 m/s.

Ricostruzione modello stratigrafico profondo

Al fine di ricostruire con maggior dettaglio le litologie che interessano il sottosuolo nell'area di interesse, sono state ricercate alcune stratigrafie profonde relative a perforazioni del database di ISPRA (http://geoportale.isprambiente.it/); nel territorio immediatamente circostante al sito di interesse sono stati reperiti alcuni dati di perforazioni profonde.
Di seguito si riportano alcune schede tecniche di perforazioni estratte dal **Geoviewer del sito ISPRA**.





ISPRA
Istituto Superiore per la Protezione e la Ricerca Ambientale

Sistema Nazionale per la Protezione dell'Ambiente

Istituto Superiore per la Protezione e la Ricerca Ambientale

Archivio nazionale delle indagini nel sottosuolo (Legge 464/1984)

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Perforazione 1

STRATIGRAFIA

Progr	Da profondità (m)	A profondità (m)	Spessore (m)	Età geologica	Descrizione litologica
1	0,00	3,00	3,00		TERRENO VEGETALE
2	3,00	10,00	7,00		ARGILLA
3	10,00	16,00	6,00		ARGILLA SABBIOSA
4	16,00	24,00	8,00		ARGILLA CON TORBA
5	24,00	37,00	13,00		TORBA SABBIOSA
6	37,00	46,00	9,00		LIMO E ARGILLA MOLLE
7	46,00	53,00	7,00		SABBIA MEDIA
8	53,00	65,00	12,00		ARGILLA
9	65,00	75,00	10,00		TORBA FRIABILE
10	75,00	91,00	16,00		LIMO ARGILLOSO CON TORBA
11	91,00	109,00	18,00		SABBIA CON TORBA
12	109,00	132,00	23,00		ARGILLA SABBIOSA
13	132,00	150,00	18,00		SABBIA MEDIA CON FOSSILI
14	150,00	155,00	5,00		ARGILLA SABBIOSA

Perforazione 2

STRATIGRAFIA

Progr	Da profondità (m)	A profondità (m)	Spessore (m)	Età geologica	Descrizione litologica
1	0,00	36,00	36,00		TERRA CON STRATI DI ARGILLA
2	36,00	40,00	4,00		SABBIA MEDIA
3	40,00	63,00	23,00		STRATI DI ARGILLA E TORBA
4	63,00	66,00	3,00		SABBIA MEDIA
5	66,00	105,00	39,00		STRATI DI ARGILLA E TORBA
6	105,00	108,00	3,00		SABBIA MEDIA
7	108,00	122,00	14,00		ARGILLA COMPATTA
8	122,00	137,00	15,00		GHIAINO

Perforazione 3

STRATIGRAFIA

Progr	Da profondità (m)	A profondità (m)	Spessore (m)	Età geologica	Descrizione litologica
1	0,00	3,00	3,00		TERRENO VEGETALE
2	3,00	18,00	15,00		ARGILLA
3	18,00	23,00	5,00		SABBIA MEDIA
4	23,00	74,00	51,00		ARGILLA SABBIOSA
5	74,00	82,00	8,00		ARGILLA CON TORBA
6	82,00	99,00	17,00		ARGILLA MISTA
7	99,00	111,00	12,00		SABBIA FINE
8	111,00	123,00	12,00		ARGILLA
9	123,00	141,00	18,00		SABBIA CON FOSSILI

Le perforazioni riportate alla pagina seguente, evidenziano nel complesso che gli orizzonti significativi di sabbie medie o ghiaie si intercettano oltre una profondità compresa circa tra -120 e -150 m dal piano campagna.

FONDAMENTI DI RISPOSTA SISMICA LOCALE

La definizione dell'azione sismica di progetto consiste nel definire i carichi dinamici dovuti ad uno scuotimento sismico, che agiscono sulla struttura in progetto in aggiunta ai carichi statici, e alla definizione del loro contenuto in frequenza in termini di spettro di risposta elastico (su terreno roccioso o rigido) o in termini di spettro di progetto se riferito ad una struttura di determinate caratteristiche.
Le normative tecniche permettono di definire, per determinate opere e condizioni, l'azione sismica con metodi semplificati differenziando gli spettri di pericolosità di base solamente in funzione delle categorie di sottosuolo e delle categorie topografiche e per determinati valori di probabilità di eccedenza (definiti per ciascuno Stato Limite).
L'analisi di Risposta Sismica locale consente di tenere in conto con maggiore dettaglio le condizioni specifiche del sito e definire pertanto con maggiore dettaglio il valore dell'azione sismica di progetto, sempre in termini di accelerazione massima attesa al suolo (o alla base delle fondazioni) e del relativo contenuto in frequenza.
Il moto generato da un terremoto in un sito, infatti, dipende dalle particolari condizioni locali; l'analisi di risposta sismica locale consente di definire le modifiche che un segnale sismico in ingresso subisce a causa dei cosiddetti fattori locali.
Come enunciato al punto 7.11.3.1 delle recenti NTC2018, nell'analisi di risposta sismica locale l'azione sismica di ingresso è definita in termini di storia temporale dell'accelerazione (accelerogrammi) su di un sito di riferimento rigido ed affiorante con superficie topografica orizzontale. Come verrà ripreso più avanti, per la scelta degli accelero grammi si fa riferimento alle indicazioni del punto 3.2.3.6 delle NTC per la definizione dell'azione sismica.

Le basi per l'analisi di risposta sismica locale richiedono essenzialmente due tipi di input:
1 – la sismicità di base del sito
2 – la ricostruzione del modello del sottosuolo o sismo-stratigrafia
L'approccio numerico si snoda nelle seguenti fasi fondamentali:

- Definizione della geometria del problema (ad esempio 1D monodimensionale...);
- Caratterizzazione dinamica dei terreni coinvolti;
- Scelta di terremoti di input;
- Utilizzo del codice di calcolo.

L'output fornito dal codice di calcolo consiste nella definizione del moto del suolo previsto in superficie o alla base delle fondazioni, in termini di accelerogramma output o di spettro di risposta elastico e permette il calcolo del Fattore di amplificazione.

Ricostruzione stratigrafica ai fini della Risposta Sismica Locale

Per quanto riguarda la caratterizzazione dei terreni necessita sottolineare che il software utilizzato ai fini della presente analisi utilizza il "metodo lineare equivalente" che permette di tenere conto, al procedere delle iterazioni del calcolo, del variare dei parametri quali rigidezza e smorzamento dei diversi tipi di materiali che costituiscono gli orizzonti stratigrafici, parametri che infatti in natura variano al variale del grado di deformazione.
In bibliografia, così come all'interno del software stesso, è possibile reperire i grafici di rigidezza e smorzamento per ciascun tipo di materiale ed assegnare pertanto la categoria più adatta a ciascun sismo-strato considerato.
Il dettaglio del modello stratigrafico o sismo-stratigrafico utilizzato per il presente studio è riportato nei report finali delle analisi di RSL eseguite.
Alle pagine seguenti si riporta una tabella riassuntiva (modello sismo-stratigrafico di input) dei parametri di partenza introdotti per ciascun orizzonte.

La sismo-stratigrafia è stata ricostruita, per la porzione più superficiale di sottosuolo, innanzitutto dai risultati delle indagini condotte nel sito in esame e mediante l'interpretazione delle indagini sismiche quali la prova SCPTU1 e la misura HVSR1, la cui ubicazione è rappresentata ai capitoli precedenti.
Le informazioni stratigrafiche delle perforazioni profonde presentate ai capitoli precedenti permettono di osservare che in questo contesto il raggiungimento del bedrock sismico non può essere attribuito al raggiungimento di una formazione litoide.
Dal punto di vista del profilo sismico del sottosuolo, considerando in particolare il contesto geologico in cui ci poniamo, si evidenzia che il passaggio a valori di Vs > 800 m/s non necessariamente corrisponde al passaggio al substrato roccioso e il bedrock sismico può anche essere attribuito semplicemente al primo contrasto di impedenza significativo, non necessariamente corrispondente al passaggio verso Vs>800 m/s, oppure raggiunto in modo graduale con la profondità.

L'elaborazione delle indagini sismiche eseguite, in parallelo all'osservazione delle stratigrafie profonde, ha condotto al seguente modello sismo-stratigrafico:

Modello sismo-stratigrafico di input (per RSL)

n. strato	**Spessore [m]**	**Profondità da p.c. [m]**	**Litologia**	**Vs (m/s)** media dello strato	**Densità (kN/m^3)** media dello strato	**Gmax (Mpa)** calcolato da Vs e D
1	1.0	0.0 – 1.0	Argilla prevalente	120	17.5	25.69
2	1.6	1.0 – 2.6	Argilla e limo consistenti	205	18.0	77.11
3	7.0	2.6 – 9.6	Argilla e argilla limosa	175	18.6	58.07
4	11.9	9.6 – 21.5	Sabbia addensata	290	19.0	162.88
5	6.1	21.5 – 27.6	Sabbia e sabbia limosa	220	19.5	96.21
6	22.4	27.6 – 50.0	Sabbia addensata	300	20.0	183.49
7	45.0	50.0 – 95.0	Argilla e argilla limosa	360	21.0	277.43
8	50.0	95.0 – 145.0	Sabbia addensata prevalente	430	22.0	414.66
9	--	>145.0	Sabbia prevalente (si considera il bedrock)	540.0	23.0	683.67

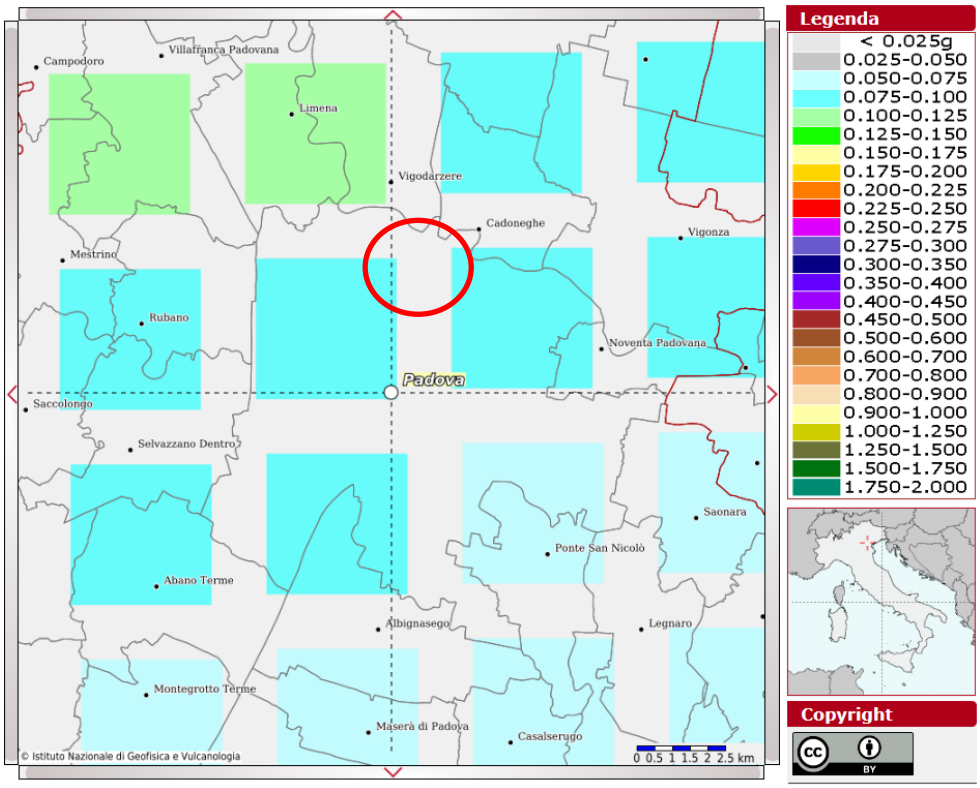
La soggiacenza minima della falda nell'area in esame viene considerata a circa -1,0 m rispetto al piano campagna.

SISMICITÀ DI BASE DEL SITO

Il secondo step di una Risposta Sismica Locale è la definizione della pericolosità sismica di base, con la quale si intende lo scuotimento del suolo, in condizioni di campo libero, atteso in un determinato punto del territorio. Nelle normative NTC2018 nella pericolosità sismica entra anche il concetto probabilistico e si intende infatti come "lo scuotimento del suolo atteso in un dato sito con una certa probabilità di eccedenza in un dato intervallo di tempo, ovvero la probabilità che un certo valore di scuotimento si verifiche in un dato intervallo".

Per il territorio italiano i parametri di riferimento che esprimono la pericolosità sismica di base sono disponibili per una griglia di punti, per diversi valori di probabilità, e sono disponibili nel sito dell'INGV (mappa interattiva di pericolosità sismica).

Sulla base della "Deliberazione della Giunta Regionale n. 244 del 09 marzo 2021 - Aggiornamento dell'elenco delle zone sismiche del Veneto. D.P.R. 6 giugno 2001, n. 380, articolo 83, comma 3; D. Lgs 31 marzo 1998, n. 112, articoli 93 e 94. D.G.R./CR n. 1 del 19/01/2021", il Comune di Padova ricade in zona sismica **3**.



Estratto mappa sismica *(OPCM 3519/2006)*

La mappa rappresenta il modello di pericolosità sismica per l'Italia e i diversi colori indicano il valore di scuotimento (PGA = Peak Ground Acceleration; accelerazione di picco del suolo, espressa in termini di g, l'accelerazione di gravità) atteso con una probabilità di eccedenza pari al 10% in 50 anni su suolo rigido (classe A, Vs30 > 800 m/s) e pianeggiante.

Sulla base dell'Ordinanza PCM del 28 aprile 2006 n. 3519 l'area in esame è caratterizzata da valori di accelerazione massima al suolo a_g, (con probabilità di superamento del 10% in 50 anni, riferita a suoli rigidi caratterizzati da valori di Vs30 > di 800 m/s) compresi fra 0,075 e 0,100 g.

Pericolosità di base da NTC

Le forme degli spettri di risposta ai sensi delle NTC 2018 sono definite, per ciascuna delle probabilità di superamento nel periodo di riferimento P_{VR}, a partire dai valori dei seguenti parametri su sito di riferimento rigido orizzontale:

a_g : accelerazione orizzontale massima al sito;

Fo : valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale;

T_C* : periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale.

Il sito di interesse presenta le seguenti coordinate:

Coordinate	Datum ED50	WGS84
Latitudine	45,434155	45,433244
Longitudine	11,892221	11,891225

Il periodo di riferimento V_R si ricava per ciascun tipo di costruzione, moltiplicando la vita nominale V_N per il coefficiente d'uso C_U definito, al variare della classe d'uso.

La **vita nominale V_N** relativa al presente intervento di progetto è di 50 anni (tipo di costruzione 2 "*Opere ordinarie, ponti, opere infrastrutturali e dighe di dimensioni contenute o di importanza normale*").

La classe d'uso utilizzata è:

Classe III: "*Costruzioni il cui uso preveda affollamenti significativi. Industrie con attività pericolose per l'ambiente. Reti viarie extraurbane non ricadenti in Classe d'uso IV. Ponti e reti ferroviarie la cui interruzione provochi situazioni di emergenza. Dighe rilevanti per le conseguenze di un loro eventuale collasso*"

A tale classe corrisponde un coefficiente d'uso C_U pari a 1,5.
In questo modo si ottiene un periodo di riferimento V_R di 75 anni.

Le probabilità di superamento nel periodo di riferimento P_{VR}, cui riferirsi per individuare l'azione sismica agente in ciascuno degli stati limite considerati, sono riportate nella successiva tabella.

Stati Limite	**PVR: Probabilità di superamento nel periodo di riferimento V_R**		**T_R (anni)**
Stati limite di esercizio	**SLO**	81%	45
	SLD	63%	75
Stati limite ultimi	**SLV**	10%	712
	SLC	5%	1462

Probabilità di superamento PVR e periodo di ritorno TR

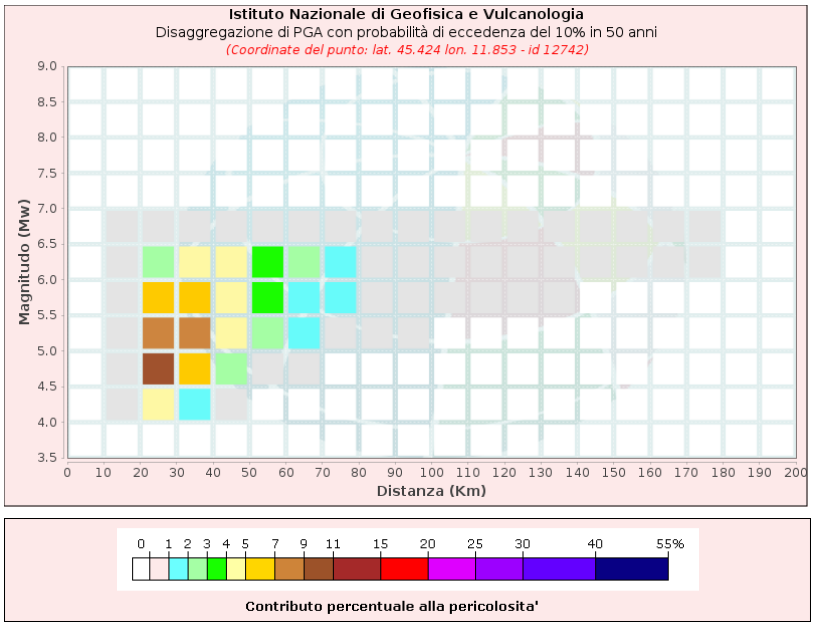
I parametri a_g, F_o, T_C* per i periodi di riferimento corrispondenti agli stati limite considerati sono di seguito riportati in forma tabulare.

STATO LIMITE	**T_R (anni)**	**a_g (g)**	**F_0 (-)**	**T_{c^*} (s)**
SLO	45	0,036	2,558	0,244
SLD	75	0,044	2,536	0,279
SLV	712	0,103	2,575	0,340
SLC	1462	0,132	2,580	0,352

Valori ag, F0,TC per i diversi stati limite*

Partendo dalla mappa interattiva di pericolosità sismica (sito INGV) è possibile ottenere l'analisi della probabilità di avvenimento di determinati eventi sismici in termini di Magnitudo e Distanza epicentrale aventi maggiore probabilità per un determinato punto della griglia della mappa stessa.

Tale elaborazione, definita "disaggregazione", viene riportata di seguito in estratto per il territorio in esame.



Il grafico rappresenta il contributo percentuale delle possibili coppie di valori di magnitudo-distanza epicentrale alla pericolosità del nodo, rappresentata in questo caso dal valore della PGA mediana, per una probabilità di eccedenza del 10% in 50 anni.

La tabella seguente riporta i valori mostrati nel grafico ed i valori medi di magnitudo, distanza ed epsilon.

Disaggregazione di PGA con probabilità di eccedenza del 10% in 50 anni (Coordinate del punto: lat. 45.424 lon. 11.853 - id 12742)

Distanza (Km)	Magnitudo (Mw)										
	3.5-4.0	4.0-4.5	4.5-5.0	5.0-5.5	5.5-6.0	6.0-6.5	6.5-7.0	7.0-7.5	7.5-8.0	8.0-8.5	8.5-9.0
0-10	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
10-20	0.0000	0.3450	0.7190	0.4570	0.2340	0.0993	0.0106	0.0000	0.0000	0.0000	0.0000
20-30	0.0000	4.1600	10.2000	8.1100	5.1900	2.7500	0.3400	0.0000	0.0000	0.0000	0.0000
30-40	0.0000	1.9200	6.6200	7.3800	6.3000	4.3500	0.6310	0.0000	0.0000	0.0000	0.0000
40-50	0.0000	0.3220	2.8000	4.5100	4.8200	4.0200	0.6510	0.0000	0.0000	0.0000	0.0000
50-60	0.0000	0.0000	0.7360	2.4100	3.2300	3.1900	0.5680	0.0000	0.0000	0.0000	0.0000
60-70	0.0000	0.0000	0.0669	1.0300	1.9300	2.1500	0.4150	0.0000	0.0000	0.0000	0.0000
70-80	0.0000	0.0000	0.0000	0.3960	1.2300	1.4000	0.2820	0.0000	0.0000	0.0000	0.0000
80-90	0.0000	0.0000	0.0000	0.0904	0.6700	0.8440	0.1770	0.0000	0.0000	0.0000	0.0000
90-100	0.0000	0.0000	0.0000	0.0069	0.3420	0.5290	0.1180	0.0000	0.0000	0.0000	0.0000
100-110	0.0000	0.0000	0.0000	0.0000	0.1430	0.3340	0.0804	0.0000	0.0000	0.0000	0.0000
110-120	0.0000	0.0000	0.0000	0.0000	0.0403	0.1860	0.0509	0.0000	0.0000	0.0000	0.0000
120-130	0.0000	0.0000	0.0000	0.0000	0.0079	0.1040	0.0332	0.0000	0.0000	0.0000	0.0000
130-140	0.0000	0.0000	0.0000	0.0000	0.0005	0.0828	0.0324	0.0000	0.0000	0.0000	0.0000
140-150	0.0000	0.0000	0.0000	0.0000	0.0000	0.0561	0.0282	0.0000	0.0000	0.0000	0.0000
150-160	0.0000	0.0000	0.0000	0.0000	0.0000	0.0237	0.0162	0.0000	0.0000	0.0000	0.0000
160-170	0.0000	0.0000	0.0000	0.0000	0.0000	0.0083	0.0085	0.0000	0.0000	0.0000	0.0000
170-180	0.0000	0.0000	0.0000	0.0000	0.0000	0.0015	0.0027	0.0000	0.0000	0.0000	0.0000
180-190	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0001	0.0000	0.0000	0.0000	0.0000
190-200	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

Valori Medi		
Magnitudo	Distanza	Epsilon
5.45	40.7	1.51

DEFINIZIONE DELLE AZIONI DI INPUT

La normativa italiana NTC2018 e la relativa Circolare esplicativa affrontano i metodi per la definizione dell'azione sismica di ingresso al punto 3.2.3 ed in particolare al 3.2.3.6 si introduce il concetto dell'utilizzo delle storie temporali del moto del terreno; si fa esplicito riferimento all'uso di accelerogrammi registrati per le analisi dinamiche di opere e sistemi geotecnici. In particolare essi devono essere adeguatamente scalati in modo da approssimare al meglio gli spettri di risposta nel campo di periodi di interesse per il problema in esame.
L'obiettivo dello studio consiste nel rappresentare il moto sismico atteso in superficie nella forma utile al fine progettuale ed in particolare valutare quanto esso si discosti dal moto al bedrock potendo quindi quantificare eventuali effetti di amplificazione.

La ricerca dei terremoti di input deve partire dalla sismicità di base del sito e dalla estrazione di dati disaggregati relativi alle coppie ad esempio di Magnitudo (M) e Distanza epicentrale (R). La scelta finale dei dati utilizzati nella ricerca di accelerogrammi deve essere eseguita pertanto anche in relazione alla tipologia di struttura che si sta verificando, in relazione cioè ai sui peridi di vibrazione, poiché al variare di M e R varia il contenuto in frequenza ed il valore di ampiezza del moto sismico di input.

La ricerca di accelerogrammi è stata svolta con l'utilizzo di REXELweb.
REXELweb è uno strumento online disponibile sul sito di ITACA4.0 e ESM (banche dati di registrazioni accelerometriche italiane ed europee) che fornisce un'interfaccia web guidata e di facile utilizzo, per la ricerca di accelerogrammi registrati compatibili – in media – con un assegnato spettro target, per l'analisi dinamica in ambito di ingegneria strutturale e geotecnica. REXELweb si basa sullo stesso codice di calcolo del programma REXEL; sviluppato dall'Università degli Studi di Napoli Federico II nell'ambito delle attività di ReLUIS) e sostituisce REXELite (la precedente versione online semplificata di REXEL).
L'utilizzo di REXELweb va citato come: *Sgobba, S., Felicetta, C., Russo, E., D'Amico, M., Lanzano, G., Pacor F., Luzi, L., Baraschino, R., Baltzopoulos, G., Iervolino, I. The online graphical user interface of REXELweb for the selection of accelerograms from the Engineering Strong Motion database (ESM). 39° Convegno Nazionale Gruppo Nazionale Geofisica della Terra Solida (GNGTS), 22 – 24 giugno 2021 (online).*

Le analisi RSL, nel caso in esame, sono state condotte per gli stati limite SLD e SLV.

ANALISI DI RISPOSTA SISMICA LOCALE

Per l'elaborazione della Risposta Sismica Locale viene utilizzato il software RSL III di Geostru.
Si introducono i dati di base del sito e si caricano i 7 accelerogrammi della relativa combinazione considerata.
La procedura che segue passo passo il software consente di ottenere lo spettro in accelerazione, velocità e spostamento ottenuto partendo dal moto di input assegnato al bedrock di riferimento e trasferito in superficie, dopo l'introduzione del modello sismo-stratigrafico del sottosuolo.

Ottengo due tipologie di output:

1. Il confronto tra il moto di input e quello di output permette di valutare l'eventuale amplificazione in termini di accelerazione (calcolata per ciascuna traccia);

2. Il rapporto fra lo spettro in superficie (spettro di output) e lo spettro al bedrock (spettro di input) eseguito in determinate finestre spettrali permette di ottenere i fattori di amplificazione secondo le ICMS (fattori di amplificazione FA ed FV da applicare alle ordinate spettrali a basso periodo FA e alto periodo FV).

Per il calcolo di questi due fattori è stata utilizzata la procedura descritta negli ICMS (§ 2.5.3.3).
Il fattore FA si calcola attraverso la seguente espressione:

$$FA = \frac{SAm_o}{SAm_i}$$

dove SAm_i e SAm_o rappresentano i valori medi degli spettri di input e di output calcolati nell'intorno del periodo di massimo valore dello spettro di input e di output (TA); l'espressione per il calcolo del valore medio è la seguente:

$$SAm = \frac{1}{TA} \int_{t_1}^{t_2} SA(t)\, dt$$

dove:
- SA(t): spettro in pseudoaccellerazione;
- TA: massimo valore del periodo dello spettro;

- t_1: estremo di integrazione pari a 0.5*TA;
- t_2: estremo di integrazione pari a 1.5*TA.

Gli spettri in pseudovelocità si ricavano dagli spettri in pseudoaccellerazione secondo la seguente espressione:

$$SV(t) = SA(t) \cdot \frac{T}{2\pi}$$

Dagli spettri in pseudovelocità si ricava il fattore FV attraverso la seguente espressione:

$$FV = \frac{SVm_o}{SVm_i}$$

dove SVm_i e SVm_o rappresentano i valori medi degli spettri di input e di output in pseudovelocità calcolati nell'intorno del periodo di massimo valore dello spettro di input e di output (TA); l'espressione per il calcolo del valore medio è la seguente:

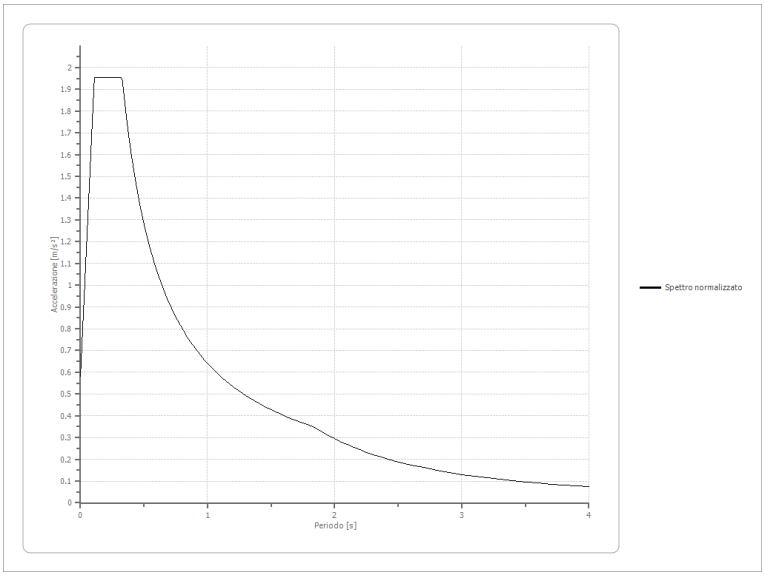
$$SVm = \frac{1}{0.4 \cdot TA} \int_{t_1}^{t_2} SV(t)\, dt$$

dove:
- SV(t) = spettro in psudovelocità;
- TA: massimo valore del periodo dello spettro;
- t_1: estremo di integrazione pari a 0.8*TA;
- t_2: estremo di integrazione pari a 1.2*TA.

Analisi di risposta sismica locale - SLD

Si rimanda all'Allegato 1 per il report completo dell'elaborazione eseguita.

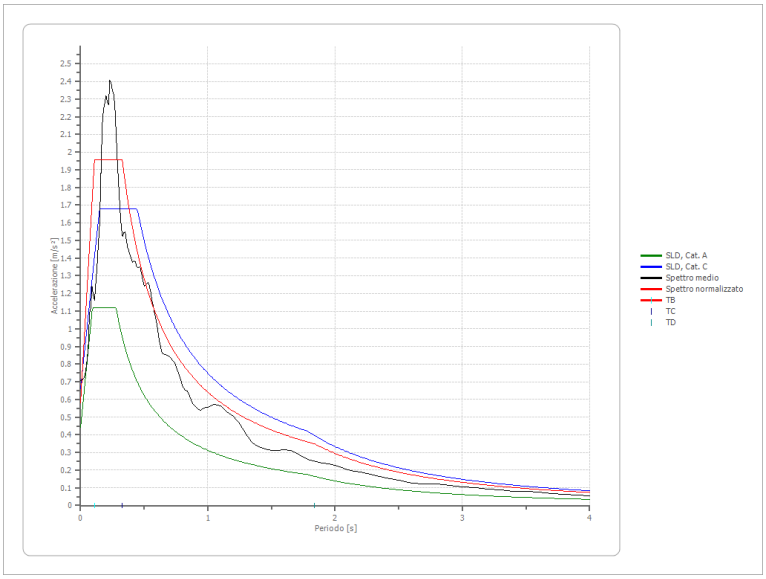
Spettro normalizzato di risposta elastico - SLD



Parametri spettro normalizzato - SLD

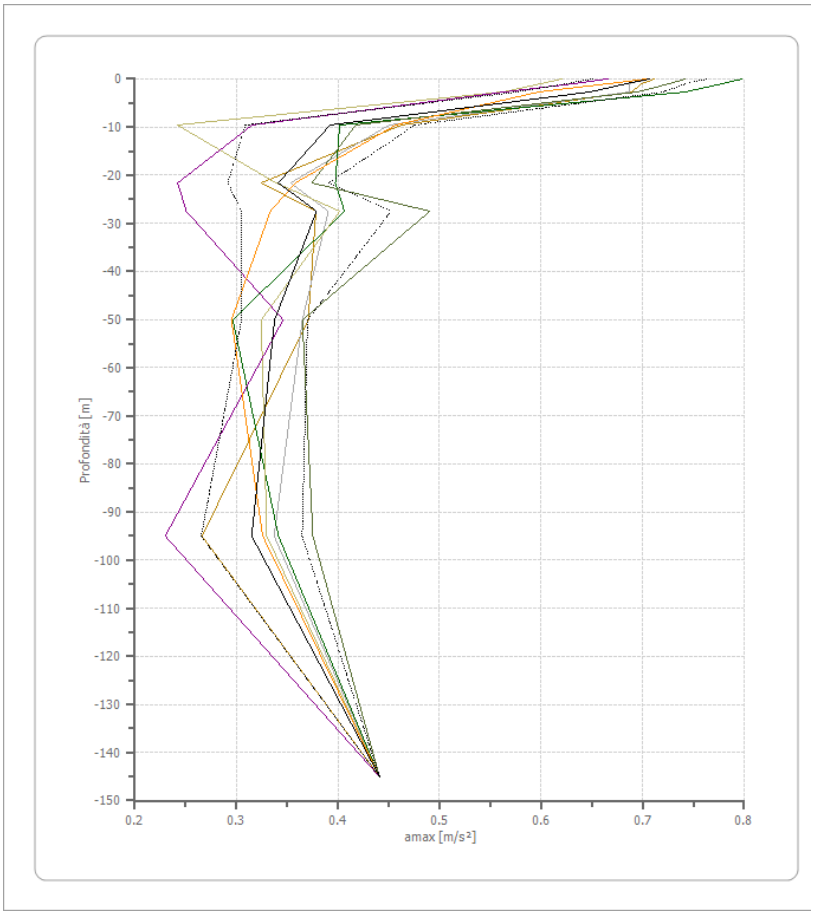
Ag [m/s²]	F0	Tc*	TB [s]	TC [s]	TD [s]	Se(0) [m/s²]	Se(TB) [m/s²]	S
0.581	3.364302	--	0.109	0.328	1.837	0.581	1.955	1.318

Confronto spettro normativa - SLD



Profilo A_max SLD

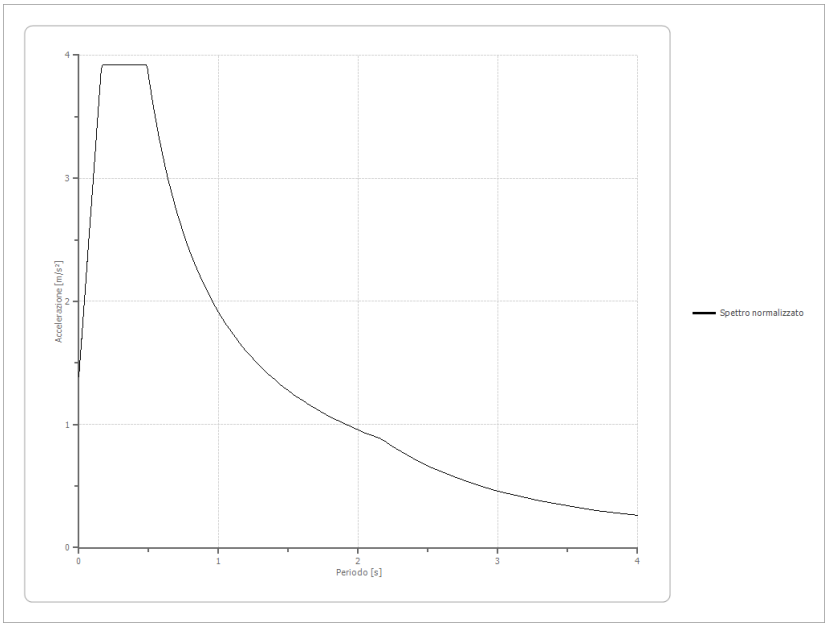
	0.0 [m]	1.0 [m]	2.6 [m]	9.6 [m]	21.5 [m]	27.6 [m]	50.0 [m]	95.0 [m]	145.0 [m]
media [m/s²]	**0.707**	**0.684**	**0.648**	**0.392**	**0.341**	**0.379**	**0.337**	**0.315**	**0.441**
Dev. St. [m/s²]	0.056	0.059	0.072	0.083	0.050	0.073	0.033	0.050	0.000



Analisi allo stato limite SLV

Si rimanda all'Allegato 2 per il report completo dell'elaborazione eseguita.

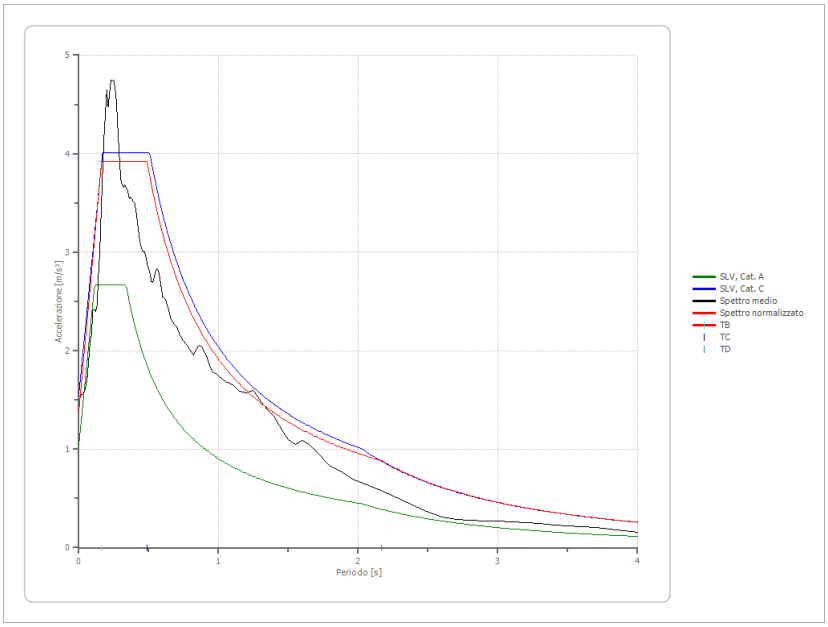
Spettro normalizzato di risposta elastico - SLV



Parametri spettro normalizzato - SLV

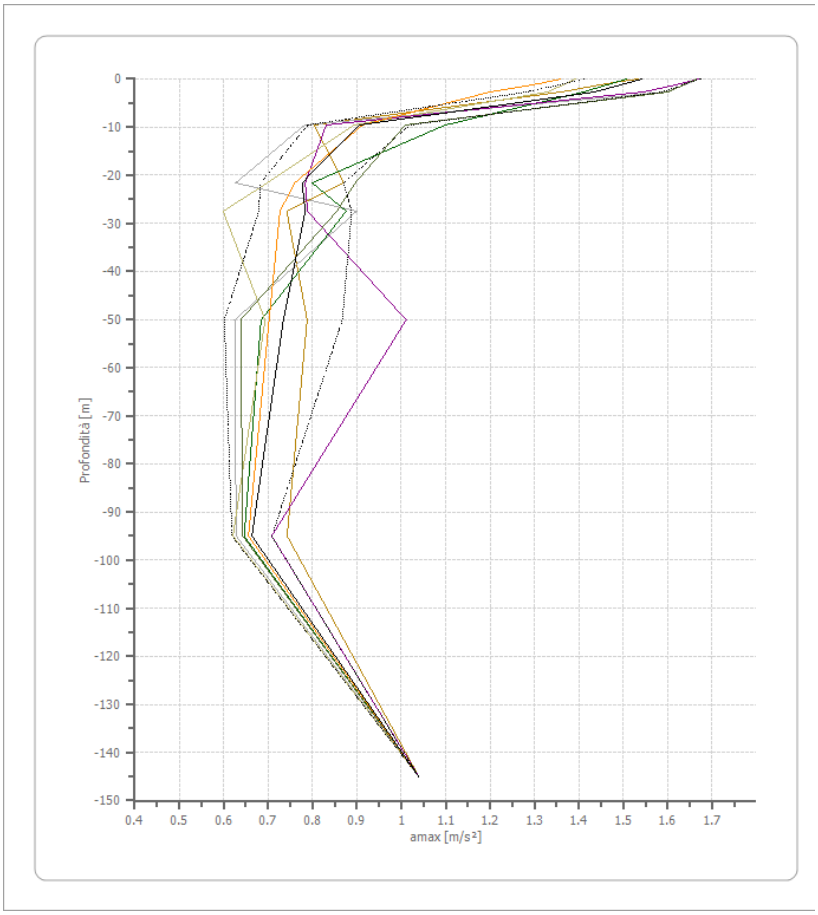
Ag [m/s²]	F0	Tc*	TB [s]	TC [s]	TD [s]	Se(0) [m/s²]	Se(TB) [m/s²]	S
1.386	2.829997	--	0.162	0.487	2.165	1.386	3.923	1.333

Confronto spettro normativa - SLV



Profilo A_max SLV

	0.0 [m]	1.0 [m]	2.6 [m]	9.6 [m]	21.5 [m]	27.6 [m]	50.0 [m]	95.0 [m]	145.0 [m]
media [m/s²]	**1.542**	**1.504**	**1.436**	**0.905**	**0.777**	**0.784**	**0.735**	**0.664**	**1.040**
Dev. St. [m/s²]	0.132	0.137	0.152	0.115	0.093	0.105	0.133	0.045	0.000



SINTESI E CONSIDERAZIONI

Il presente elaborato di Analisi di Risposta Sismica Locale permette di definire con dettaglio i valori delle accelerazioni attese in superficie e gli spettri da considerare per la progettazione.

Stato limite SLD

Dal profilo delle accelerazioni si osserva che la PGA attesa ha un valore medio pari a 0,707 m/s^2; si determina pertanto un rapporto Pga/Pga0 = 1,603 (PGA0= 0,441 m/s^2).

Dal *confronto con gli spettri di normativa* (SLD - suolo C) risulta che, allo stato limite SLD, lo spettro normalizzato determinato dall'analisi di risposta sismica locale risulta superiore al rispettivo spettro di normativa.

Stato limite SLV

Dal profilo delle accelerazioni si osserva che la PGA attesa ha un valore medio pari a 1,542 m/s^2; si determina pertanto un rapporto Pga/Pga0 = 1,483 (PGA0= 1,040 m/s^2).

Dal *confronto con gli spettri di normativa* (SLV - suolo C) risulta che, allo stato limite SLV, lo spettro normalizzato determinato dall'analisi di risposta sismica locale risulta inferiore al rispettivo spettro di normativa.

Dalle analisi RSL condotte risulta che nella situazione in esame sia adeguato considerare i parametri sismici e gli spettri derivati dalla procedura di Analisi di Risposta Sismica Locale per verifiche allo Stato limite SLD; viceversa per verifiche allo Stato limite SLV risulta più cautelativo l'approccio semplificato che considera gli Spettri di normativa NTC.

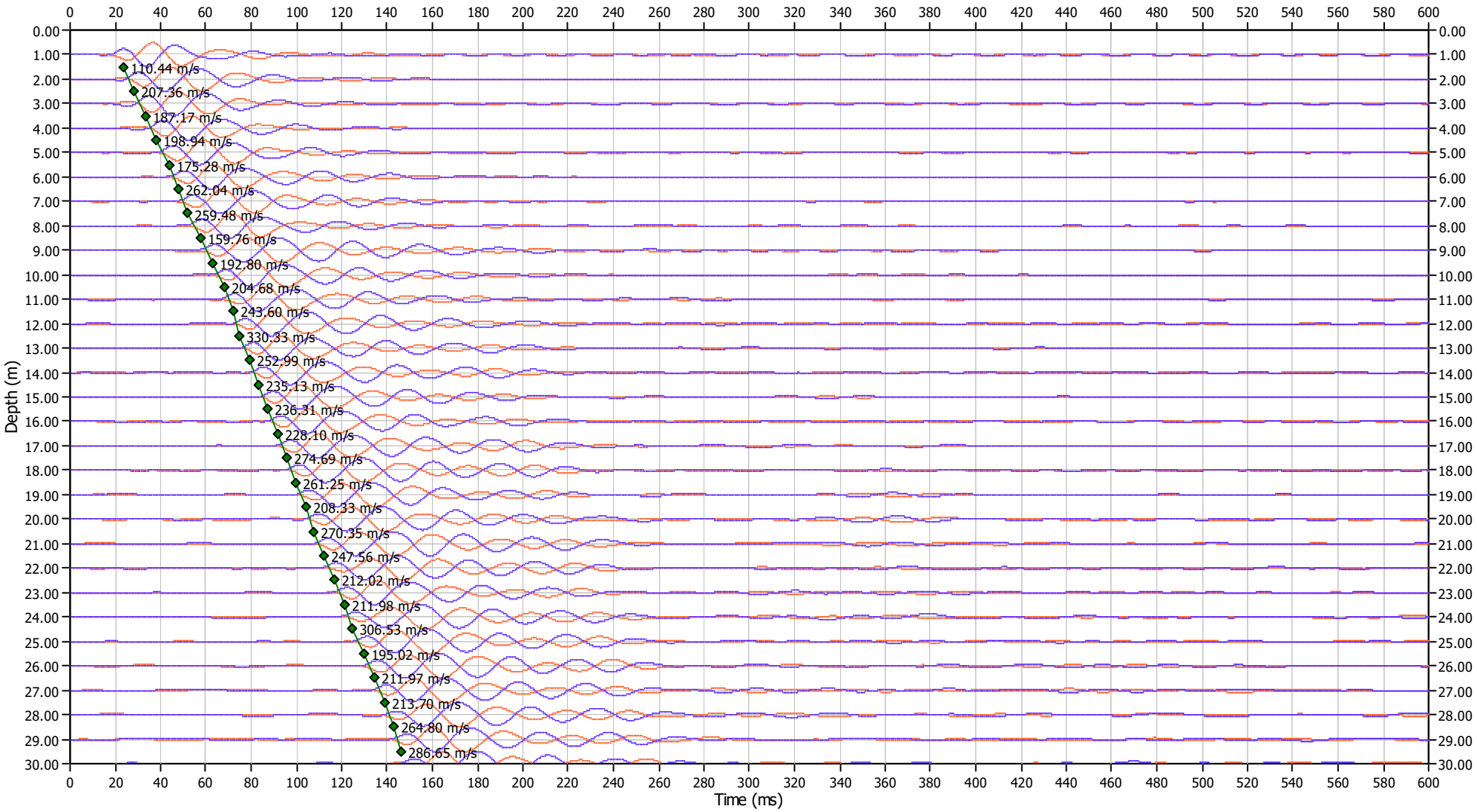
Sarà cura del Progettista valutare le condizioni sismiche più cautelative in relazione alle caratteristiche delle strutture in progetto.

GeoLogismiki
Geotechnical Engineers
Merarhias 56
http://www.geologismiki.gr

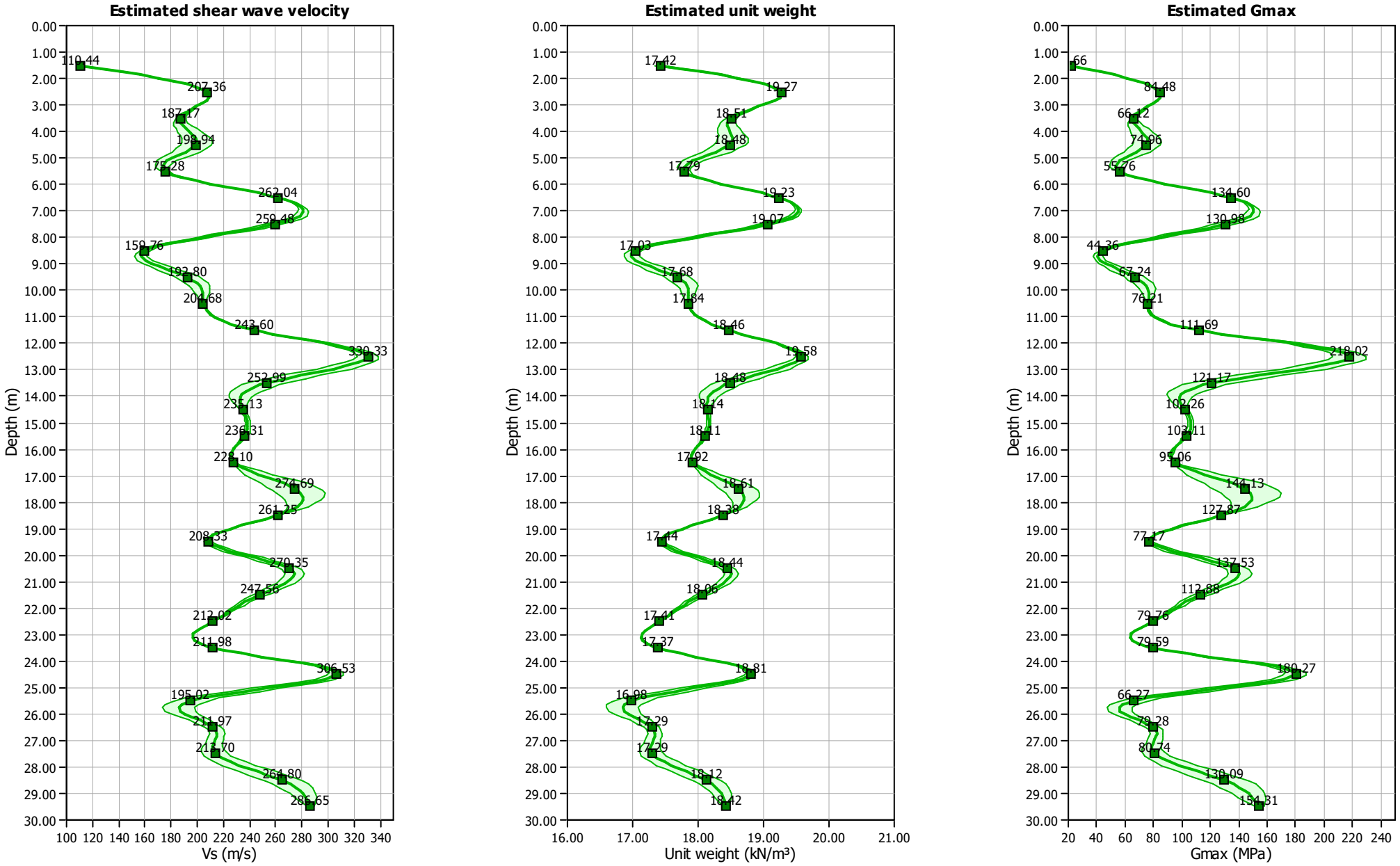
Project:

Borehole ID: SCPTU1

Average S signals full graph (L & R signals)



Detailed result plots over depth



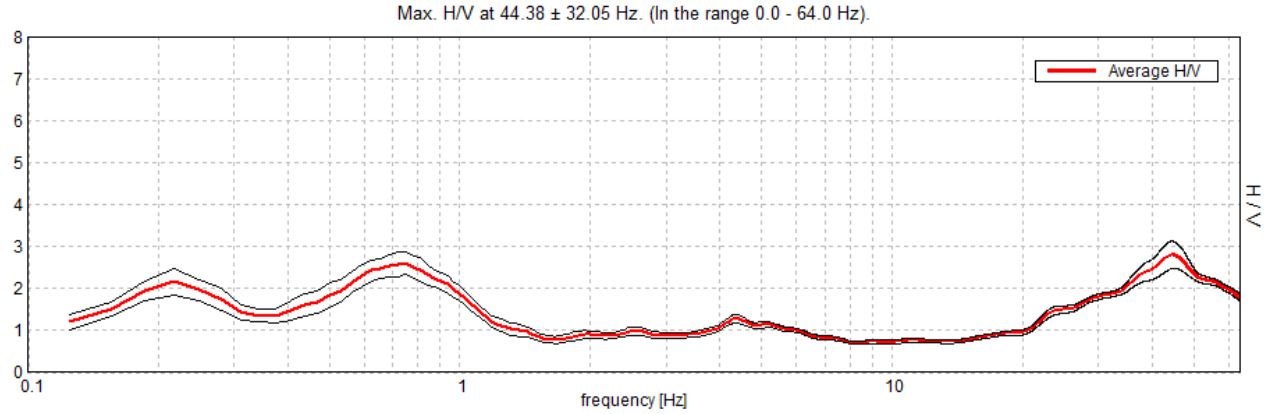
C7999, GEODELTA
Ex Configliachi – via Guido Reni, Padova

Misura sismica passiva a stazione singola HVSR1

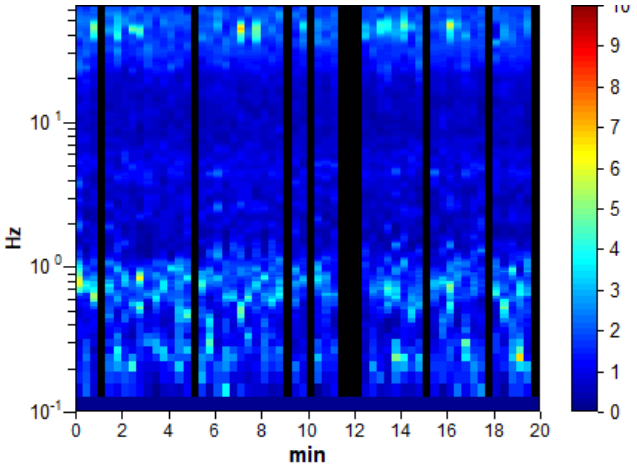
Instrument: TRZ-0027/01-09
Data format: 16 byte
Full scale [mV]: 51
Start recording: 26/02/26 14:59:26 End recording: 26/02/26 15:19:26
Channel labels: NORTH SOUTH; EAST WEST ; UP DOWN
GPS data not available

Trace length: 0h20'00". Analyzed 83% trace (manual window selection)
Sampling rate: 128 Hz
Window size: 20 s
Smoothing type: Triangular window
Smoothing: 10%

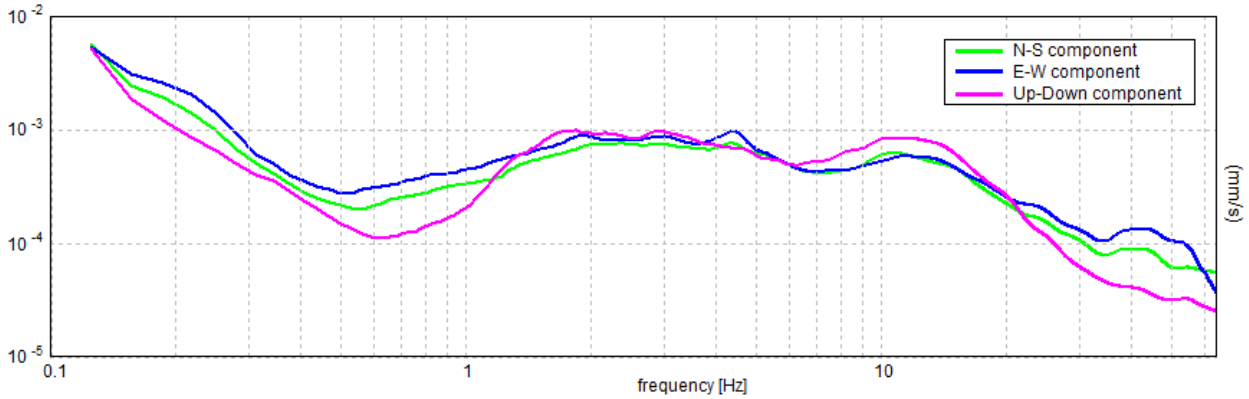
HORIZONTAL TO VERTICAL SPECTRAL RATIO



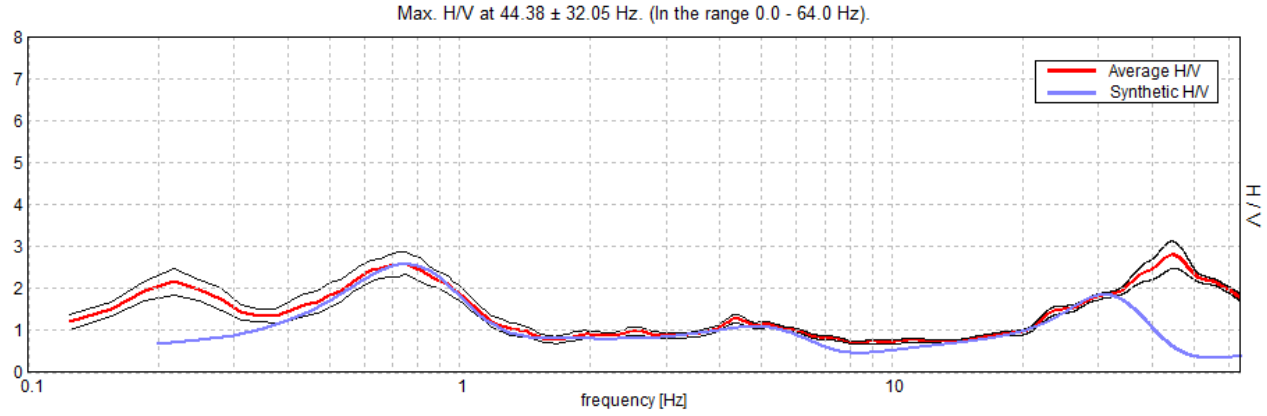
H/V TIME HISTORY



SINGLE COMPONENT SPECTRA

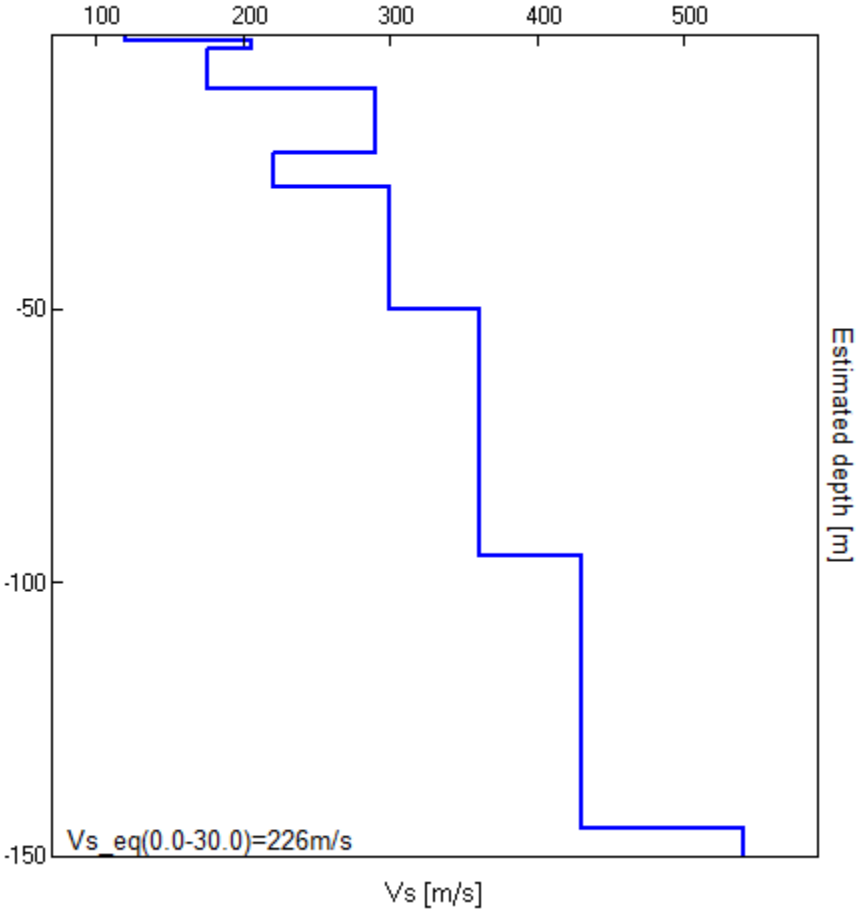


EXPERIMENTAL vs. SYNTHETIC H/V



Depth at the bottom of the layer [m]	Thickness [m]	Vs [m/s]	Poisson ratio
1.00	1.00	120	0.48
2.60	1.60	205	0.48
9.60	7.00	175	0.48
21.50	11.90	290	0.47
27.60	6.10	220	0.48
50.00	22.40	300	0.47
95.00	45.00	360	0.48
145.00	50.00	430	0.46
inf.	inf.	540	0.46

Vs_eq(0.0-30.0)=226m/s


100
200
300
400
500
-50
-100
-150
Vs_eq(0.0-30.0)=226m/s
Vs [m/s]
Estimated depth [m]

[According to the SESAME, 2005 guidelines. **Please read carefully the *Grilla* manual before interpreting the following tables**.]

Max. H/V at 44.38 ± 32.05 Hz (in the range 0.0 - 64.0 Hz).

Criteria for a reliable H/V curve [All 3 should be fulfilled]			
$f_0 > 10 / L_w$	44.38 > 0.50	OK	
$n_c(f_0) > 200$	44375.0 > 200	OK	
$\sigma_A(f) < 2$ for $0.5f_0 < f < 2f_0$ if $f_0 > 0.5$Hz **$\sigma_A(f) < 3$ for $0.5f_0 < f < 2f_0$ if $f_0 < 0.5$Hz**	Exceeded 0 out of 1339 times	OK	
Criteria for a clear H/V peak [At least 5 out of 6 should be fulfilled]			
Exists f^- in $[f_0/4, f_0]$ | $A_{H/V}(f^-) < A_0 / 2$	23.031 Hz	OK	
Exists f^+ in $[f_0, 4f_0]$ | $A_{H/V}(f^+) < A_0 / 2$			NO
$A_0 > 2$	2.80 > 2	OK	
$f_{peak}[A_{H/V}(f) \pm \sigma_A(f)] = f_0 \pm 5\%$	|0.72219| < 0.05		NO
$\sigma_f < \varepsilon(f_0)$	32.04737 < 2.21875		NO
$\sigma_A(f_0) < \theta(f_0)$	0.3256 < 1.58	OK	

L_w	window length
n_w	number of windows used in the analysis
$n_c = L_w n_w f_0$	number of significant cycles
f	current frequency
f_0	H/V peak frequency
σ_f	standard deviation of H/V peak frequency
$\varepsilon(f_0)$	threshold value for the stability condition $\sigma_f < \varepsilon(f_0)$
A_0	H/V peak amplitude at frequency f_0
$A_{H/V}(f)$	H/V curve amplitude at frequency f
f^-	frequency between $f_0/4$ and f_0 for which $A_{H/V}(f^-) < A_0/2$
f^+	frequency between f_0 and $4f_0$ for which $A_{H/V}(f^+) < A_0/2$
$\sigma_A(f)$	standard deviation of $A_{H/V}(f)$, $\sigma_A(f)$ is the factor by which the mean $A_{H/V}(f)$ curve should be multiplied or divided
$\sigma_{logH/V}(f)$	standard deviation of log $A_{H/V}(f)$ curve
$\theta(f_0)$	threshold value for the stability condition $\sigma_A(f) < \theta(f_0)$

Threshold values for σ_f and $\sigma_A(f_0)$					
Freq. range [Hz]	< 0.2	0.2 – 0.5	0.5 – 1.0	1.0 – 2.0	> 2.0
$\varepsilon(f_0)$ [Hz]	0.25 f_0	0.2 f_0	0.15 f_0	0.10 f_0	0.05 f_0
$\theta(f_0)$ for $\sigma_A(f_0)$	3.0	2.5	2.0	1.78	1.58
log $\theta(f_0)$ for $\sigma_{logH/V}(f_0)$	0.48	0.40	0.30	0.25	0.20

Analisi di Risposta sismica locale - SLD

Dati generali

Cantiere	via Guido Reni, Padova
Data della prova	d.C./03/2026
Latitudine	45,4332428[°]
Longitudine	11,8912249[°]

Stratigrafia

n.	Descrizione	Profondità [m]	Spessore [m]	Terreno	Gmax [MPa]	Peso unità vol. [kN/m³]	Vs [m/s]	Tensione verticale [kPa]
1	Argilla prevalente	0.0-1.0	1.0	Vucetic & Dorby (1991) PI=30	25.69	17.5	120.0	8.8
2	Argilla e limo consistenti	1.0-2.6	1.6	Vucetic & Dorby (1991) PI=15	77.11	18.0	205.0	24.1
3	Argilla e argilla limosa	2.6-9.6	7.0	Vucetic & Dorby (1991) PI=30	58.07	18.6	175.0	61.4
4	Sabbia addensata	9.6-21.5	11.9	EPRI Sand (1993) 15,54-36,57 metri	162.88	19.0	290.0	146.8
5	Sabbia e sabbia limosa	21.5-27.6	6.1	Lombardia - Limi sabbiosi	96.21	19.5	220.0	231.0
6	Sabbia addensata	27.6-50.0	22.4	EPRI Sand (1993) 36,88-76,20 metri	183.49	20.0	300.0	374.7
7	Argilla e argilla limosa	50.0-95.0	45.0	Vucetic & Dorby (1991) PI=30	277.43	21.0	360.0	740.6
8	Sabbia addensata prevalente	95.0-145.0	50.0	EPRI Sand (1993) 76,50-152,40 metri	414.66	22.0	430.0	1297.2
9	Sabbia prevalente (si considera il bedrock)	oo	--	Smorzamento costante	683.67	23.0	540.0	1601.9

Strato con falda: 1
Strato rilevamento accelerogramma: 9 Affiorante

Elaborazione SLD

Numero di iterazioni 50
Rapporto tra deformazione a taglio effettiva e deformazione massima 0.5
Tipo di modulo elastico Shake 91
Massimo errore percentuale di convergenza --

Fattori di amplificazione ICMS 2018 - SLD

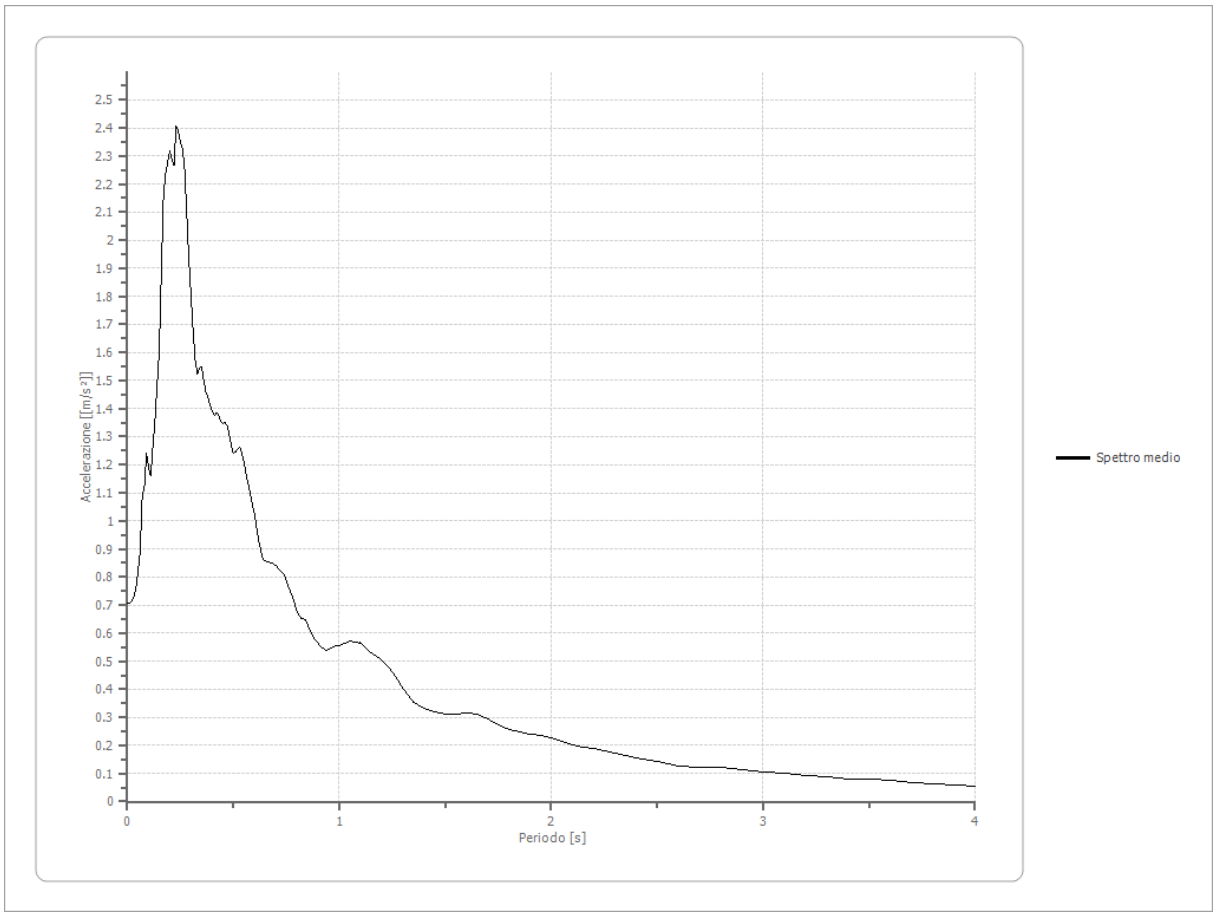
Tai	0.230 [s]
Tvi	0.530 [s]
Tao	0.230 [s]
Tvo	0.530 [s]
Sami	1.188 [m/s²]
Svmi	0.058 [m/s]
Samo	1.955 [m/s²]
Svmo	0.102 [m/s]
Fa	**1.646 [-]**
Fv	**1.743 [-]**
TB	0.109 [s]
TC	0.328 [s]
TD	1.837 [s]
SA(0)	0.581 [m/s²]
SA(TB)	1.955 [m/s²]

Fattori di amplificazione su intensità spettrale - SLD

Periodo minino [s]	Periodo massimo [s]	Int. Housner input [m]	Int. Housner output [m]	Int. Housner input/output [m]	FA
0.100	0.500	0.018	0.030	0.200	1.658
0.400	0.800	0.023	0.039	0.500	1.718
0.700	1.100	0.022	0.038	0.636	1.690

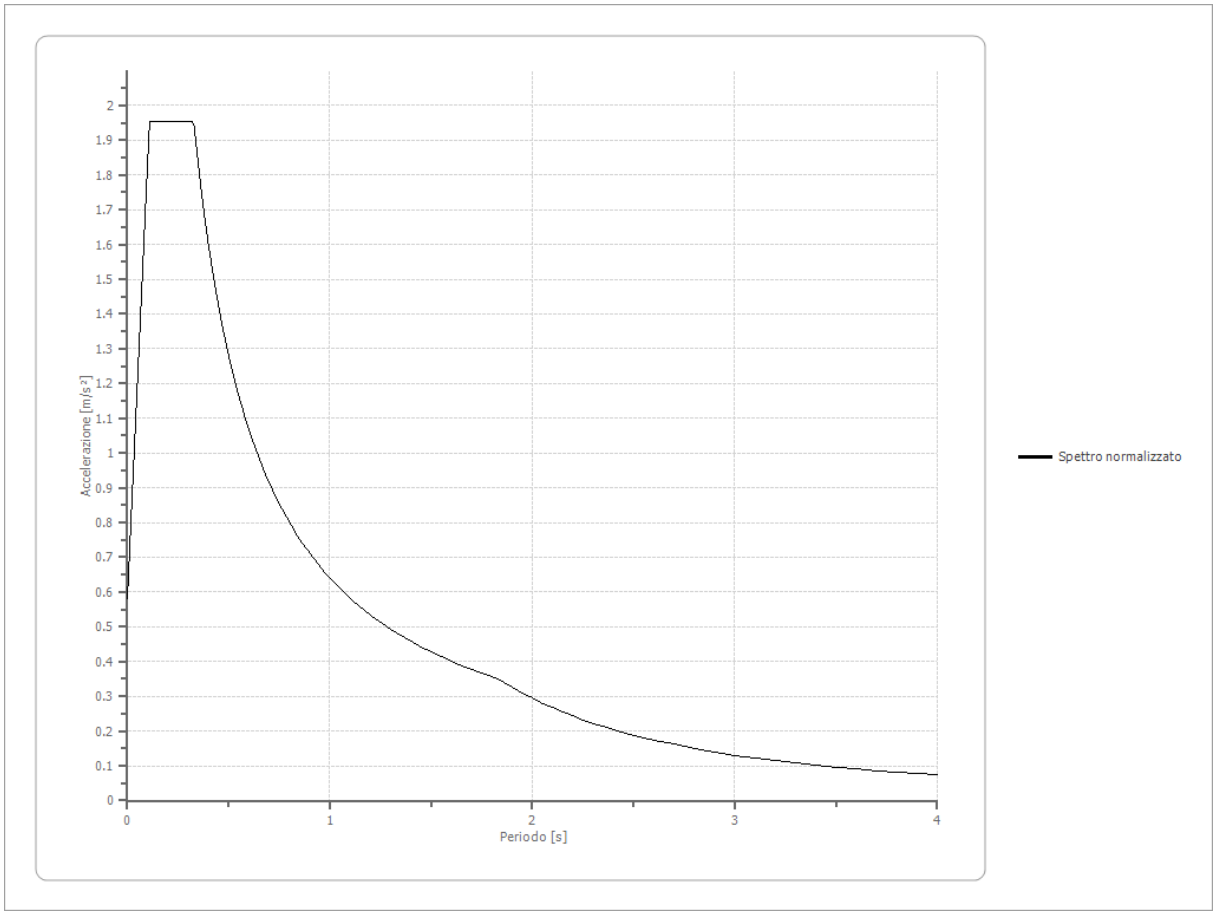
Spettro medio di risposta elastico - SLD

Periodo [s]	Accelerazione [m/s²]	Periodo [s]	Accelerazione [m/s²]	Periodo [s]	Accelerazione [m/s²]	Periodo [s]	Accelerazione [m/s²]	Periodo [s]	Accelerazione [m/s²]
0.00	0.7070	0.26	2.3276	0.52	1.2519	0.98	0.5574	2.25	0.1802
0.01	0.7071	0.27	2.2566	0.53	1.2620	1.00	0.5536	2.30	0.1711
0.02	0.7133	0.28	2.0921	0.54	1.2432	1.05	0.5734	2.35	0.1645
0.03	0.7296	0.29	1.9342	0.55	1.2097	1.10	0.5617	2.40	0.1568
0.04	0.7583	0.30	1.8065	0.56	1.1667	1.15	0.5298	2.50	0.1429
0.05	0.8201	0.31	1.6752	0.57	1.1302	1.20	0.5039	2.60	0.1280
0.06	0.8880	0.32	1.5748	0.58	1.0957	1.25	0.4616	2.70	0.1234
0.07	1.0886	0.33	1.5235	0.60	1.0227	1.30	0.4059	2.80	0.1202
0.08	1.1171	0.34	1.5442	0.62	0.9242	1.35	0.3541	2.90	0.1138
0.09	1.2429	0.35	1.5469	0.64	0.8642	1.40	0.3311	3.00	0.1056
0.10	1.1893	0.36	1.5016	0.66	0.8526	1.45	0.3191	3.10	0.1003
0.11	1.1622	0.37	1.4590	0.68	0.8486	1.50	0.3098	3.20	0.0936
0.12	1.2604	0.38	1.4392	0.70	0.8396	1.55	0.3121	3.30	0.0874
0.13	1.3540	0.39	1.4124	0.72	0.8254	1.60	0.3153	3.40	0.0820
0.14	1.4832	0.40	1.3945	0.74	0.8082	1.65	0.3123	3.50	0.0793
0.15	1.5970	0.41	1.3763	0.76	0.7671	1.70	0.2950	3.60	0.0745
0.16	1.8813	0.42	1.3829	0.78	0.7285	1.75	0.2720	3.70	0.0683
0.17	2.1529	0.43	1.3791	0.80	0.6753	1.80	0.2575	3.80	0.0623
0.18	2.2384	0.44	1.3550	0.82	0.6521	1.85	0.2488	3.90	0.0571
0.19	2.2764	0.45	1.3467	0.84	0.6463	1.90	0.2414	4.00	0.0530
0.20	2.3173	0.46	1.3506	0.86	0.6161	1.95	0.2343		
0.21	2.2827	0.47	1.3437	0.88	0.5785	2.00	0.2260		
0.22	2.2667	0.48	1.3094	0.90	0.5622	2.05	0.2162		
0.23	2.4078	0.49	1.2685	0.92	0.5485	2.10	0.2027		
0.24	2.3882	0.50	1.2410	0.94	0.5403	2.15	0.1954		
0.25	2.3467	0.51	1.2453	0.96	0.5481	2.20	0.1876		



Spettro normalizzato di risposta elastico - SLD

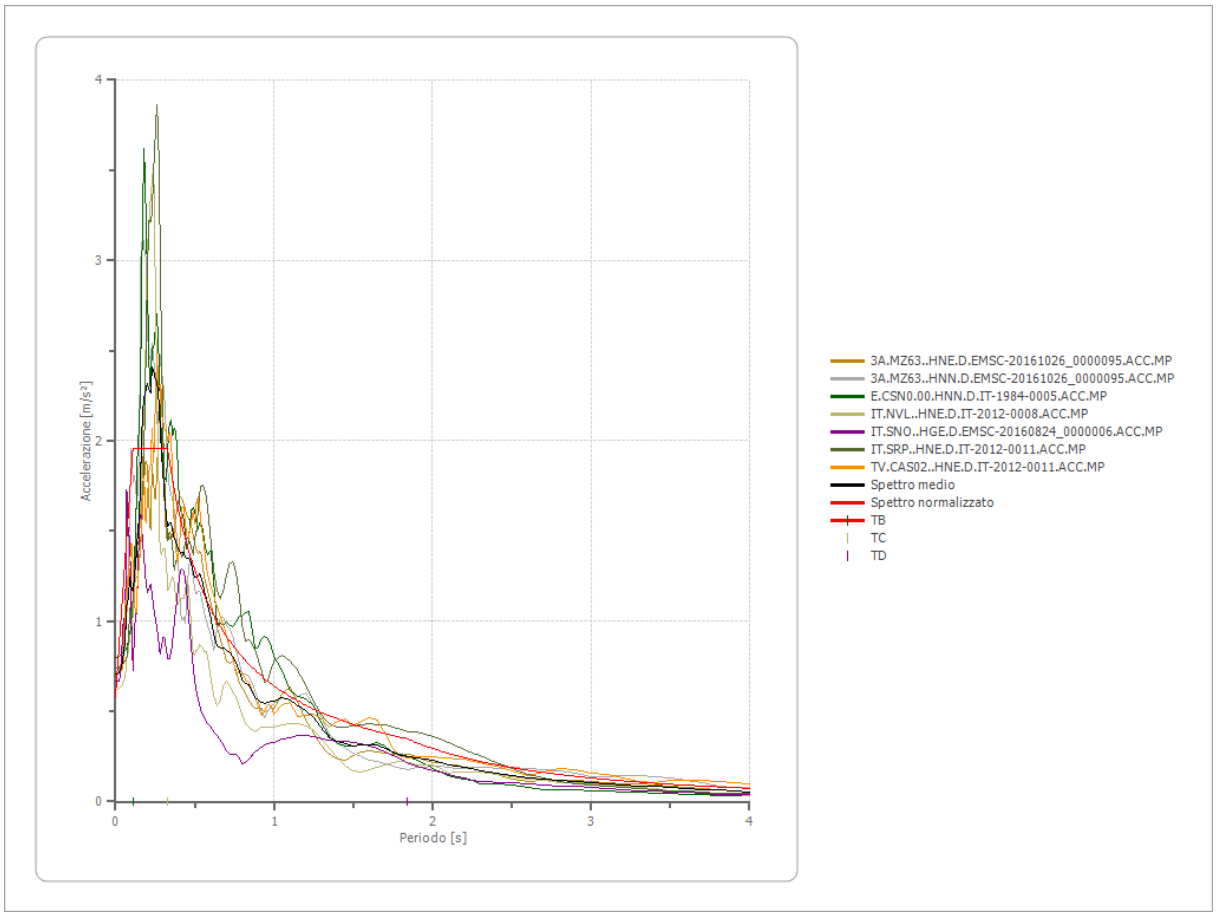
Periodo [s]	Accelerazione [m/s²]	Periodo [s]	Accelerazione [m/s²]	Periodo [s]	Accelerazione [m/s²]	Periodo [s]	Accelerazione [m/s²]	Periodo [s]	Accelerazione [m/s²]
0.00	0.5812	0.26	1.9555	0.52	1.2323	0.98	0.6539	2.25	0.2325
0.01	0.7071	0.27	1.9555	0.53	1.2091	1.00	0.6408	2.30	0.2225
0.02	0.8329	0.28	1.9555	0.54	1.1867	1.05	0.6103	2.35	0.2132
0.03	0.9587	0.29	1.9555	0.55	1.1651	1.10	0.5825	2.40	0.2044
0.04	1.0845	0.30	1.9555	0.56	1.1443	1.15	0.5572	2.50	0.1883
0.05	1.2103	0.31	1.9555	0.57	1.1242	1.20	0.5340	2.60	0.1741
0.06	1.3361	0.32	1.9555	0.58	1.1048	1.25	0.5126	2.70	0.1615
0.07	1.4619	0.33	1.9418	0.60	1.0680	1.30	0.4929	2.80	0.1501
0.08	1.5877	0.34	1.8847	0.62	1.0335	1.35	0.4747	2.90	0.1400
0.09	1.7135	0.35	1.8309	0.64	1.0012	1.40	0.4577	3.00	0.1308
0.10	1.8393	0.36	1.7800	0.66	0.9709	1.45	0.4419	3.10	0.1225
0.11	1.9555	0.37	1.7319	0.68	0.9424	1.50	0.4272	3.20	0.1150
0.12	1.9555	0.38	1.6863	0.70	0.9154	1.55	0.4134	3.30	0.1081
0.13	1.9555	0.39	1.6431	0.72	0.8900	1.60	0.4005	3.40	0.1018
0.14	1.9555	0.40	1.6020	0.74	0.8659	1.65	0.3884	3.50	0.0961
0.15	1.9555	0.41	1.5629	0.76	0.8432	1.70	0.3769	3.60	0.0908
0.16	1.9555	0.42	1.5257	0.78	0.8215	1.75	0.3662	3.70	0.0860
0.17	1.9555	0.43	1.4902	0.80	0.8010	1.80	0.3560	3.80	0.0815
0.18	1.9555	0.44	1.4564	0.82	0.7815	1.85	0.3439	3.90	0.0774
0.19	1.9555	0.45	1.4240	0.84	0.7629	1.90	0.3261	4.00	0.0736
0.20	1.9555	0.46	1.3930	0.86	0.7451	1.95	0.3096		
0.21	1.9555	0.47	1.3634	0.88	0.7282	2.00	0.2943		
0.22	1.9555	0.48	1.3350	0.90	0.7120	2.05	0.2801		
0.23	1.9555	0.49	1.3078	0.92	0.6965	2.10	0.2669		
0.24	1.9555	0.50	1.2816	0.94	0.6817	2.15	0.2547		
0.25	1.9555	0.51	1.2565	0.96	0.6675	2.20	0.2432		



Parametri spettro normalizzato - SLD

Ag [m/s²]	F0	Tc*	TB [s]	TC [s]	TD [s]	Se(0) [m/s²]	Se(TB) [m/s²]	S
0.581	3.364302	--	0.109	0.328	1.837	0.581	1.955	1.318

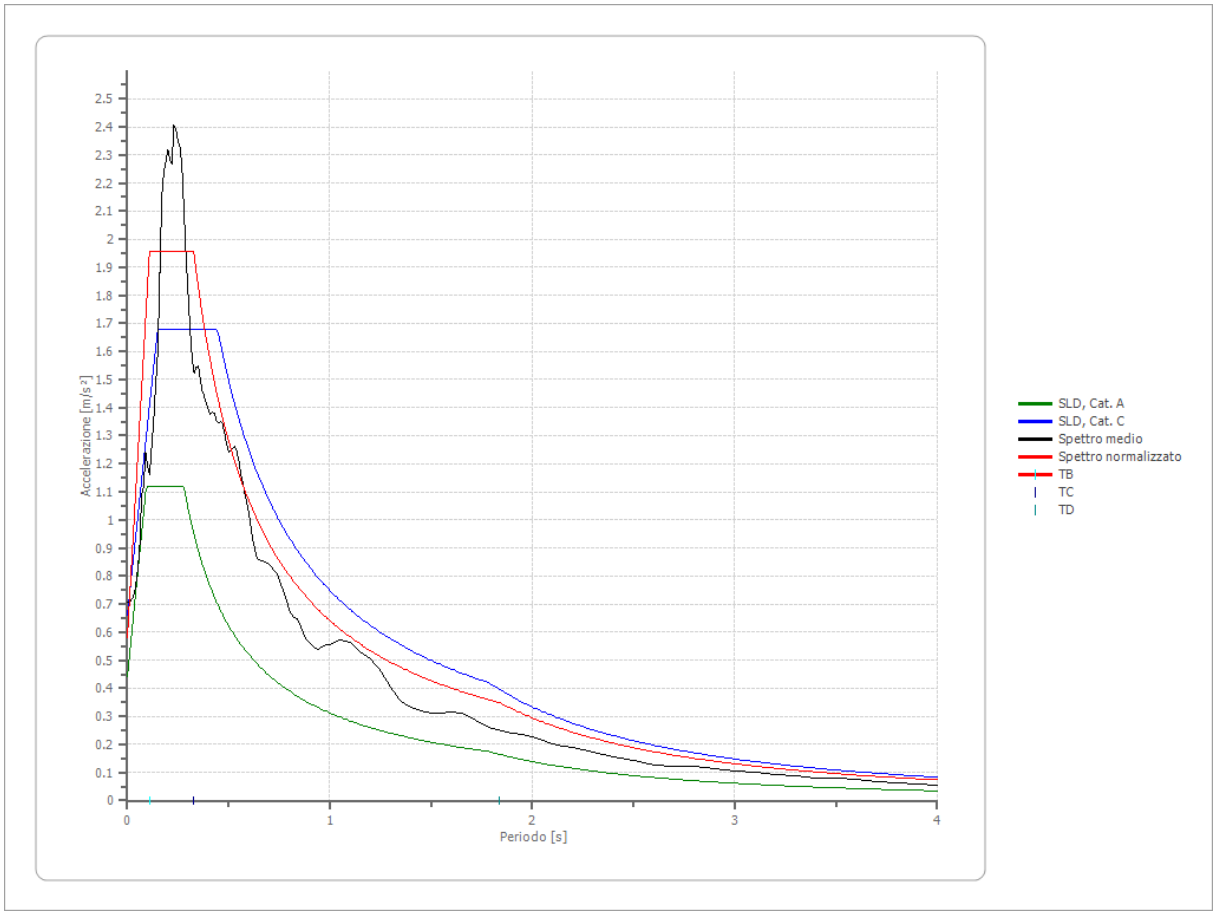
Confronto tra gli spettri - SLD



Confronto spettro normativa - SLD

Tipo di spettro: Spettro di risposta elastico

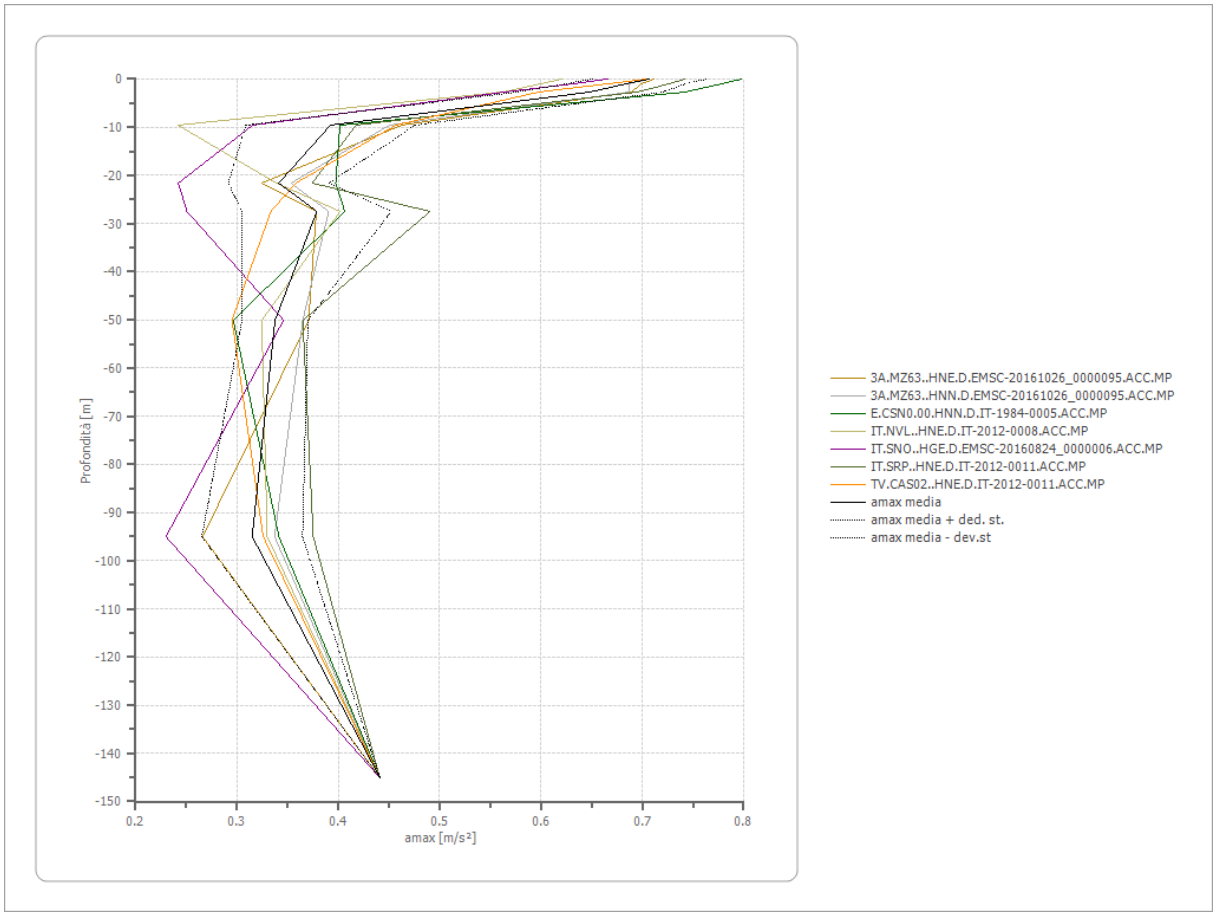
	Operatività SLO Cat. A	Danno SLD Cat. A	Salvaguardia vita SLV Cat. A	Prev. collasso SLC Cat. A	Operatività SLO Cat. C	Danno SLD Cat. C	Salvaguardia vita SLV Cat. C	Prev. collasso SLC Cat. C
Tr [anni]	45	75	712	1462	45	75	712	1462
ag [m/s²]	0.353	0.441	1.040	1.324	0.353	0.441	1.040	1.324
Fo	2.563	2.535	2.568	2.578	2.563	2.535	2.568	2.578
Tc* [s]	0.245	0.279	0.338	0.35	0.245	0.279	0.338	0.35
Ss	1.00	1.00	1.00	1.00	1.50	1.50	1.50	1.49
St	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Cc	1.00	1.00	1.00	1.00	1.67	1.60	1.50	1.48
TB [s]	0.082	0.093	0.113	0.117	0.136	0.149	0.169	0.173
TC [s]	0.245	0.279	0.338	0.350	0.409	0.446	0.508	0.520
TD [s]	1.744	1.780	2.024	2.140	1.744	1.780	2.024	2.140
Se(0) [m/s²]	0.353	0.441	1.040	1.324	0.529	0.662	1.560	1.974
Se(TB) [m/s²]	0.905	1.118	2.671	3.413	1.357	1.677	4.006	5.090



Profilo A_max - SLD

	0.0 [m]	1.0 [m]	2.6 [m]	9.6 [m]	21.5 [m]	27.6 [m]	50.0 [m]	95.0 [m]	145.0 [m]
3A.MZ63..HNE.D.EMSC-20161026_0000095.ACC.MP [m/s²]	0.712	0.699	0.689	0.463	0.324	0.378	0.371	0.266	0.441
3A.MZ63..HNN.D.EMSC-20161026_0000095.ACC.MP [m/s²]	0.707	0.686	0.687	0.450	0.353	0.390	0.365	0.337	0.441
E.CSN0.00.HNN.D.IT-1984-0005.ACC.MP [m/s²]	0.798	0.778	0.742	0.402	0.397	0.406	0.296	0.341	0.441
IT.NVL..HNE.D.IT-2012-0008.ACC.MP [m/s²]	0.621	0.600	0.563	0.242	0.339	0.402	0.324	0.330	0.441
IT.SNO..HGE.D.EMSC-20160824_0000006.ACC.MP [m/s²]	0.666	0.632	0.564	0.315	0.242	0.251	0.346	0.230	0.441
IT.SRP..HNE.D.IT-2012-0011.ACC.MP [m/s²]	0.742	0.726	0.695	0.418	0.374	0.490	0.365	0.375	0.441
TV.CAS02..HNE.D.IT-2012-0011.ACC.MP [m/s²]	0.704	0.666	0.598	0.457	0.358	0.333	0.295	0.326	0.441
media [m/s²]	**0.707**	**0.684**	**0.648**	**0.392**	**0.341**	**0.379**	**0.337**	**0.315**	**0.441**
Dev. St. [m/s²]	0.056	0.059	0.072	0.083	0.050	0.073	0.033	0.050	0.000

Profilo A_max - SLD



Analisi di Risposta sismica locale - SLV

Dati generali

Cantiere	via Guido Reni, Padova
Data della prova	d.C./03/2026
Latitudine	45,4332428[°]
Longitudine	11,8912249[°]

Stratigrafia

n.	Descrizione	Profondità [m]	Spessore [m]	Terreno	Gmax [MPa]	Peso unità vol. [kN/m³]	Vs [m/s]	Tensione verticale [kPa]
1	Argilla prevalente	0.0-1.0	1.0	Vucetic & Dorby (1991) PI=30	25.69	17.5	120.0	8.8
2	Argilla e limo consistenti	1.0-2.6	1.6	Vucetic & Dorby (1991) PI=15	77.11	18.0	205.0	24.1
3	Argilla e argilla limosa	2.6-9.6	7.0	Vucetic & Dorby (1991) PI=30	58.07	18.6	175.0	61.4
4	Sabbia addensata	9.6-21.5	11.9	EPRI Sand (1993) 15,54-36,57 metri	162.88	19.0	290.0	146.8
5	Sabbia e sabbia limosa	21.5-27.6	6.1	Lombardia - Limi sabbiosi	96.21	19.5	220.0	231.0
6	Sabbia addensata	27.6-50.0	22.4	EPRI Sand (1993) 36,88-76,20 metri	183.49	20.0	300.0	374.7
7	Argilla e argilla limosa	50.0-95.0	45.0	Vucetic & Dorby (1991) PI=30	277.43	21.0	360.0	740.6
8	Sabbia addensata prevalente	95.0-145.0	50.0	EPRI Sand (1993) 76,50-152,40 metri	414.66	22.0	430.0	1297.2
9	Sabbia prevalente (si considera il bedrock)	oo	--	Smorzamento costante	683.67	23.0	540.0	1601.9

Strato con falda: 1
Strato rilevamento accelerogramma: 9 Affiorante

Elaborazione - SLV

Numero di iterazioni 50
Rapporto tra deformazione a taglio effettiva e deformazione massima 0.5
Tipo di modulo elastico Shake 91
Massimo errore percentuale di convergenza 3.73 E-05

Fattori di amplificazione ICMS 2018 - SLV

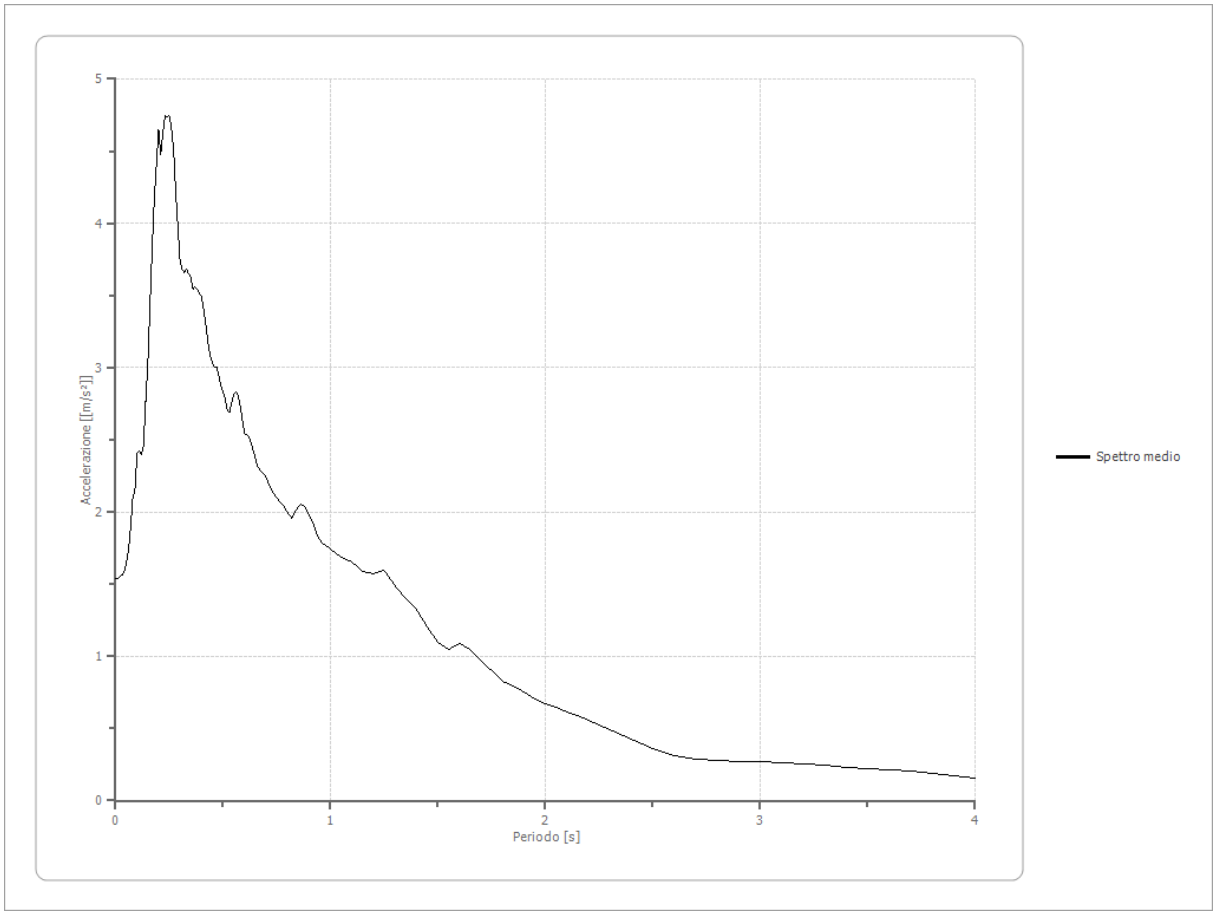
Tai	0.230 [s]
Tvi	1.250 [s]
Tao	0.230 [s]
Tvo	1.250 [s]
Sami	2.719 [m/s²]
Svmi	0.174 [m/s]
Samo	3.923 [m/s²]
Svmo	0.304 [m/s]
Fa	**1.443 [-]**
Fv	**1.746 [-]**
TB	0.162 [s]
TC	0.487 [s]
TD	2.165 [s]
SA(0)	1.386 [m/s²]
SA(TB)	3.923 [m/s²]

Fattori di amplificazione su intensità spettrale - SLV

Periodo minino [s]	Periodo massimo [s]	Int. Housner input [m]	Int. Housner output [m]	Int. Housner input/output [m]	FA
0.100	0.500	0.043	0.064	0.200	1.481
0.400	0.800	0.057	0.095	0.500	1.666
0.700	1.100	0.065	0.109	0.636	1.664

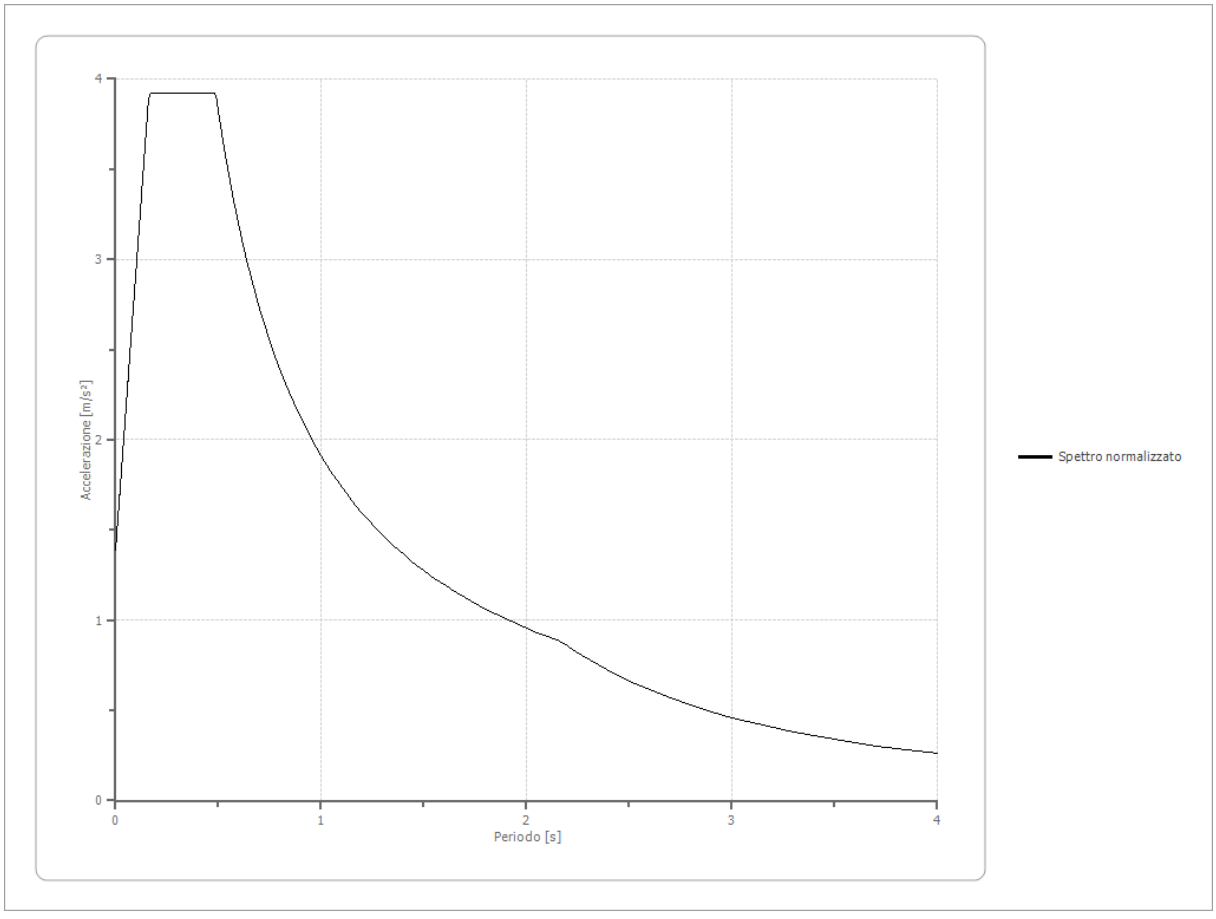
Spettro medio di risposta elastico - SLV

Periodo [s]	Accelerazione [m/s²]	Periodo [s]	Accelerazione [m/s²]	Periodo [s]	Accelerazione [m/s²]	Periodo [s]	Accelerazione [m/s²]	Periodo [s]	Accelerazione [m/s²]
0.00	1.5424	0.26	4.6594	0.52	2.6982	0.98	1.7641	2.25	0.5209
0.01	1.5424	0.27	4.5061	0.53	2.6923	1.00	1.7436	2.30	0.4903
0.02	1.5511	0.28	4.2182	0.54	2.7585	1.05	1.6876	2.35	0.4569
0.03	1.5662	0.29	3.9657	0.55	2.8171	1.10	1.6517	2.40	0.4219
0.04	1.5843	0.30	3.7389	0.56	2.8298	1.15	1.5885	2.50	0.3565
0.05	1.6470	0.31	3.6815	0.57	2.8030	1.20	1.5749	2.60	0.3107
0.06	1.7325	0.32	3.6600	0.58	2.7294	1.25	1.5949	2.70	0.2871
0.07	1.8921	0.33	3.6800	0.60	2.5470	1.30	1.4909	2.80	0.2755
0.08	2.0946	0.34	3.6462	0.62	2.5167	1.35	1.4002	2.90	0.2710
0.09	2.1549	0.35	3.6231	0.64	2.4288	1.40	1.3236	3.00	0.2661
0.10	2.4061	0.36	3.5456	0.66	2.3123	1.45	1.2014	3.10	0.2592
0.11	2.4257	0.37	3.5568	0.68	2.2721	1.50	1.0928	3.20	0.2509
0.12	2.3999	0.38	3.5440	0.70	2.2429	1.55	1.0483	3.30	0.2415
0.13	2.4558	0.39	3.5122	0.72	2.1719	1.60	1.0879	3.40	0.2315
0.14	2.7676	0.40	3.4965	0.74	2.1174	1.65	1.0495	3.50	0.2211
0.15	3.0159	0.41	3.4050	0.76	2.0807	1.70	0.9770	3.60	0.2145
0.16	3.4321	0.42	3.3009	0.78	2.0479	1.75	0.8976	3.70	0.2013
0.17	3.8323	0.43	3.1774	0.80	1.9927	1.80	0.8293	3.80	0.1862
0.18	4.1711	0.44	3.0879	0.82	1.9570	1.85	0.7949	3.90	0.1725
0.19	4.4147	0.45	3.0366	0.84	2.0161	1.90	0.7526	4.00	0.1589
0.20	4.6520	0.46	3.0073	0.86	2.0524	1.95	0.7061		
0.21	4.4770	0.47	3.0009	0.88	2.0338	2.00	0.6696		
0.22	4.6267	0.48	2.9433	0.90	1.9765	2.05	0.6449		
0.23	4.7476	0.49	2.8692	0.92	1.9239	2.10	0.6171		
0.24	4.7347	0.50	2.8353	0.94	1.8347	2.15	0.5855		
0.25	4.7460	0.51	2.7795	0.96	1.7847	2.20	0.5531		



Spettro normalizzato di risposta elastico - SLV

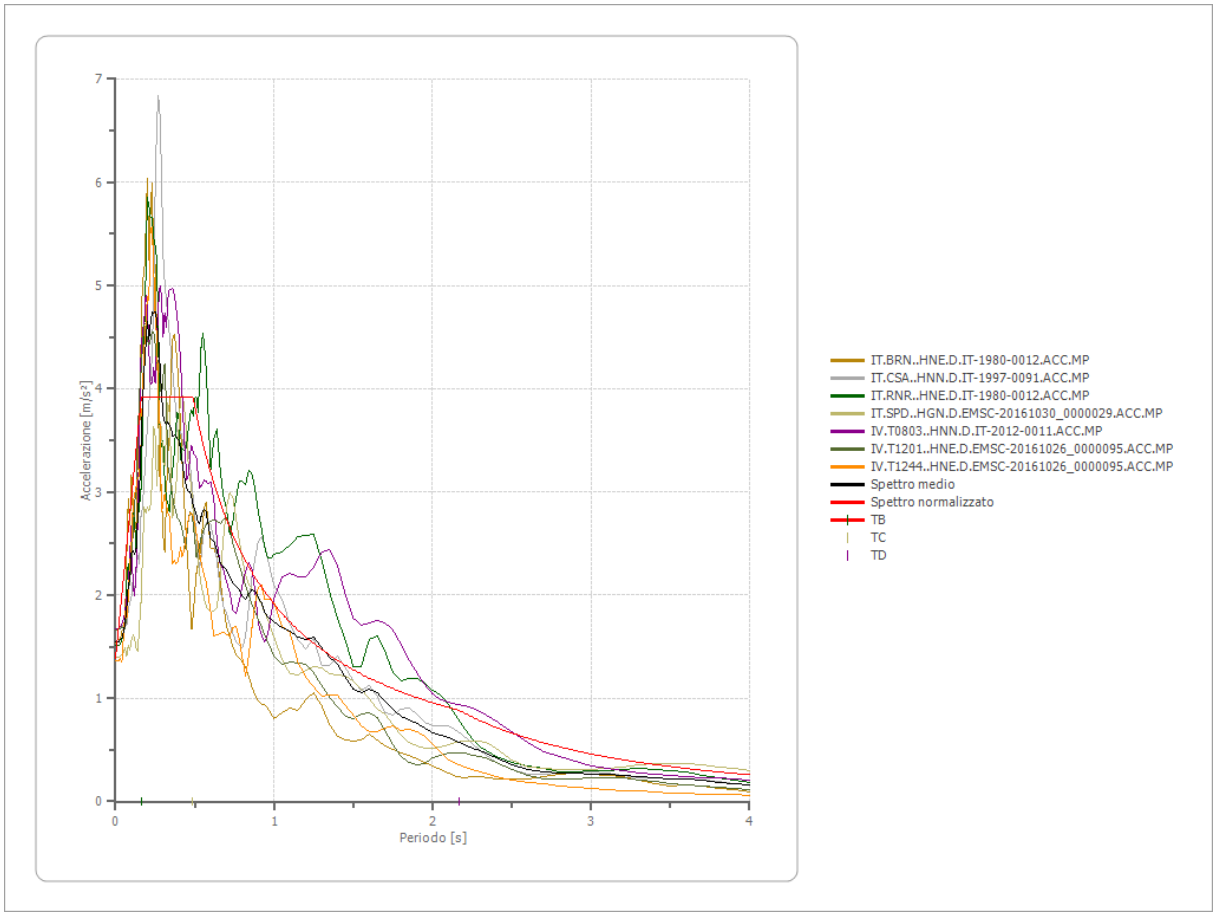
Periodo [s]	Accelerazione [m/s²]	Periodo [s]	Accelerazione [m/s²]	Periodo [s]	Accelerazione [m/s²]	Periodo [s]	Accelerazione [m/s²]	Periodo [s]	Accelerazione [m/s²]
0.00	1.3863	0.26	3.9232	0.52	3.6775	0.98	1.9513	2.25	0.8179
0.01	1.5424	0.27	3.9232	0.53	3.6081	1.00	1.9123	2.30	0.7827
0.02	1.6986	0.28	3.9232	0.54	3.5413	1.05	1.8212	2.35	0.7498
0.03	1.8547	0.29	3.9232	0.55	3.4769	1.10	1.7384	2.40	0.7188
0.04	2.0108	0.30	3.9232	0.56	3.4148	1.15	1.6629	2.50	0.6625
0.05	2.1670	0.31	3.9232	0.57	3.3549	1.20	1.5936	2.60	0.6125
0.06	2.3231	0.32	3.9232	0.58	3.2970	1.25	1.5298	2.70	0.5680
0.07	2.4793	0.33	3.9232	0.60	3.1871	1.30	1.4710	2.80	0.5281
0.08	2.6354	0.34	3.9232	0.62	3.0843	1.35	1.4165	2.90	0.4923
0.09	2.7915	0.35	3.9232	0.64	2.9879	1.40	1.3659	3.00	0.4601
0.10	2.9477	0.36	3.9232	0.66	2.8974	1.45	1.3188	3.10	0.4309
0.11	3.1038	0.37	3.9232	0.68	2.8122	1.50	1.2749	3.20	0.4044
0.12	3.2600	0.38	3.9232	0.70	2.7318	1.55	1.2337	3.30	0.3802
0.13	3.4161	0.39	3.9232	0.72	2.6559	1.60	1.1952	3.40	0.3582
0.14	3.5722	0.40	3.9232	0.74	2.5842	1.65	1.1590	3.50	0.3380
0.15	3.7284	0.41	3.9232	0.76	2.5162	1.70	1.1249	3.60	0.3195
0.16	3.8845	0.42	3.9232	0.78	2.4516	1.75	1.0927	3.70	0.3025
0.17	3.9232	0.43	3.9232	0.80	2.3903	1.80	1.0624	3.80	0.2867
0.18	3.9232	0.44	3.9232	0.82	2.3320	1.85	1.0337	3.90	0.2722
0.19	3.9232	0.45	3.9232	0.84	2.2765	1.90	1.0065	4.00	0.2588
0.20	3.9232	0.46	3.9232	0.86	2.2236	1.95	0.9807		
0.21	3.9232	0.47	3.9232	0.88	2.1730	2.00	0.9561		
0.22	3.9232	0.48	3.9232	0.90	2.1248	2.05	0.9328		
0.23	3.9232	0.49	3.9026	0.92	2.0786	2.10	0.9106		
0.24	3.9232	0.50	3.8246	0.94	2.0343	2.15	0.8894		
0.25	3.9232	0.51	3.7496	0.96	1.9920	2.20	0.8555		



Parametri spettro normalizzato - SLV

Ag [m/s²]	F0	Tc*	TB [s]	TC [s]	TD [s]	Se(0) [m/s²]	Se(TB) [m/s²]	S
1.386	2.829997	--	0.162	0.487	2.165	1.386	3.923	1.333

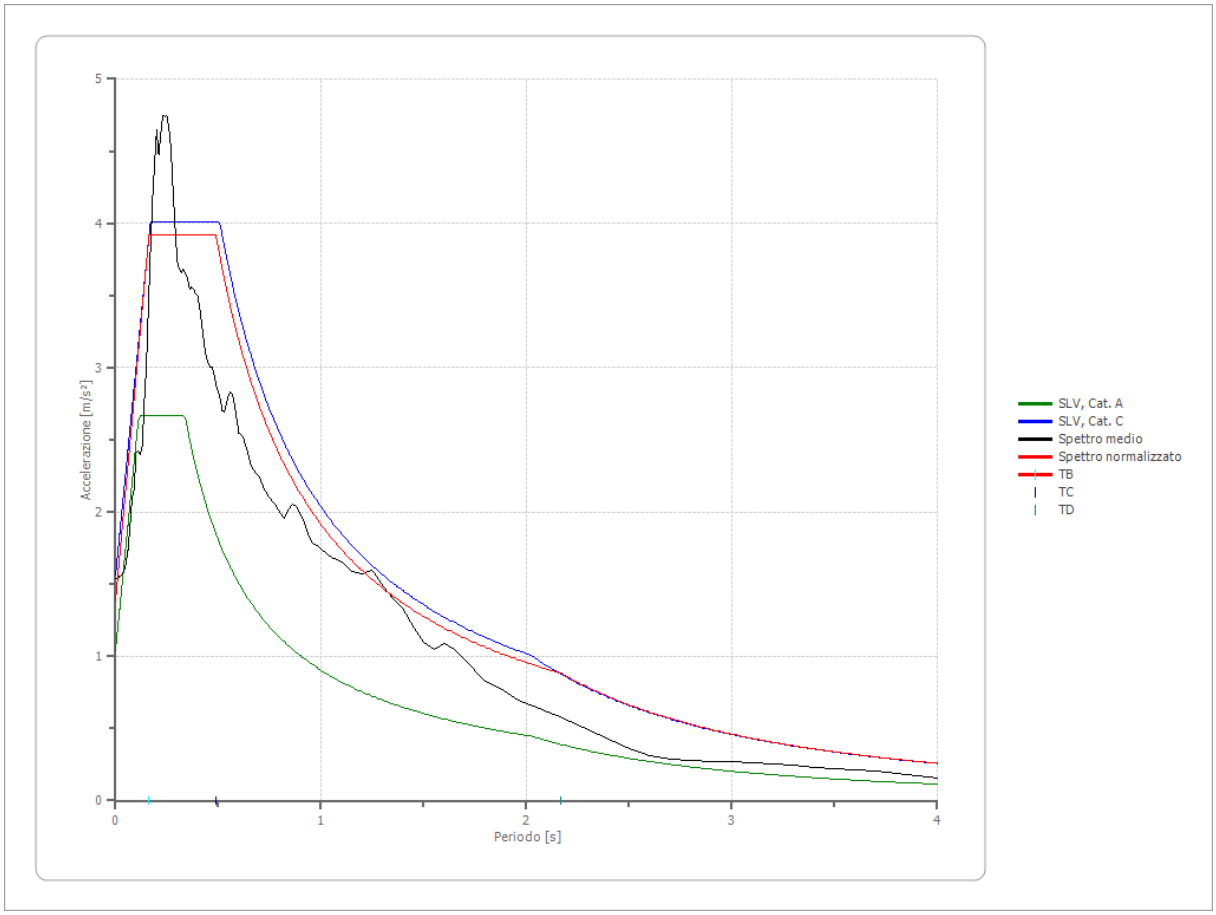
Confronto tra gli spettri - SLV



Confronto spettro normativa - SLV

Tipo di spettro: Spettro di risposta elastico

	Operatività SLO Cat. A	Danno SLD Cat. A	Salvaguardia vita SLV Cat. A	Prev. collasso SLC Cat. A	Operatività SLO Cat. C	Danno SLD Cat. C	Salvaguardia vita SLV Cat. C	Prev. collasso SLC Cat. C
Tr [anni]	45	75	712	1462	45	75	712	1462
ag [m/s²]	0.353	0.441	1.040	1.324	0.353	0.441	1.040	1.324
Fo	2.563	2.535	2.568	2.578	2.563	2.535	2.568	2.578
Tc* [s]	0.245	0.279	0.338	0.35	0.245	0.279	0.338	0.35
Ss	1.00	1.00	1.00	1.00	1.50	1.50	1.50	1.49
St	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Cc	1.00	1.00	1.00	1.00	1.67	1.60	1.50	1.48
TB [s]	0.082	0.093	0.113	0.117	0.136	0.149	0.169	0.173
TC [s]	0.245	0.279	0.338	0.350	0.409	0.446	0.508	0.520
TD [s]	1.744	1.780	2.024	2.140	1.744	1.780	2.024	2.140
Se(0) [m/s²]	0.353	0.441	1.040	1.324	0.529	0.662	1.560	1.974
Se(TB) [m/s²]	0.905	1.118	2.671	3.413	1.357	1.677	4.006	5.090



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	0.0 [m]	1.0 [m]	2.6 [m]	9.6 [m]	21.5 [m]	27.6 [m]	50.0 [m]	95.0 [m]	145.0 [m]
IT.BRN..HNE.D.IT-1980-0012.ACC.MP [m/s²]	1.535	1.462	1.361	0.804	0.871	0.742	0.788	0.743	1.040
IT.CSA..HNN.D.IT-1997-0091.ACC.MP [m/s²]	1.668	1.645	1.598	0.782	0.627	0.900	0.625	0.628	1.040
IT.RNR..HNE.D.IT-1980-0012.ACC.MP [m/s²]	1.507	1.472	1.410	1.099	0.800	0.876	0.684	0.646	1.040
IT.SPD..HGN.D.EMSC-20161030_0000029.ACC.MP [m/s²]	1.393	1.369	1.331	0.894	0.699	0.599	0.693	0.621	1.040
IV.T0803..HNN.D.IT-2012-0011.ACC.MP [m/s²]	1.669	1.629	1.547	0.831	0.784	0.789	1.011	0.708	1.040
IV.T1201..HNE.D.EMSC-20161026_0000095.ACC.MP [m/s²]	1.665	1.642	1.601	1.009	0.896	0.855	0.638	0.643	1.040
IV.T1244..HNE.D.EMSC-20161026_0000095.ACC.MP [m/s²]	1.359	1.310	1.200	0.913	0.760	0.727	0.702	0.656	1.040
media [m/s²]	**1.542**	**1.504**	**1.436**	**0.905**	**0.777**	**0.784**	**0.735**	**0.664**	**1.040**
Dev. St. [m/s²]	0.132	0.137	0.152	0.115	0.093	0.105	0.133	0.045	0.000

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